

Appendix 3.5 Calculations of NO2 Concentration inside the Two Sections of Deckover on Road D1

Section between Area 138L/M and Area 76 R1 Site - Normal speed

Tunnel Parameter

Tunnel length (m), L	=	190
Tunnel height (m), H	=	10
Tunnel width (m), W	=	22
Tunnel size (m ²), At	=	H * W 220
Equivalent diameter (m), dt	=	$(4*At/p)^{0.5}$ 16.73657
Effective length of the tunnel (m), Le	=	L + 2*3*dt 290.4194

Emission Data

	Traffic flow (veh/hr)	Traffic Breakdown (%)				
		P/C	Taxi	Bus	LGV	HGV
Tunnel traffic	4800	51	18	4	9	18
Q (veh/hr)		2448	864	192	432	864
Emission Factor (g/km) - EURO3		P/C 0.71	Taxi 0.73	Bus 6.8	LGV 1.23	HGV 3.84
Weighted NOX E.F. (g/km/veh)	=	1.5674				
NO2 emission factor per unit length (g/m/s), w	=	0.000418				

Vehicle Data

Nominal dimensions of vehicles are given in Transport Planning and Design Manual, Vol. 2 as:

	W	H	L
Cars and Taxi	1.7	1.5	4.6
Bus	2.5	4.6	12
LGV	2.1	1.6	5.2
HGV	2.5	4.6	16
Nominal cross-sectional area (m ²)	= $(1.7*1.5*(0.51+0.18))+(2.5*4.6*0.04)+(2.1*1.6*0.09)+(2.5*4.6*0.18)$ = 4.5919		
Number of lanes per direction, nl	= 2		
Equivalent cross-sectional area for each direction (m ²), Av	= 9.1838		
Equivalent diameter of vehicle (m), dv	= $(4*Av/p)^{0.5}$ = 3.41953		
Traffic density (traffic flow /s), N	= 1.333333		
Average vehicle speed (m/s), v	= 50 km/hr = 13.88889		
Head to head distance on a lane (m), l	= $2*nl*v/N$ = 41.66667		

Diffusion Parameters

Reynolds number, Re	= (v*dv)/s	where s = 15.6*10^-6
	= 3044454	
According to Figure 16 (Ohashi and Koso)		
Since l / dt	= 2.489558	
D / (N * dt^2 * Re^0.13)	= 0.29	
Longitudinal diffusion coefficient (m2/s) , D	= 0.29 * (N * dt^2 * Re^0.13)	
	= 754.2688	

Maximum Concentration of NO2

Cmax (µg/m ³)	= $w * Le^2 / (8 * D * At)$
(without background)	= 26.55591

Appendix 3.5 Calculations of NO2 Concentration inside the Two Sections of Deckover on Road D1

Section between Area 138L/M and Area 76 R1 Site - Worse case

Tunnel Parameter

Tunnel length (m), L	= 190
Tunnel height (m), H	= 10
Tunnel width (m), W	= 22
Tunnel size (m ²), At	= H * W 220
Equivalent diameter (m), dt	= $(4*At/p)^{0.5}$ 16.73657
Effective length of the tunnel (m), Le	= L + 2*3*dt 290.4194

Emission Data

	Traffic flow (veh/hr)	Traffic Breakdown (%)				
		P/C	Taxi	Bus	LGV	HGV
Tunnel traffic	4800	51	18	4	9	18
Q (veh/hr)		2448	864	192	432	864
		P/C	Taxi	Bus	LGV	HGV
Emission Factor (g/km) - EURO3		0.71	0.73	6.8	1.23	3.84
Weighted NOX E.F. (g/km/veh)	= 1.5674					
NO2 emission factor per unit length (g/m/s), w	=	0.000418				

Vehicle Data

Nominal dimensions of vehicles are given in Transport Planning and Design Manual, Vol. 2 as:

	W	H	L
Cars and Taxi	1.7	1.5	4.6
Bus	2.5	4.6	12
LGV	2.1	1.6	5.2
HGV	2.5	4.6	16
Nominal cross-sectional area (m ²)	= $(1.7*1.5*(0.51+0.18))+(2.5*4.6*0.04)+(2.1*1.6*0.09)+(2.5*4.6*0.18)$ = 4.5919		
Number of lanes per direction, nl	= 2		
Equivalent cross-sectional area for each direction (m ²), Av	= 9.1838		
Equivalent diameter of vehicle (m), dv	= $(4*Av/p)^{0.5}$ = 3.41953		
Equivalent length of each vehicle (m)	= $(4.6*(0.51+0.18))+(12*0.04)+(5.2*0.09)+(16*0.18)$ = 7.002		
Distance between vehicle (m)	= 1 (worst case)		
Head to head distance on a lane (m), l	= 8.002		
Traffic density (traffic flow /s), N	= 1.333333		
Average vehicle speed (m/s), v	= $l*N/(2*nl)$ = 2.667333		

Diffusion Parameters

Reynolds number, Re	= $(v*dv)/s$ = 584681.2	where s = $15.6*10^{-6}$
According to Figure 16 (Ohashi and Koso)		
Since l / dt	= 0.478115	
$D / (N * dt^2 * Re^{0.13})$	= 0.13	
Longitudinal diffusion coefficient (m ² /s), D	= $0.13 * (N * dt^2 * Re^{0.13})$ = 272.8442	

Maximum Concentration of NO2

Cmax (µg/m ³)	= $w * Le^2 / (8 * D * At)$
(without background)	= 73.41293

**Appendix 3.5 Calculations of NO2 Concentration inside the Two Sections
of Deckover on Road D1**

**Section between Area 138L/M - Overall Concentrations
and Area 76 R1 Site**

Four assessment points (ASRs P1-P4) at the boundary of the Deckover are chosen (see Figure A3.2).
Using CALINE4 model, the NO2 concentrations at the 4 assessment points at different levels are calculated
(see Appendix A3.1). The highest concentration among the four assessment points is assumed to be the background
NO2 concentration inside the Deckover section.

Elevation NO2 Concentrations (ug/m3) at Various Levels				
(mAG)	P1	P2	P3	P4
0	257	265	381	396
5	402	403	243	258
10	247	256	144	150

Therefore, the background concentration inside the Deckover section is 403 ug/m3.

Overall Maximum NO2 concentration inside
the Deckover section (Normal Speed)

$$\begin{aligned} &= 26.5 + 403 \\ &= 430 \text{ ug/m3} \end{aligned}$$

Overall Maximum NO2 concentration inside
the Deckover section (Worse Case)

$$\begin{aligned} &= 73.4 + 403 \\ &= 477 \text{ ug/m3} \end{aligned}$$

Appendix 3.5 Calculations of NO2 Concentration inside the Two Sections of Deckover on Road D1

Section between Area 138A/B and Area 65D R1 Site - Normal speed

Tunnel Parameter

Tunnel length (m), L	=	115
Tunnel height (m), H	=	10
Tunnel width (m), W	=	22
Tunnel size (m ²), At	=	H * W 220
Equivalent diameter (m), dt	=	$(4*At/p)^{0.5}$ 16.73657
Effective length of the tunnel (m), Le	=	L + 2*3*dt 215.4194

Emission Data

	Traffic flow (veh/hr)	Traffic Breakdown (%)				
		P/C	Taxi	Bus	LGV	HGV
Tunnel traffic	3400	51	18	4	9	18
Q (veh/hr)		1734	612	136	306	612
Emission Factor (g/km) - EURO3		P/C 0.71	Taxi 0.73	Bus 6.8	LGV 1.23	HGV 3.84
Weighted NOX E.F. (g/km/veh)	=	1.5674				
NO2 emission factor per unit length (g/m/s), w	=	0.000296				

Vehicle Data

Nominal dimensions of vehicles are given in Transport Planning and Design Manual, Vol. 2 as:

	W	H	L
Cars and Taxi	1.7	1.5	4.6
Bus	2.5	4.6	12
LGV	2.1	1.6	5.2
HGV	2.5	4.6	16
Nominal cross-sectional area (m ²)	= $(1.7*1.5*(0.51+0.18))+(2.5*4.6*0.04)+(2.1*1.6*0.09)+(2.5*4.6*0.18)$ = 4.5919		
Number of lanes per direction, nl	= 2		
Equivalent cross-sectional area for each direction (m ²), Av	= 9.1838		
Equivalent diameter of vehicle (m), dv	= $(4*Av/p)^{0.5}$ = 3.41953		
Traffic density (traffic flow /s), N	= 0.944444		
Average vehicle speed (m/s), v	= 50 km/hr = 13.88889		
Head to head distance on a lane (m), l	= $2*nl*v/N$ = 58.82353		

Diffusion Parameters

Reynolds number, Re	= (v*dv)/s	where s = 15.6*10^-6
	= 3044454	
According to Figure 16 (Ohashi and Koso)		
Since l / dt	= 3.51467	
D / (N * dt^2 * Re^0.13)	= 0.33	
Longitudinal		
diffusion coefficient (m2/s) , D	= 0.37 * (N * dt^2 * Re^0.13)	
	= 607.9666	

Maximum Concentration of NO2

Cmax (µg/m ³)	= $w * Le^2 / (8 * D * At)$
(without background)	= 12.83996

Appendix 3.5 Calculations of NO2 Concentration inside the Two Sections of Deckover on Road D1

Section between Area 138A/B and Area 65D R1 Site - Worse case

Tunnel Parameter

Tunnel length (m), L	= 115
Tunnel height (m), H	= 10
Tunnel width (m), W	= 22
Tunnel size (m ²), At	= H * W 220
Equivalent diameter (m), dt	= $(4*At/p)^{0.5}$ 16.73657
Effective length of the tunnel (m), Le	= L + 2*3*dt 215.4194

Emission Data

	Traffic flow (veh/hr)	Traffic Breakdown (%)				
		P/C	Taxi	Bus	LGV	HGV
Tunnel traffic	3400	51	18	4	9	18
Q (veh/hr)		1734	612	136	306	612
Emission Factor (g/km) - EURO3		P/C 0.71	Taxi 0.73	Bus 6.8	LGV 1.23	HGV 3.84
Weighted NOX E.F. (g/km/veh)	= 1.5674					
NO2 emission factor per unit length (g/m/s), w			=	0.000296		

Vehicle Data

Nominal dimensions of vehicles are given in Transport Planning and Design Manual, Vol. 2 as:

	W	H	L
Cars and Taxi	1.7	1.5	4.6
Bus	2.5	4.6	12
LGV	2.1	1.6	5.2
HGV	2.5	4.6	16
Nominal cross-sectional area (m ²)	= $(1.7*1.5*(0.51+0.18))+(2.5*4.6*0.04)+(2.1*1.6*0.09)+(2.5*4.6*0.18)$ = 4.5919		
Number of lanes per direction, nl	= 2		
Equivalent cross-sectional area for each direction (m ²), Av	= 9.1838		
Equivalent diameter of vehicle (m), dv	= $(4*Av/p)^{0.5}$ = 3.41953		
Equivalent length of each vehicle (m)	= $(4.6*(0.51+0.18))+(12*0.04)+(5.2*0.09)+(16*0.18)$ = 7.002		
Distance between vehicle (m)	= 1 (worst case)		
Head to head distance on a lane (m), l	= 8.002		
Traffic density (traffic flow /s), N	= 0.944444		
Average vehicle speed (m/s), v	= $l*N/(2*nl)$ = 1.889361		

Diffusion Parameters

Reynolds number, Re	= $(v*dv)/s$	where s = 15.6*10 ⁻⁶
	= 414149.2	
According to Figure 16 (Ohashi and Koso)		
Since l / dt	= 0.478115	
$D / (N * dt^2 * Re^{0.13})$	= 0.13	
Longitudinal		
diffusion coefficient (m ² /s), D	= $0.15 * (N * dt^2 * Re^{0.13})$ = 184.7921	

Maximum Concentration of NO2

Cmax (µg/m ³)	= $w * Le^2 / (8 * D * At)$
(without background)	= 42.24352

Overall Maximum NO2 concentration inside the Deckover section (Worse Case)	=	42.2 + 282	
	=	325	ug/m3

Appendix A3.1 Computer Output of CALINE4 Calculation for the Assessment Points near the Deckover

CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL									
JUNE 1989 VERSION									
PAGE 1									
JOB: TKO - NOX (potral) (WORST CASE ANGLE)									
RUN: NOX									
POLLUTANT: NOX									
I. SITE VARIABLES									
U= 1.0 M/S Z0= 100. CM ALT= 1. (M)									
BRG= WORST CASE VD= .0 CM/S									
CLAS= 4 (D) VS= .0 CM/S									
MINH= 50. DEGREES									
SIGTH= 18. DEGREES TEMP= 25.0 DEGREE (C)									
II. LINK VARIABLES									
LINK	*	LINK COORDINATES (M)				*	EF	H	W
DESCRIPTION	*	X1	Y1	X2	Y2	* TYPE	VPH	(G/MI)	(M)
-----	*	-----	-----	-----	-----	-----	-----	-----	-----
0. 1	*	44560	17360	44679	17298	* BG	5700	318.7	8.3 32.0
1. 2	*	44679	17298	44847	17160	* BG	5700	318.7	19.5 26.0
2. 3	*	44947	17160	45079	17093	* BG	5700	318.7	27.5 26.0
3. 4	*	45079	17093	45172	17057	* BG	5700	318.7	28.0 26.0
4. 5	*	45172	17057	45300	17029	* BG	5700	318.7	24.0 26.0
5. 6	*	45300	17029	45402	17020	* BG	5700	318.7	20.0 26.0
6. 7	*	45402	17020	45525	17021	* BG	5700	318.7	16.0 26.0
7. 8	*	45176	18204	45195	18083	* BG	1800	218.5	8.5 26.0
8. 9	*	45195	18083	45264	17800	* BG	1800	218.5	11.3 26.0
9. 10	*	45264	17800	45299	17663	* AG	1800	218.5	.0 26.0
0. 11	*	45299	17663	45326	17602	* AG	1800	218.5	.0 26.0
1. 12	*	45333	17607	45383	17552	* AG	625	240.0	.0 16.0
2. 13	*	45383	17552	45459	17511	* AG	625	240.0	.0 16.0
3. 14	*	45459	17511	45537	17504	* AG	625	240.0	.0 16.0
4. 15	*	45319	17597	45364	17539	* AG	625	240.0	.0 16.0
5. 16	*	45364	17539	45438	17496	* AG	625	240.0	.0 16.0
6. 17	*	45438	17496	45534	17478	* AG	625	240.0	.0 16.0
7. 18	*	45326	17602	45377	17548	* BG	550	169.5	1.9 20.0
8. 19	*	45377	17548	45456	17502	* BG	550	169.5	5.6 20.0
9. 20	*	45456	17502	45534	17489	* BG	550	169.5	9.4 20.0
0. 21	*	44343	18173	44367	18100	* AG	2150	297.5	.0 24.0
1. 22	*	44367	18100	44374	17984	* FL	2150	297.5	7.5 20.0
2. 23	*	44374	17984	44367	17828	* FL	2150	297.5	7.5 18.0
3. 24	*	44438	18172	44412	18099	* AG	3600	225.4	.0 22.0
4. 25	*	44412	18099	44489	18009	* FL	3600	225.4	7.5 22.0
5. 26	*	44489	18009	44497	17827	* FL	3600	225.4	7.5 22.0
6. 27	*	44371	17828	44361	17734	* BG	2000	278.4	4.4 14.0
7. 28	*	44361	17734	44345	17670	* BG	2000	278.4	7.2 14.0
8. 29	*	44345	17670	44325	17615	* BG	2000	278.4	10.0 14.0
9. 30	*	44401	17827	44394	17751	* BG	3450	211.2	8.9 14.0
0. 31	*	44394	17751	44374	17667	* BG	3450	211.2	11.7 14.0
1. 32	*	44374	17667	44350	17603	* BG	3450	211.2	14.5 14.0
2. 33	*	44338	17608	44296	17534	* BG	8500	240.2	15.8 36.0
3. 34	*	44296	17534	44236	17474	* BG	8500	242.6	13.0 32.0
4. 35	*	44236	17474	44124	17404	* BG	8500	242.6	8.0 32.0
5. 36	*	44124	17404	44015	17331	* BG	8500	242.6	14.0 32.0
6. 37	*	44000	17340	44000	17400	* BG	2400	367.2	15.5 14.0
7. 38	*	44000	17400	44121	17445	* BG	2400	367.2	16.5 14.0
8. 39	*	44121	17445	44192	17476	* BG	2400	367.2	12.0 14.0
9. 40	*	44192	17476	44255	17484	* BG	2400	367.2	13.5 14.0
0. 41	*	44255	17484	44337	17473	* BG	2400	367.2	23.5 14.0
1. 42	*	44337	17473	44419	17438	* BG	2400	367.2	15.0 14.0
2. 43	*	44419	17438	44497	17365	* BG	2400	367.2	9.8 14.0
3. 44	*	44025	17318	44132	17387	* BG	3100	270.1	8.0 14.0
4. 45	*	44132	17387	44201	17418	* BG	3100	270.1	8.0 14.0
5. 46	*	44201	17418	44281	17442	* BG	3100	270.1	17.5 14.0
6. 47	*	44281	17442	44345	17442	* BG	3100	270.1	11.8 14.0
7. 48	*	44345	17442	44401	17433	* BG	3100	270.1	27.5 14.0
8. 49	*	44391	17433	44445	17413	* BG	3100	270.1	9.0 14.0
9. 50	*	44445	17413	44557	17357	* BG	3100	270.1	8.8 14.0
0. 51	*	44363	17828	44344	17708	* AG	150	552.5	.0 14.0
1. 52	*	44344	17708	44321	17625	* AG	150	552.5	.0 14.0
2. 53	*	44321	17625	44302	17564	* AG	150	552.5	.0 14.0
3. 54	*	44302	17564	44293	17545	* AG	150	552.5	.0 14.0
4. 55	*	44410	17827	44404	17757	* FL	150	552.5	5.0 14.0
5. 56	*	44404	17757	44386	17680	* AG	150	552.5	.0 14.0
6. 57	*	44386	17680	44369	17628	* AG	150	552.5	.0 14.0
7. 58	*	44369	17628	44346	17584	* AG	150	552.5	.0 14.0
8. 59	*	44346	17584	44323	17552	* AG	150	552.5	.0 14.0
9. 60	*	44324	17552	44308	17533	* AG	150	552.5	.0 14.0
0. 61	*	44299	17539	44255	17484	* AG	400	509.7	.0 30.0
1. 62	*	44255	17484	44218	17434	* AG	400	509.7	.0 20.0
2. 63	*	44218	17434	44158	17382	* AG	400	509.7	.0 20.0
3. 64	*	44158	17382	44047	17295	* AG	400	509.7	.0 20.0
4. 65	*	44318	17533	44395	17465	* BG	150	462.8	7.0 14.0
5. 66	*	44395	17465	44444	17433	* BG	150	462.8	1.3 14.0
6. 67	*	44444	17433	44565	17371	* BG	150	462.8	5.5 10.0
7. 68	*	44389	17522	44361	17480	* BG	150	462.8	7.0 14.0
8. 69	*	44361	17480	44405	17423	* BG	150	462.8	1.3 14.0
9. 70	*	44405	17423	44449	17394	* BG	150	462.8	3.5 14.0
0. 71	*	44449	17394	44554	17350	* BG	1100	462.8	6.5 14.0
1. 72	*	44707	18172	44706	17835	* AG	2400	241.4	.0 22.0
2. 73	*	44986	18174	44986	17834	* AG	650	241.4	.0 22.0
3. 74	*	44700	18630	44711	18573	* AG	1650	241.4	.0 32.0
4. 75	*	44711	18573	44707	18466	* AG	1650	241.4	.0 28.0
5. 76	*	44707	18466	44707	18367	* AG	1650	241.4	.0 24.0
6. 77	*	44707	18367	44703	18173	* AG	1950	247.0	.0 23.0
7. 78	*	44973	18732	44986	18661	* AG	600	258.1	.0 26.0
8. 79	*	44986	18661	44987	18432	* AG	600	258.1	.0 23.0
9. 80	*	44987	18431	44986	18175	* AG	800	236.3	.0 23.0
0. 81	*	45341	18424	45218	18220	* FL	1800	252.2	7.3 23.0
1. 82	*	45223	18220	45311	18598	* FL	1850	235.5	5.0 23.0
2. 83	*	45311	18598	45347	18492	* FL	1850	235.5	7.3 23.0
3. 84	*	45347	18492	45341	18424	* FL	1850	235.5	7.3 23.0
4. 85	*	44143	18393	44200	18248	* FL	2800	210.9	7.3 22.0
5. 86	*	44200	18248	44241	18202	* FL	2800	210.9	7.3 24.0
6. 87	*	44241	18202	44302	18174	* FL	2800	210.9	7.3 24.0
7. 88	*	44302	18174	44343	18173	* FL	2800	210.9	7.3 32.0
8. 89	*	44394	18523	44389	18400	* FL	4300	274.0	8.0 36.0
9. 90	*	44390	18400	44390	18173	* BG	4050	254.4	11.7 24.0
0. 91	*	44390	18173	44388	17828	* BG	4050	254.4	16.3 24.0
1. 92	*	44388	17828	44373	17716	* BG	4050	254.4	17.2 24.0
2. 93	*	44373	17716	44340	17608	* BG	4050	254.4	11.9 24.0
3. 94	*	44375	18400	44375	18270	* FL	150	552.5	7.5 12.0
4. 95	*	44375	18270	44343	18173	* FL	150	552.5	7.5 12.0
5. 96	*	44406	18400	44405	18266	* FL	150	552.5	8.0 14.0
6. 97	*	44405	18266	44438	18172	* FL	150	552.5	5.0 14.0
7. 98	*	45893	19724	45877	19492	* AG	2550	394.9	.0 26.0
8. 99	*	45877	19492	45806	19424	* AG	1850	394.9	.0 26.0
9. 100	*	45806	19424	45489	19316	* AG	2950	318.6	.0 26.0
0. 101	*	45489	19316	45401	19208	* AG	2950	318.6	.0 26.0
1. 102	*	45893	19724	45908	19652	* AG	1850	270.7	.0 14.0

3. 103	*	5980	19552	46065	19555	FL	1850	270.7	5.0	20.0
4. 104	*	46065	19555	46132	19496	AG	1850	270.7	.0	20.0
5. 105	*	46132	19496	46233	19454	AG	1850	270.7	.0	20.0
6. 106	*	46233	19454	46250	19427	AG	1850	270.7	.0	20.0
7. 107	*	46250	19427	46252	19300	AG	1850	270.7	.0	20.0
8. 108	*	46252	19300	46208	19211	AG	1850	270.7	.0	20.0
9. 109	*	46208	19211	46233	19129	AG	1850	270.7	.0	20.0
10. 110	*	46233	19129	46339	19025	AG	1850	270.7	.0	20.0
11. 111	*	46339	19025	46339	19025	AG	1850	270.7	.0	20.0
12. 112	*	46342	18932	46341	18881	FL	1850	270.7	7.3	20.0
1. 113	*	46341	18881	46339	18791	FL	1850	270.7	7.3	20.0
2. 114	*	46339	18791	46341	18881	FL	1850	270.7	5.5	20.0
3. 115	*	46337	18711	46345	18561	FL	1850	270.7	5.5	20.0
4. 116	*	46341	18562	46338	18461	AG	1850	270.7	.0	20.0
5. 117	*	46338	18461	46313	18399	AG	1850	270.7	.0	20.0
6. 118	*	46317	18397	46284	18349	FL	1850	270.7	8.0	20.0
7. 119	*	46284	18349	46285	18295	FL	1850	270.7	8.0	20.0
8. 120	*	46226	18305	46098	19211	FL	1850	270.7	8.0	20.0
9. 121	*	45408	20071	45529	18888	AG	900	344.0	.0	26.0
10. 122	*	45529	18888	45623	19954	AG	900	344.0	.0	26.0
1. 123	*	45623	19954	45993	19725	AG	900	344.0	.0	26.0
2. 124	*	45993	19725	45996	20032	AG	2650	274.7	.0	14.0
3. 125	*	45996	20032	45997	19954	AG	2650	274.7	.0	14.0
4. 126	*	45988	19938	45953	19810	AG	2650	274.7	.0	18.0
5. 127	*	45953	19810	45993	19725	AG	2650	274.7	.0	22.0
6. 128	*	45516	18986	45563	18919	AG	1900	250.1	.0	21.0
7. 129	*	45563	18919	45627	18851	AG	1900	250.1	.0	21.0
8. 130	*	45627	18851	45656	18800	AG	1900	250.1	.0	21.0
9. 131	*	45656	18800	45694	18696	AG	1900	250.1	.0	21.0
10. 132	*	45694	18696	45745	18613	AG	1900	250.1	.0	21.0
1. 133	*	45755	18615	45870	18509	AG	1900	250.1	.0	21.0
2. 134	*	45870	18509	45910	18460	AG	1900	250.1	.0	21.0
3. 135	*	45910	18460	45957	18359	AG	1900	250.1	.0	21.0
4. 136	*	45957	18359	46028	18263	AG	1900	250.1	.0	21.0
5. 137	*	46028	18266	46038	18166	AG	1900	250.1	.0	21.0
6. 138	*	46095	18216	46116	18186	AG	1550	295.1	.0	21.0
7. 139	*	46116	18163	46110	18000	AG	1550	295.1	.0	21.0
8. 140	*	46110	18000	46059	18080	AG	1550	295.1	.0	21.0
9. 141	*	46059	18080	46018	17957	AG	1550	295.1	.0	21.0
10. 142	*	46018	17957	46018	17957	AG	1550	295.1	.0	21.0
1. 143	*	46093	17895	46011	17831	AG	1550	295.1	.0	21.0
2. 144	*	46011	17831	46073	17692	AG	1550	295.1	.0	21.0
3. 145	*	47707	18431	44461	18430	AG	550	202.2	.0	16.0
4. 146	*	44461	18430	44435	18408	AG	550	202.2	.0	16.0
5. 147	*	44435	18408	44435	18373	AG	550	202.2	.0	16.0
6. 148	*	44435	18373	44435	18344	AG	800	224.0	.0	16.0
7. 149	*	44434	18344	44458	18320	AG	800	224.0	.0	16.0
8. 150	*	44458	18320	44706	18319	AG	800	224.0	.0	18.0
9. 151	*	44706	18318	44987	18500	AG	900	263.1	.0	16.0
10. 152	*	44987	18432	45298	18431	AG	700	224.0	.0	16.0
1. 153	*	45298	18431	45342	18424	AG	700	224.0	.0	18.0
2. 154	*	44706	17834	44822	17833	AG	1250	215.9	.0	16.0
3. 155	*	44706	17834	44822	17833	AG	1250	215.9	.0	16.0
4. 156	*	44822	17833	44865	17833	AG	1250	215.9	.0	16.0
5. 157	*	44865	17833	44986	17833	AG	1000	305.1	-2.0	22.0
6. 158	*	44706	17834	44705	17641	AG	650	224.0	.0	20.0
7. 159	*	44986	17833	44988	17684	AG	400	531.1	.0	20.0
8. 160	*	45665	18321	45665	18321	AG	1250	215.9	.0	16.0
9. 161	*	43752	18229	43813	18193	AG	1250	215.9	.0	16.0
10. 162	*	43813	18193	43897	18190	AG	1250	215.9	.0	16.0
1. 163	*	43897	18190	43975	18236	AG	1250	215.9	.0	16.0
2. 164	*	43975	18236	44144	18398	AG	1250	215.9	.0	16.0
3. 165	*	43665	18321	43794	18365	AG	1750	236.6	.0	16.0
4. 166	*	43794	18365	43813	18193	AG	1750	236.6	.0	22.0
5. 167	*	43887	18415	44041	18451	AG	1750	236.6	.0	22.0
6. 168	*	45264	18860	45391	18926	AG	3400	303.8	.0	22.0
7. 169	*	45391	18926	45299	19087	AG	3400	303.8	.0	22.0
8. 170	*	45299	19087	45398	19259	AG	3400	303.8	.0	22.0
9. 171	*	45267	19345	45267	19345	AG	1650	233.0	.0	46.0
10. 172	*	45398	19210	45438	19100	AG	700	233.0	.0	46.0
1. 173	*	45438	19150	45512	18970	AG	700	233.0	.0	44.0
2. 174	*	45267	19345	45398	19210	AG	1250	271.8	4.0	16.0
3. 175	*	45398	19210	45438	19150	AG	1250	271.8	6.9	16.0
4. 176	*	45438	19150	45512	18977	AG	1250	271.8	2.9	16.0
5. 177	*	45041	18551	44107	18464	AG	2650	215.9	.0	39.0
6. 178	*	44107	18464	44145	18397	AG	2650	215.9	.0	39.0
7. 179	*	44220	18454	44285	18489	AG	650	224.6	1.7	20.0
8. 180	*	44285	18489	44355	18513	AG	650	224.6	5.1	20.0
9. 181	*	44355	18513	44404	18527	AG	650	224.6	8.0	20.0
10. 182	*	44404	18527	44453	18543	AG	650	224.6	5.6	20.0
1. 183	*	44144	18397	44107	18464	AG	1150	262.0	.0	32.0
2. 184	*	44220	18454	44285	18489	AG	1150	262.0	.0	32.0
3. 185	*	44285	18489	44355	18513	AG	1150	262.0	.0	32.0
4. 186	*	44355	18513	44404	18527	AG	1150	262.0	.0	32.0
5. 187	*	44404	18527	44453	18543	AG	2950	535.7	.0	32.0
6. 188	*	44668	18615	44715	18634	AG	2950	535.7	.0	30.0
7. 189	*	44715	18634	44705	18615	AG	2350	535.8	.0	28.0
8. 190	*	44762	18651	44898	18705	AG	2350	535.8	.0	28.0
9. 191	*	44898	18705	44947	18722	AG	2350	535.8	.0	28.0
10. 192	*	44947	18722	44974	18739	AG	2450	764.3	.0	28.0
1. 193	*	45178	18808	45223	18831	AG	2450	764.3	.0	36.0
2. 194	*	45223	18831	45264	18846	AG	3400	764.3	.0	16.0
3. 195	*	44041	18551	44041	18636	AG	1550	271.8	.0	20.0
4. 196	*	44041	18551	44000	18649	AG	900	271.8	.0	26.0
5. 197	*	44000	18639	44022	18727	AG	900	271.8	.0	26.0
6. 198	*	44022	18726	44087	18786	AG	900	258.3	.0	22.0
7. 199	*	44087	18786	44338	18928	AG	900	258.3	.0	22.0
8. 200	*	44338	18928	44393	18948	AG	900	258.3	.0	22.0
9. 201	*	44393	18948	44393	18948	AG	1300	242.4	6.1	16.0
10. 202	*	44565	19010	44388	19109	AG	1000	265.3	.0	24.0
1. 203	*	44838	19109	45043	19186	AG	550	232.6	.0	24.0
2. 204	*	44533	18772	44640	18807	AG	1200	202.2	.0	20.0
3. 205	*	44640	18807	44912	18907	AG	650	226.5	.0	20.0
4. 206	*	44912	18907	44912	18907	AG	1250	252.2	.0	23.0
5. 207	*	44640	18807	44702	18628	AG	1250	252.2	.0	23.0
6. 208	*	44912	18907	44975	18733	AG	1300	302.3	.0	23.0
7. 209	*	44565	19010	44640	18807	AG	500	226.5	.0	23.0
8. 210	*	44838	19109	44912	18907	AG	500	236.3	.0	23.0
9. 211	*	44943	19301	45044	19186	AG	850	241.3	.0	26.0
10. 212	*	45044	19186	45115	19095	AG	800	252.2	.0	24.0
1. 213	*	45115	19095	45180	18950	AG	800	252.2	.0	24.0
2. 214	*	45180	18950	45223	18831	AG	800	252.2	.0	24.0
3. 215	*	44438	19150	44496	19047	AG	1000	271.0	.0	36.0
4. 216	*	44406	19047	44393	18948	AG	1000	271.0	.0	46.0
5. 217	*	44393	18948	44391	18730	AG	900	271.8	.0	36.0
6. 218	*	44438	19150	44496	19047	AG	1300	242.4	2.9	16.0
7. 219	*	44406	19047	44393	18948	AG	1300	242.4	6.1	16.0
8. 220	*	44393	18948	44391	18730	AG	1300	242.4	4.0	16.0
9. 221	*	44391	18731	44393	18524	AG	2250	252.2	.0	32.0
10. 222	*	45526	17021	45797	17022	FL	5700	318.7	8.0	32.0
1. 223	*	45537	17594	45584	17592	AG	450	250.1	.0	13.5
2. 224	*	45584	17592	45582	17532	AG	450	250.1	.0	13.5
3. 225	*	45622	17532	45864	17611	AG	450	250.1	.0	13.5
4. 226	*	45536	17477	45591	17492	AG	450	250.1	.0	13.5
5. 227	*	45591	17492	45708	17532	AG	450	250.1	.0	

7. 238	*	46228	16882	46268	16774	*	AG	4200	413.3	.0	34.0
8. 239	*	46268	16774	46360	16604	*	AG	4200	413.3	.0	34.0
9. 240	*	46360	16604	46410	16466	*	AG	4200	413.3	.0	34.0
0. 241	*	44385	18169	44435	18170	*	FL	4800	412.0	5.0	28.0
1. 242	*	44435	18170	44486	18170	*	FL	4800	571.7	5.0	28.0
2. 243	*	44677	18172	44727	18173	*	AG	4800	571.7	.0	28.0
3. 244	*	44727	18173	44777	18173	*	FL	2800	521.1	5.0	28.0
4. 245	*	44777	18173	44910	18173	*	AG	2800	247.2	.0	28.0
5. 246	*	44910	18173	44960	18173	*	FL	2800	364.6	5.5	28.0
6. 247	*	44960	18173	45010	18172	*	AG	3400	445.6	.0	28.0
7. 248	*	45124	18177	45169	18198	*	FL	3400	445.6	6.0	28.0
8. 249	*	45170	18198	45215	18218	*	FL	1800	434.9	6.0	28.0

III. RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (M)		
		X	Y	Z
1. P1-0	*	44486	18184	.0
2. P1-5	*	44486	18184	5.0
3. P1-10	*	44486	18184	10.0
4. P2-0	*	44486	18157	.0
5. P2-5	*	44486	18157	5.0
6. P2-10	*	44486	18157	10.0
7. P3-0	*	44676	18187	.0
8. P3-5	*	44676	18187	5.0
9. P3-10	*	44676	18187	10.0
10. P4-0	*	44676	18159	.0
11. P4-5	*	44676	18159	5.0
12. P4-10	*	44676	18159	10.0
13. P5-0	*	45010	18184	.0
14. P5-5	*	45010	18184	5.0
15. P5-10	*	45010	18184	10.0
16. P6-0	*	45010	18160	.0
17. P6-5	*	45010	18160	5.0
18. P6-10	*	45010	18160	10.0
19. P7-0	*	45123	18186	.0
20. P7-5	*	45123	18186	5.0
21. P7-10	*	45123	18186	10.0
22. P8-0	*	45125	18168	.0
23. P8-5	*	45125	18168	5.0
24. P8-10	*	45125	18168	10.0

IV. MODEL RESULTS (WORST CASE WIND ANGLE)

RECEPTOR	*	BRG (DEG)	PRED CONC (PPM)	CONC/LINK (PPM)							
				0	1	2	3	4	5	6	7
1. P1-0	*	249.	55.1	.0	.0	.0	.0	.0	.0	.0	.0
2. P1-5	*	241.	93.5	.0	.0	.0	.0	.0	.0	.0	.0
3. P1-10	*	251.	52.5	.0	.0	.0	.0	.0	.0	.0	.0
4. P2-0	*	283.	57.1	.0	.0	.0	.0	.0	.0	.0	.0
5. P2-5	*	289.	94.0	.0	.0	.0	.0	.0	.0	.0	.0
6. P2-10	*	284.	54.7	.0	.0	.0	.0	.0	.0	.0	.0
7. P3-0	*	114.	89.1	.0	.0	.0	.0	.0	.0	.0	.0
8. P3-5	*	105.	51.2	.0	.0	.0	.0	.0	.0	.0	.2
9. P3-10	*	98.	24.9	.0	.0	.0	.0	.0	.0	.0	.4
10. P4-0	*	71.	91.9	.0	.0	.0	.0	.0	.0	.0	.0
11. P4-5	*	78.	55.2	.0	.0	.0	.0	.0	.0	.0	.1
12. P4-10	*	92.	26.6	.0	.0	.0	.0	.0	.0	.0	.2
13. P5-0	*	261.	61.8	.0	.0	.0	.0	.0	.0	.0	.0
14. P5-5	*	264.	40.9	.0	.0	.0	.0	.0	.0	.0	.0
15. P5-10	*	265.	24.5	.0	.0	.0	.0	.0	.0	.0	.0
16. P6-0	*	282.	59.7	.0	.0	.0	.0	.0	.0	.0	.0
17. P6-5	*	278.	39.5	.0	.0	.0	.0	.0	.0	.0	.0
18. P6-10	*	276.	24.0	.0	.0	.0	.0	.0	.0	.0	.0
19. P7-0	*	75.	23.0	.0	.0	.0	.0	.0	.0	.0	1.3
20. P7-5	*	84.	52.9	.0	.0	.0	.0	.0	.0	.0	1.8
21. P7-10	*	76.	34.5	.0	.0	.0	.0	.0	.0	.0	1.2
22. P8-0	*	54.	24.8	.0	.0	.0	.0	.0	.0	.0	1.1
23. P8-5	*	52.	50.6	.0	.0	.0	.0	.0	.0	.0	.9
24. P8-10	*	53.	35.1	.0	.0	.0	.0	.0	.0	.0	.9

