

Appendix 3-12

Sensitivity Test on Vehicular Emissions Due to Traffic Generated by this Project

Appendix 3-12 Vehicular Emissions Due to Traffic Generated by the Development

1.0 Introduction

The proposed development has incorporated adequate setback distance from nearby roads so that adverse air quality impact upon the development site due to vehicular emissions from nearby road networks, is not anticipated.

During operation of the proposed development, there will be additional traffic generated as a result, which may potentially affect other nearby existing/ planned ASRs although it is expected that the increase in traffic flow due to this Project will arise insignificant impact given the small scale of this Project (32 houses).

There are existing ASRs in adjacent to the existing roads such as existing Helene Terrace, Fairview Park and village houses. These ASRs are also adequately setback from the nearby road by the existing planting area/ slope along the edge of Yau Pok Road and Kam Pok Road. Thus, they should not be adversely affected by vehicular emissions as well.

A sensitivity test on vehicular emissions upon nearby roads as a result of the traffic generated by this Project, has been undertaken. The purpose of this test is to provide information that the concerned increase in traffic flow due to this Project will not worsen the air quality or has any adverse impact on nearby ASRs.

2.0 Selection of Representative ASRs

ASRs that have been identified for construction phase air quality assessment of this Project, are also selected for vehicular emissions impact assessment with due consideration of worst affected locations near the road edge. The locations of selected ASRs for vehicular emissions impact assessment are presented in Figure 1 below.

3.0 Methodology

3.1 Air Dispersion Model

The pollutants levels at the ASRs due to vehicular emission were calculated by the dispersion model "CALINE4". The hourly concentrations of pollutants concerned at the representative ASRs have been predicted. The modelled hourly concentrations have been converted to daily average concentration by taking the average value of 24 hours in a day. Similarly, the annual concentration has been determined by taking the average value of 8760 hours in a year.

In order to represent a worst case scenario, it is assumed that all the road segments are located on the same elevation level (i.e. at-grade level) in the model.

3.2 Parameters

Traffic emission would consist of major pollutants including RSP, FSP, NO₂ and CO.

Sulphur dioxide is mainly generated by chimney emission and other local emission sources like open road traffic emission would have little contribution. SO₂ emission from chimney stack is not a concern for the Project due to absence of industrial chimney nearby (see Section 3.6.2.1 of EIA report), thus no further study is considered necessary.

Ozone is not a primary pollutant emitted from man-made sources but is formed by a set of complex chain reactions between various chemical species, including NO_x and VOC, in the presence of sunlight. Therefore, O₃ recorded locally can be attributed to emission generated from places afar. O₃ concentration is highly influenced by regional sources instead of local emission sources. Thus, no further study is considered necessary.

Carbon monoxide is one of the primary pollutants emitted by road transport. Based on the statistics of emission inventory for 2013, road transport emission contributes 59% of CO emission. According to the highest hourly concentrations measured in 2014 at EPD's monitoring stations, highest hourly CO concentration is 3590µg/m³ at Central station in urban area nearby road carriageway and is still well below the acceptable standard. On the other hand, CO is used to be considered a less critical parameter due to its more relaxed standard and non-excessive emission in relation to open road traffic. Should the predicted NO₂, FSP and RSP concentration comply with relevant standard, no exceedance of CO concentration standard is anticipated.

Leaded petrol had been banned in Hong Kong since 1999 and is no longer considered a primary source in Hong Kong. Chimney emission may generate small amount of Pb emission. Owing to the absence of industrial chimney nearby, lead emission impact is not considered significant.

Having discussed above, RSP, FSP and NO₂ are focused in this study for assessment of air quality impact due to local emission sources (traffic emission).

3.3 Predicted Traffic Flow Generated/ Attracted by this Project

According to the traffic consultant of this Project, traffic generated from this Project will make use of a section of nearby existing Kam Pok Road as the vehicular access. Vehicles arriving at the Project Site will make use of Kam Pok Road through Castle Peak Road. On the other hand, vehicles leaving the Project Site may either go north to Castle Peak Road or go south to Fairview Park Boulevard. Other existing roads such as Castle Peak Road, San Tin Highway and Fairview Park Boulevard are further away and the amount of traffic concerned due to this Project, will be negligible when compared with the road traffic travelling on these roads. Since this Project will arise more impacts on the section of Kam Pok Road immediately adjacent to the Project Site, these sections of roads are assessed further. Please refer to Figure 1 for the existing road segments concerned in this vehicular emission assessment.

Information of traffic flow generated by this Project is provided by the traffic consultant. According to the provided information, this Project will likely to generate 18 vehicles/ hour during the AM Peak hour and 19 vehicles/ hour during the PM peak hour, respectively. The compositions of traffic flow will mainly be private cars from the development site as well as heavy vehicles such as school mini-buses and refuse collection vehicle. Given such small number of traffic generated by this Project and that a majority of the concerned vehicles will be private cars only, it is unlikely that it will adversely affect any nearby ASRs.

3.4 Fleet Average Emission Factors

The emission model EMFAC-HK was adopted to calculate the vehicle emission factors of NO₂ and RSP. The following details the input assumptions of the model.

3.4.1 Methodology of EMFAC-HK Modeling

Objective

The aim of conducting EMFAC Model is to calculate project-specific vehicle emission factor of criteria air pollutants (e.g. NO₂ and RSP) arising from vehicular tailpipe emission on the road carriageways of the proposed development.

EMFAC-HK Model

The EMFAC-HK Model version 2.6 dated 2 Jan 2014 (the EMFAC-HK Model), which was the latest available version, was adopted.

Guideline and Document

Several guidelines and documents published by the EPD, which are available from the following EPD EMFAC-HK website (the EPD website), are referred for EMFAC-HK Model input:

- http://www.epd.gov.hk/epd/english/environmentinhk/air/guide_ref/emfac.html (the EPD website)
- Guideline on Modelling Vehicle Emissions (Revised on 2.1.2014) (the EPD Guideline)
- 2010 Licensed Vehicle by Age and Technology Group Fractions (the EPD Document)

3.4.2 Traffic Data

Predicted traffic data

Project specific peak hour traffic data generated by this Project during operational phase, is adopted in combination with emission factor based on EMFAC-HK Model (with calendar year set as 2017 (Section 3.4.3 refers), the project completion year) to estimate the highest vehicular emission rate for each roadway.

Predicted traffic flow generated/ attracted by this Project is provided in Section 3.3 above.

Traffic data adopted in EMFAC-HK Model

As a conservative approach, the PM peak hour traffic data is adopted in order to represent a worst case scenario (i.e. total 19 vehicles/ hour, which comprises 15 private cars, 3 school mini-buses and 1 refuse collection vehicle). Private cars were modelled as “Private Cars (PC)” in the EMFAC model, while school buses and refuse collection vehicle were modelled as “Private Light Bus (>3.5t) (PV5)” and “Heavy Goods Vehicles (>=15t) (HGV8)” in the EMFAC model, respectively. A listing of the EMFAC-HK vehicle classes is provided in Table 1 below.

It has also been assumed that the AM peak hour traffic flow and traffic composition would persist for 24 hours of a day and throughout the whole year (i.e. 8760 hours). Speed limit of 50 kph was adopted for 24 hours for the concerned roads.

As discussed above, traffic generated by this Project will use only a section of Kam Pok Road for access. Figure 1 shows the section of road carriageways that have been modelled.

Table 1 EMFAC-HK Vehicle Classes

Vehicle Class Description	Fuel Type	Gross Vehicle Weight (tonnes)	Symbol 1 (in csv output file)	Symbol 2 (in bcd output file & traffic data)
Private Cars (PC)	ALL	ALL	PC	PC
Taxi	ALL	ALL	Taxi	Taxi
Light Goods Vehicles (<=2.5t)	ALL	<=2.5t	LGV<=2.5t	LGV3
Light Goods Vehicles (2.5-3.5t)	ALL	>2.5-3.5t	LGV2.5-3.5t	LGV4
Light Goods Vehicles (3.5-5.5t)	ALL	>3.5-5.5t	LGV>3.5t	LGV6
Medium & Heavy Goods Vehicles (5.5-15t)	ALL	>5.5-15t	HGV<=15t	HGV7
Medium & Heavy Goods Vehicles (>=15t)	ALL	>15t	HGV>15t	HGV8
Public Light Buses	ALL	ALL	PLB	PLB
Private Light Buses (<=3.5t)	ALL	<=3.5t	PrLB<=3.5t	PV4
Private Light Buses (>3.5t)	ALL	>3.5t	PrLB>3.5t	PV5
Non-franchised Buses (<6.4t)	ALL	<=6.36t	NFB<=6.4t	NFB6
Non-franchised Buses (6.4-15t)	ALL	>6.36-15t	NFB6.4-15t	NFB7
Non-franchised Buses (>15t)	ALL	>15t	NFB>15t	NFB8
Single Deck Franchised Buses	ALL	ALL	FBSD	FBSD
Double Deck Franchised Buses	ALL	ALL	FBDD	FBDD
Motor Cycles	ALL	ALL	MC	MC

3.4.3 EMFAC-HK Input

Geographical Area.

“Hong Kong” is selected as the Geographical Area.

Calendar Year.

Year 2017 is chosen as the Calendar Year in EMFAC-HK Model, which is even more conservative than the Project completion year in 2018, to represent the worst case scenario emissions (because the vehicle fleet will become cleaner over time as the fleet incorporates newer vehicles adhering to more stringent emission standards).

Season or Month.

Per the EPD Guideline, “Annual” is selected in this study to evaluate the highest vehicle emission within the Model Year.

Mode and Output.

EMFAC-HK Model is run in EMFAC mode for calculating area fleet average emissions.

Temperature and Humidity.

Referring to 1-year weather data recorded at Hong Kong Observatory, the temperature ranges from 5.9°C to 33.8°C; relative humidity (RH) ranges from 21% to 100% (see Table 1 of Annex 1). For output configuration, temperature is set from 5°C to 35°C with increment of 5°C. RH is set from 20% to 100% with increment of 10%.

Speeds.

Speed limit of 50 kph was adopted.

Exhaust / Evaporation Technology Fractions.

Vehicle classes are grouped with different exhaust and evaporation technology group indexes and technology fractions. Each technology group represents a distinct emission control technologies. Default exhaust and evaporation technology fractions are adopted in this assessment.

Population and Accrual Rate.

Default vehicle populations forecast and accrual rate in EMFAC-HK Model is adopted.

Trips and VKT.

Default trips and VKT for HK total is adopted.

Detailed impact rates will be generated with respect to each combination of temperature, RH and speed for running exhaust emission, and combination of temperature and duration for cold start emission.

3.4.4 Calculation of Emission Factors by EMFAC-HK Model Output

RSP and FSP emission factors generated using EMFAC-HK model have been reviewed. It is observed that the magnitude of FSP emission factor for individual combination of vehicle class, temperature, relative humidity and speed amounts to about 80% to 95% of RSP emission factor. The percentage is lowest for MC and highest for “PC”. On average, FSP emission factor amounts to about 90% of RSP emission factor.

In this study, NO₂ and RSP emission factor generated using EMFAC-HK are adopted. The FSP concentration is determined by applying a multiplying factor of 0.9 to the predicted concentration

determined using RSP emission factor (note: it shall be noted that even the determined RSP level as shown in Annex 1 is adopted as FSP level, the contribution from FSP is still insignificant and is negligible).

Running Exhaust Emission Rate

To represent the worst case scenario, maximum running exhaust emission rate (g/km) among all combinations of temperature (5°C to 35°C) and humidity (20% to 100%) with respect to each combination of speed and vehicle class will be adopted for NO_x, RSP, RSP – Brake Wear & RSP – Tire Wear. Total RSP emission rate = RSP + RSP – Brake Wear + RSP – Tire Wear.

For each road group (i.e. roads with same speed limit), hourly running exhaust emission rate (NO_x/RSP) for each vehicle class is determined by:

Hourly running exhaust emission rate (NO_x/RSP) for each vehicle class (g/veh-km) = \sum [running exhaust emission rate for a particular speed x speed fraction of particular speed]

For each road, hourly composite running exhaust emission rate (NO_x/RSP) is determined by:

Hourly composite running exhaust emission rate (NO_x/RSP) (g/veh-km) = \sum [hourly running exhaust emission rate for each vehicle class (determined for the corresponding road group) x % composition of corresponding vehicle class]

Starting Emission Rate

For cold start emission which is applicable to non-trunk road only, maximum starting emission (g/trip) among different durations (from 5min to 720min) is adopted. It is notable that only 8 of 16 vehicle classes would have starting emission.

Reference is made to “Agreement No. CE 45/2008 (CE) Liantang / Heung Yuen Wai Boundary Control Point and Associated Works” (EIA-190/2010) (the Liantang EIA). In the EIA Report, correlation is established between number of trips and VMT/VKT. The estimated VMT/VKT for rural and local roads with possible cold start emission amounts to 13% of total VMT/VKT.

In this assessment, the assumption in Liantang EIA is followed. EMFAC Model is used to generate HK total number of trips and VKT travelled in Year 2017 for each vehicle class (Section 3.4.3 refers). Trip per VKT for rural and local road for each class is determined by:

Trip/VKT (1/veh-km) for each vehicle class = HK total number of trips for each vehicle class ÷ (HK total VKT travelled for each vehicle class x 13%).

Based on the hourly VKT travelled data from project traffic consultant, hourly total cold start emission (gram) for each vehicle class along each road is determined by:

Hourly total cold start emission (g) for each vehicle class = starting emission rate for each vehicle class x Trip/VKT for each vehicle class x VKT travelled for each vehicle class along each road

The hourly total cold start emission rate for each road is the sum of hourly total cold start emission (gram) for each vehicle class along the same road. The hourly composite cold start emission rate is calculated by dividing the value using the hourly traffic flow:

$$\text{Hourly total cold start emission (g)} = \sum [\text{hourly total cold start emission for each vehicle class}]$$

Hourly composite cold start emission rate (g/veh-km) = hourly total cold start emission ÷ hourly total VKT travelled.

3.4.5 Emission Factors Adopted for CALINE4 Modeling

Based on the methodology described above, hourly running exhaust emission rate and hourly cold start emission rate (applied to non-trunk road only) are determined for 24 hours. Annex 1 showed details of derivation of hourly composite running exhaust and cold start emission rates for CALINE4 modelling.

3.4.6 Meteorological Data

As discussed in 3.4.2 above, in order to represent a worst case scenario, it has also been assumed that the PM peak hour traffic flow and traffic composition would persist for 24 hours of a day and throughout the whole year (i.e. 8,760 hours), although this is very unlikely to occur. As such, the Caline4 was modelled using a worst case scenario.

Typical worst-case meteorological conditions were assumed as following:

- Wind direction: worst-case angle selected by model
- Wind speed: 1 m/s
- Directional Variability: 6°
- Stability Class: F
- Mixing Height: 500 m
- Temperature: 20 °C

3.4.7 NOx/NO₂ Conversion

Ozone limiting method has been adopted to convert the predicted NOx concentration due to local emission sources to NO₂ concentration. The formula adopted for conversion is:

$$[\text{NOx}]_p \times 7.5\% + \text{Min}(46/48 \times [\text{O3}]_a, [\text{NOx}]_p \times 92.5\%) \text{ where}$$

[NOx]_p = predicted NOx concentration due to local emission sources;
[O3]_a = background O3 concentration (from PATH model)

Note: tailpipe emission is assumed as 7.5% of NOx according to “Guidelines on Choice of Models and Model Parameters” published in EPD’s website; molecular mass of NO₂/O₃ is 46/48.

As a worst case scenario has been adopted using the AM peak hour traffic data, the highest hourly ozone level from the PATH output file was then adopted for the above conversation. The Project Site and the concerned roads are within grid(20,40) in the PATH system, thus PATH output file for grid(20,40) in year 2015 has been adopted to represent a worst case scenario.

According to the PATH output file for grid(20,40), the highest hourly ozone level is 285.4 $\mu\text{g}/\text{m}^3$ under 25°C. The said ozone concentration was then adopted and converted to 20°C in the NO_x/NO₂ conversion.

3.4.8 CALINE4 Modeling Parameters

Calculation of Hourly Average Pollutant Concentration

The peak hour traffic flow and determined hourly composite emission rate is adopted, which was then applied to all 24 hours (i.e. 24 sets of traffic flow and composite emission rate adopted in the modeling data file (see Table 5 of Annex 1).

The results of worst case scenario modelled, were then applied to every hour of a year. The average value of these results is taken as the annual average concentration. The average value of every 24 hours of result (from hour 1 (00:00-01:00) to 24 (23:00-00:00)) is taken as daily average concentration.

To determine maximum hourly and daily concentration, the maximum value among hourly and calculated daily concentration values are taken.

3.5 Assessment Results

According to the assessment results, the predicted RSP and FSP, NO₂ concentrations were very small, which is considered insignificant and will not have adverse impact on the ASRs. Details of the assessment results are provided in Annex 2.

As discussed above, the current assessment has been based on a very conservative approach by adopting air pollutants level generated from the peak hour under a worst wind angle and meteorological conditions, and assuming that the pollutants would persist for 24 hours of a day and throughout the whole year. In reality, the traffic flow during most time of the day during non-peak hours would be much smaller, thus it is expected that the actual air pollutants concentrations generated by the traffic of this Project would be much smaller than the above predicted results.

As such, it is concluded that vehicular emissions on nearby roads due to increased traffic flow generated by this Project, will not worsen the air quality at nearby ASRs and will not result in any adverse air quality impact.

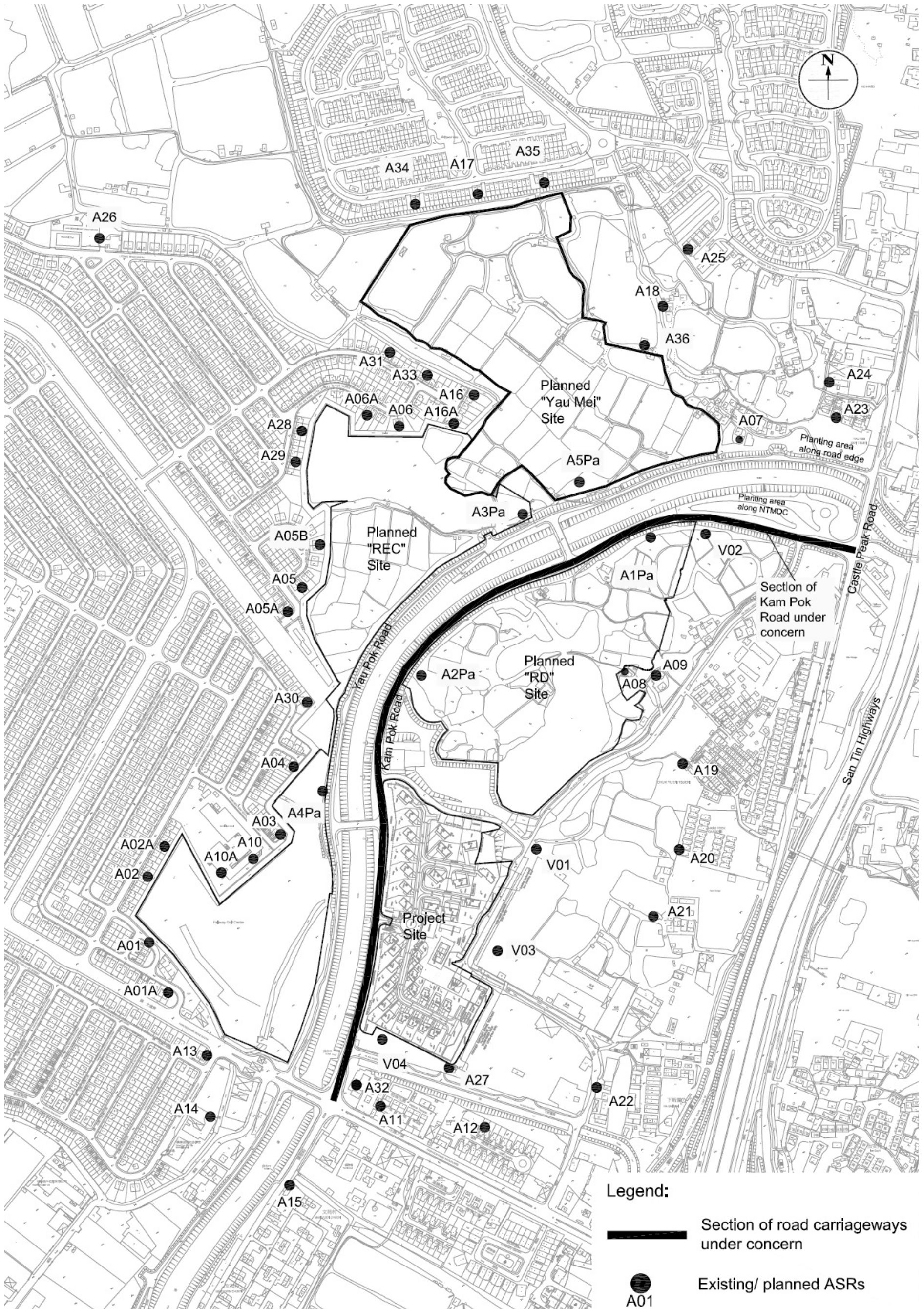


Figure 1 Locations of Representative ASRs Selected for Vehicular Emissions Impact Assessment

Annex 1

of Appendix 3-12

(Details of Determination of Running Exhaust and Starting
Emission Rate)

Table 2: Running emission for combination of speed and vehicle class (g/km) & starting emission for each vehicle class (g/trip) for Year 2017

Emission Type	pollutant	SF/time	PC	Taxi	LGV3	LGV4	LGV6	HGV7	HGV8	PLB	PV4	PV5	NFB6	NFB7	NFB8	FBSD	FBDD	MC
Running Exhaust	Nox	4	0.1368	1.1302	1.4375	1.7668	5.1672	6.7240	11.7780	1.9443	0.4191	1.8933	5.3738	10.9408	17.3785	17.1708	17.9786	0.8125
Running Exhaust	Nox	12	0.1153	0.9832	1.0982	1.4377	4.3758	5.6589	9.8852	1.8139	0.3603	1.7051	4.5900	9.3369	14.8268	14.5065	15.1006	0.7439
Running Exhaust	Nox	20	0.0995	0.8686	0.9128	1.2137	3.1537	4.0313	7.0060	1.6311	0.3157	1.4144	3.3604	6.8250	10.8325	10.4090	10.7173	0.6931
Running Exhaust	Nox	28	0.0878	0.7796	0.7915	1.0614	2.4394	3.1104	5.3996	1.5565	0.2819	1.2444	2.6080	5.2951	8.4034	8.0439	8.2624	0.6563
Running Exhaust	Nox	36	0.0792	0.7108	0.7139	0.9615	2.1914	2.8208	4.9174	1.5748	0.2564	1.1914	2.3134	4.7029	7.4665	7.2521	7.5160	0.6306
Running Exhaust	Nox	44	0.0730	0.6585	0.6706	0.9023	2.0455	2.6560	4.6478	1.6087	0.2377	1.1687	2.1337	4.3429	6.8976	6.7916	7.0966	0.6139
Running Exhaust	Nox	52	0.0688	0.6197	0.6563	0.8774	1.9272	2.5237	4.4326	1.6463	0.2245	1.1547	1.9867	4.0484	6.4324	6.4196	6.7611	0.6047
Running Exhaust	Nox	60	0.0661	0.5925	0.6691	0.8840	1.8366	2.4239	4.2715	1.6876	0.2161	1.1493	1.8722	3.8196	6.0711	6.1361	6.5097	0.6019
Running Exhaust	Nox	68	0.0650	0.5755	0.7090	0.9228	1.7736	2.3566	4.1648	1.7326	0.2120	1.1526	1.7904	3.6564	5.8135	5.9410	6.3421	0.6047
Running Exhaust	Nox	76	0.0652	0.5679	0.7787	0.9978	1.7382	2.3217	4.1124	1.7813	0.2121	1.1645	1.7412	3.5587	5.6596	5.8344	6.2585	0.6126
Running Exhaust	Nox	84	0.0668	0.5694	0.8835	1.1174	1.7305	2.3194	4.1142	1.8338	0.2167	1.1850	1.7245	3.5266	5.6096	5.8163	6.2589	0.6255
Running Exhaust	Nox	92	0.0701	0.5799	1.0324	1.2956	1.7504	2.3496	4.1704	1.8900	0.2261	1.2143	1.7405	3.5601	5.6633	5.8867	6.3432	0.6433
Running Exhaust	Nox	100	0.0752	0.6001	1.2402	1.5552	1.7980	2.4123	4.2808	1.9499	0.2413	1.2521	1.7891	3.6592	5.8207	6.0455	6.5115	0.6662
Running Exhaust	PM10-total	4	0.0182	0.0000	0.0508	0.1141	0.1555	0.4600	0.7058	0.2866	0.0501	0.0844	0.3116	0.5452	0.8919	0.1026	0.1685	0.0391
Running Exhaust	PM10-total	12	0.0116	0.0000	0.0380	0.0883	0.1302	0.3774	0.5821	0.2378	0.0341	0.0739	0.2718	0.4774	0.7497	0.0899	0.1438	0.0267
Running Exhaust	PM10-total	20	0.0078	0.0000	0.0300	0.0701	0.0885	0.2422	0.3791	0.1576	0.0244	0.0562	0.2049	0.3633	0.5150	0.0684	0.1027	0.0192
Running Exhaust	PM10-total	28	0.0055	0.0000	0.0243	0.0569	0.0595	0.1496	0.2397	0.1022	0.0182	0.0433	0.1564	0.2801	0.3512	0.0528	0.0736	0.0144
Running Exhaust	PM10-total	36	0.0041	0.0000	0.0202	0.0472	0.0478	0.1128	0.1840	0.0800	0.0142	0.0377	0.1356	0.2442	0.2845	0.0460	0.0615	0.0113
Running Exhaust	PM10-total	44	0.0032	0.0000	0.0172	0.0401	0.0416	0.0925	0.1537	0.0681	0.0116	0.0353	0.1264	0.2285	0.2501	0.0431	0.0556	0.0094
Running Exhaust	PM10-total	52	0.0026	0.0000	0.0149	0.0348	0.0379	0.0785	0.1333	0.0604	0.0098	0.0345	0.1233	0.2238	0.2301	0.0422	0.0526	0.0081
Running Exhaust	PM10-total	60	0.0023	0.0000	0.0132	0.0308	0.0367	0.0707	0.1229	0.0569	0.0086	0.0355	0.1263	0.2302	0.2242	0.0434	0.0526	0.0073
Running Exhaust	PM10-total	68	0.0021	0.0000	0.0119	0.0279	0.0378	0.0691	0.1223	0.0576	0.0078	0.0381	0.1356	0.2475	0.2326	0.0467	0.0556	0.0070
Running Exhaust	PM10-total	76	0.0020	0.0000	0.0110	0.0258	0.0414	0.0737	0.1317	0.0625	0.0073	0.0425	0.1510	0.2759	0.2552	0.0520	0.0614	0.0069
Running Exhaust	PM10-total	84	0.0020	0.0000	0.0104	0.0244	0.0473	0.0845	0.1510	0.0715	0.0072	0.0486	0.1725	0.3153	0.2920	0.0595	0.0702	0.0072
Running Exhaust	PM10-total	92	0.0022	0.0000	0.0102	0.0236	0.0557	0.1016	0.1801	0.0848	0.0073	0.0563	0.2003	0.3657	0.3430	0.0690	0.0820	0.0079
Running Exhaust	PM10-total	100	0.0024	0.0000	0.0104	0.0233	0.0666	0.1249	0.2192	0.1023	0.0078	0.0658	0.2342	0.4271	0.4083	0.0805	0.0967	0.0090
Starting emission	Nox	all	0.2162	1.8827	0.5147	0.0421	0	0	0	6.5637	0.3515	3.5091	0	0	0	0	0	0.4287
Starting emission	PM10-total	all	0.0046	0	0.0015	0.0006	0	0	0	0	0.0102	0.0001	0	0	0	0	0	0.0209

Note: running & starting emission based on highest value within temperature range of 5-35 °C and RH of 20-100% based on annual meteorological data; starting emisison based on highest value among different durations before cold start

Emission factor generated using EMFAC mode for Year 2017

Table 4: Summary of trip and VKT per day for vehicle class with starting emission in Year 2017

Model Year 2036	PC	Taxi	LGV3	LGV4	PLB	PV4	PV5	MC
Trip per day (HK total)	718122	72957	4653	177430	17392	6886	5727	269139
VKT per day (HK total)	13069820	6910043	107266	3382551	1200452	161856	134832	908215
VKT for rural & local road per day	1699076.6	898305.59	13944.58	439731.63	156058.76	21041.28	17528.16	118067.95
Trip/VKT for rural & local road	0.42265428	0.0812162	0.333678	0.4034961	0.1114452	0.327261	0.326731	2.2795263

Note: VKT for rural & local road per day = 13% of VKT per day (HK total) based on Liantang EIA

Table 5: Hourly composite emission rate for each road link

Road No.	Speed Limit	Hour	Total Vehicle	Nox-running (g/km)	Nox-starting (g/km)	Nox emission (g/km)	Nox emission (g/mile)	RSP-running (g/km)	RSP-starting (g/km)	RSP emission (g/km)	RSP emission (g/mile)	Nox (g)	RSP (g)	Nox emission x 10000 (g/mile)	RSP emission x 100 (g/mile)
1A	50	00:00-01:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.552123349	14614.319	4.081
1A	50	01:00-02:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	02:00-03:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	03:00-04:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	04:00-05:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	05:00-06:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	06:00-07:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	07:00-08:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	08:00-09:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	09:00-10:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	10:00-11:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	11:00-12:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	12:00-13:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	13:00-14:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	14:00-15:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	15:00-16:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	16:00-17:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	17:00-18:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	18:00-19:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	19:00-20:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	20:00-21:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	21:00-22:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	22:00-23:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081
1A	50	23:00-24:00	19	0.777665	0.13042894	0.90809394	1.46143190	0.023800	0.001557001	0.025357001	0.040808037	19.77283745	0.55212335	14614.319	4.081

Annex 2

Of Appendix 3-12

(Predicted RSP, FSP and NO₂ Concentrations at Discrete ASRs)

Annex 2-1 Summary Table of RSP Concentration Due to Traffic Generated by this Project

ASR ID	Height, m	Project Contribution, $\mu\text{g}/\text{m}^3$		
		Highest 24-h average *	10th highest 24-h average *	Annual average *
A01	1.5	0.031	0.031	0.031
A01A	1.5	0.029	0.029	0.029
A02	1.5	0.035	0.035	0.035
A02A	1.5	0.038	0.038	0.038
A03	1.5	0.047	0.047	0.047
A04	1.5	0.058	0.058	0.058
A05	1.5	0.037	0.037	0.037
A05A	1.5	0.041	0.041	0.041
A05B	1.5	0.032	0.032	0.032
A06	1.5	0.047	0.047	0.047
A06A	1.5	0.039	0.039	0.039
A07	1.5	0.054	0.054	0.054
A08	1.5	0.014	0.014	0.014
A09	1.5	0.012	0.012	0.012
A10	1.5	0.042	0.042	0.042
A10A	1.5	0.038	0.038	0.038
A11	1.5	0.062	0.062	0.062
A12	1.5	0.021	0.021	0.021
A13	1.5	0.027	0.027	0.027
A14	1.5	0.025	0.025	0.025
A15	1.5	0.061	0.061	0.061
A16	1.5	0.045	0.045	0.045
A16A	1.5	0.051	0.051	0.051
A17	1.5	0.028	0.028	0.028
A18	1.5	0.027	0.027	0.027
A19	1.5	0.01	0.01	0.01
A20	1.5	0.009	0.009	0.009
A21	1.5	0.009	0.009	0.009
A22	1.5	0.012	0.012	0.012
A23	1.5	0.055	0.055	0.055
A24	1.5	0.043	0.043	0.043
A25	1.5	0.025	0.025	0.025
A26	1.5	0.011	0.011	0.011
A27	1.5	0.028	0.028	0.028
A28	1.5	0.026	0.026	0.026
A29	1.5	0.025	0.025	0.025
A30	1.5	0.07	0.07	0.07
A31	1.5	0.037	0.037	0.037
A32	1.5	0.114	0.114	0.114
A33	1.5	0.044	0.044	0.044
A34	1.5	0.027	0.027	0.027
A35	1.5	0.028	0.028	0.028
A36	1.5	0.03	0.03	0.03
A1Pa	1.5	0.089	0.089	0.089
A2Pa	1.5	0.04	0.04	0.04
A3Pa	1.5	0.044	0.044	0.044
A4Pa	1.5	0.063	0.063	0.063
A5Pa	1.5	0.049	0.049	0.049
V01	1.5	0.015	0.015	0.015
V02	1.5	0.055	0.055	0.055
V03	1.5	0.016	0.016	0.016
V04	1.5	0.076	0.076	0.076
A01	4.5	0.03	0.03	0.03
A01A	4.5	0.028	0.028	0.028
A02	4.5	0.034	0.034	0.034
A02A	4.5	0.037	0.037	0.037
A03	4.5	0.045	0.045	0.045
A04	4.5	0.054	0.054	0.054
A05	4.5	0.036	0.036	0.036
A05A	4.5	0.04	0.04	0.04
A05B	4.5	0.031	0.031	0.031
A06	4.5	0.046	0.046	0.046
A06A	4.5	0.038	0.038	0.038
A07	4.5	0.051	0.051	0.051

Project Contribution, µg/m ³				
ASR ID	Height, m	Highest 24-h average *	10th highest 24-h average *	Annual average *
A08	4.5	0.013	0.013	0.013
A09	4.5	0.012	0.012	0.012
A10	4.5	0.04	0.04	0.04
A10A	4.5	0.037	0.037	0.037
A11	4.5	0.059	0.059	0.059
A12	4.5	0.02	0.02	0.02
A13	4.5	0.027	0.027	0.027
A14	4.5	0.025	0.025	0.025
A15	4.5	0.057	0.057	0.057
A16	4.5	0.044	0.044	0.044
A16A	4.5	0.049	0.049	0.049
A17	4.5	0.028	0.028	0.028
A18	4.5	0.027	0.027	0.027
A19	4.5	0.01	0.01	0.01
A20	4.5	0.009	0.009	0.009
A21	4.5	0.008	0.008	0.008
A22	4.5	0.011	0.011	0.011
A23	4.5	0.052	0.052	0.052
A24	4.5	0.042	0.042	0.042
A25	4.5	0.024	0.024	0.024
A26	4.5	0.011	0.011	0.011
A27	4.5	0.026	0.026	0.026
A28	4.5	0.025	0.025	0.025
A29	4.5	0.025	0.025	0.025
A30	4.5	0.066	0.066	0.066
A31	4.5	0.036	0.036	0.036
A32	4.5	0.104	0.104	0.104
A33	4.5	0.042	0.042	0.042
A34	4.5	0.026	0.026	0.026
A35	4.5	0.027	0.027	0.027
A36	4.5	0.029	0.029	0.029
A1Pa	4.5	0.078	0.078	0.078
A2Pa	4.5	0.034	0.034	0.034
A3Pa	4.5	0.041	0.041	0.041
A4Pa	4.5	0.058	0.058	0.058
A5Pa	4.5	0.046	0.046	0.046
V01	4.5	0.014	0.014	0.014
V02	4.5	0.048	0.048	0.048
V03	4.5	0.015	0.015	0.015
V04	4.5	0.07	0.07	0.07
A01	7.5	0.028	0.028	0.028
A01A	7.5	0.026	0.026	0.026
A02	7.5	0.032	0.032	0.032
A02A	7.5	0.035	0.035	0.035
A03	7.5	0.04	0.04	0.04
A04	7.5	0.048	0.048	0.048
A05	7.5	0.033	0.033	0.033
A05A	7.5	0.037	0.037	0.037
A05B	7.5	0.029	0.029	0.029
A06	7.5	0.043	0.043	0.043
A06A	7.5	0.036	0.036	0.036
A07	7.5	0.046	0.046	0.046
A08	7.5	0.012	0.012	0.012
A09	7.5	0.011	0.011	0.011
A10	7.5	0.036	0.036	0.036
A10A	7.5	0.034	0.034	0.034
A11	7.5	0.053	0.053	0.053
A12	7.5	0.019	0.019	0.019
A13	7.5	0.025	0.025	0.025
A14	7.5	0.023	0.023	0.023
A15	7.5	0.051	0.051	0.051
A16	7.5	0.041	0.041	0.041
A16A	7.5	0.046	0.046	0.046
A17	7.5	0.026	0.026	0.026
A18	7.5	0.025	0.025	0.025
A19	7.5	0.009	0.009	0.009
A20	7.5	0.008	0.008	0.008
A21	7.5	0.008	0.008	0.008

Project Contribution, µg/m ³				
ASR ID	Height, m	Highest 24-h average *	10th highest 24-h average *	Annual average *
A22	7.5	0.011	0.011	0.011
A23	7.5	0.048	0.048	0.048
A24	7.5	0.039	0.039	0.039
A25	7.5	0.023	0.023	0.023
A26	7.5	0.01	0.01	0.01
A27	7.5	0.024	0.024	0.024
A28	7.5	0.023	0.023	0.023
A29	7.5	0.023	0.023	0.023
A30	7.5	0.059	0.059	0.059
A31	7.5	0.034	0.034	0.034
A32	7.5	0.088	0.088	0.088
A33	7.5	0.04	0.04	0.04
A34	7.5	0.025	0.025	0.025
A35	7.5	0.026	0.026	0.026
A36	7.5	0.027	0.027	0.027
A1Pa	7.5	0.061	0.061	0.061
A2Pa	7.5	0.03	0.03	0.03
A3Pa	7.5	0.035	0.035	0.035
A4Pa	7.5	0.049	0.049	0.049
A5Pa	7.5	0.041	0.041	0.041
V01	7.5	0.013	0.013	0.013
V02	7.5	0.036	0.036	0.036
V03	7.5	0.014	0.014	0.014
V04	7.5	0.061	0.061	0.061
Range		0.008 - 0.114	0.008 - 0.114	0.008 - 0.114
Max.		0.114	0.114	0.114
AQO Criteria		-	100	50

Remark: * Estimated based on the worst case meteorological condition, wind speed, and wind angle taking account the peak hour traffic flow generated and attracted by this Project. As a conservative approach, it has been assumed that the estimated pollutant concentration during the peak hour would persist for 8760 hours of a year when calculating the daily and annual concentrations. This is considered very conservative and is unlikely to occur. In reality, the traffic flow during most time of the day during non-peak hours would be much smaller, thus it is expected that the actual air pollutants concentrations generated by the traffic of this Project would be much smaller than the above predicted results

Annex 2-2 Summary Table of FSP Concentration Due to Traffic Generated by this Project

ASR ID	Height, m	Project Contribution, $\mu\text{g}/\text{m}^3$		
		Highest 24-h average * & **	10th highest 24-h average	Annual average * & **
A01	1.5	0.028	0.028	0.028
A01A	1.5	0.026	0.026	0.026
A02	1.5	0.032	0.032	0.032
A02A	1.5	0.034	0.034	0.034
A03	1.5	0.042	0.042	0.042
A04	1.5	0.052	0.052	0.052
A05	1.5	0.033	0.033	0.033
A05A	1.5	0.037	0.037	0.037
A05B	1.5	0.029	0.029	0.029
A06	1.5	0.042	0.042	0.042
A06A	1.5	0.035	0.035	0.035
A07	1.5	0.049	0.049	0.049
A08	1.5	0.013	0.013	0.013
A09	1.5	0.011	0.011	0.011
A10	1.5	0.038	0.038	0.038
A10A	1.5	0.034	0.034	0.034
A11	1.5	0.056	0.056	0.056
A12	1.5	0.019	0.019	0.019
A13	1.5	0.024	0.024	0.024
A14	1.5	0.023	0.023	0.023
A15	1.5	0.055	0.055	0.055
A16	1.5	0.041	0.041	0.041
A16A	1.5	0.046	0.046	0.046
A17	1.5	0.025	0.025	0.025
A18	1.5	0.024	0.024	0.024
A19	1.5	0.009	0.009	0.009
A20	1.5	0.008	0.008	0.008
A21	1.5	0.008	0.008	0.008
A22	1.5	0.011	0.011	0.011
A23	1.5	0.050	0.050	0.050
A24	1.5	0.039	0.039	0.039
A25	1.5	0.023	0.023	0.023
A26	1.5	0.010	0.010	0.010
A27	1.5	0.025	0.025	0.025
A28	1.5	0.023	0.023	0.023
A29	1.5	0.023	0.023	0.023
A30	1.5	0.063	0.063	0.063
A31	1.5	0.033	0.033	0.033
A32	1.5	0.103	0.103	0.103
A33	1.5	0.040	0.040	0.040
A34	1.5	0.024	0.024	0.024
A35	1.5	0.025	0.025	0.025
A36	1.5	0.027	0.027	0.027
A1Pa	1.5	0.080	0.080	0.080
A2Pa	1.5	0.036	0.036	0.036
A3Pa	1.5	0.040	0.040	0.040
A4Pa	1.5	0.057	0.057	0.057
A5Pa	1.5	0.044	0.044	0.044
V01	1.5	0.014	0.014	0.014
V02	1.5	0.050	0.050	0.050
V03	1.5	0.014	0.014	0.014
V04	1.5	0.068	0.068	0.068
A01	4.5	0.027	0.027	0.027
A01A	4.5	0.025	0.025	0.025
A02	4.5	0.031	0.031	0.031
A02A	4.5	0.033	0.033	0.033
A03	4.5	0.041	0.041	0.041
A04	4.5	0.049	0.049	0.049
A05	4.5	0.032	0.032	0.032
A05A	4.5	0.036	0.036	0.036
A05B	4.5	0.028	0.028	0.028
A06	4.5	0.041	0.041	0.041
A06A	4.5	0.034	0.034	0.034
A07	4.5	0.046	0.046	0.046

ASR ID	Height, m	Project Contribution, µg/m ³		
		Highest 24-h average * & **	10th highest 24-h average	Annual average * & **
A08	4.5	0.012	0.012	0.012
A09	4.5	0.011	0.011	0.011
A10	4.5	0.036	0.036	0.036
A10A	4.5	0.033	0.033	0.033
A11	4.5	0.053	0.053	0.053
A12	4.5	0.018	0.018	0.018
A13	4.5	0.024	0.024	0.024
A14	4.5	0.023	0.023	0.023
A15	4.5	0.051	0.051	0.051
A16	4.5	0.040	0.040	0.040
A16A	4.5	0.044	0.044	0.044
A17	4.5	0.025	0.025	0.025
A18	4.5	0.024	0.024	0.024
A19	4.5	0.009	0.009	0.009
A20	4.5	0.008	0.008	0.008
A21	4.5	0.007	0.007	0.007
A22	4.5	0.010	0.010	0.010
A23	4.5	0.047	0.047	0.047
A24	4.5	0.038	0.038	0.038
A25	4.5	0.022	0.022	0.022
A26	4.5	0.010	0.010	0.010
A27	4.5	0.023	0.023	0.023
A28	4.5	0.023	0.023	0.023
A29	4.5	0.023	0.023	0.023
A30	4.5	0.059	0.059	0.059
A31	4.5	0.032	0.032	0.032
A32	4.5	0.094	0.094	0.094
A33	4.5	0.038	0.038	0.038
A34	4.5	0.023	0.023	0.023
A35	4.5	0.024	0.024	0.024
A36	4.5	0.026	0.026	0.026
A1Pa	4.5	0.070	0.070	0.070
A2Pa	4.5	0.031	0.031	0.031
A3Pa	4.5	0.037	0.037	0.037
A4Pa	4.5	0.052	0.052	0.052
A5Pa	4.5	0.041	0.041	0.041
V01	4.5	0.013	0.013	0.013
V02	4.5	0.043	0.043	0.043
V03	4.5	0.014	0.014	0.014
V04	4.5	0.063	0.063	0.063
A01	7.5	0.025	0.025	0.025
A01A	7.5	0.023	0.023	0.023
A02	7.5	0.029	0.029	0.029
A02A	7.5	0.032	0.032	0.032
A03	7.5	0.036	0.036	0.036
A04	7.5	0.043	0.043	0.043
A05	7.5	0.030	0.030	0.030
A05A	7.5	0.033	0.033	0.033
A05B	7.5	0.026	0.026	0.026
A06	7.5	0.039	0.039	0.039
A06A	7.5	0.032	0.032	0.032
A07	7.5	0.041	0.041	0.041
A08	7.5	0.011	0.011	0.011
A09	7.5	0.010	0.010	0.010
A10	7.5	0.032	0.032	0.032
A10A	7.5	0.031	0.031	0.031
A11	7.5	0.048	0.048	0.048
A12	7.5	0.017	0.017	0.017
A13	7.5	0.023	0.023	0.023
A14	7.5	0.021	0.021	0.021
A15	7.5	0.046	0.046	0.046
A16	7.5	0.037	0.037	0.037
A16A	7.5	0.041	0.041	0.041
A17	7.5	0.023	0.023	0.023
A18	7.5	0.023	0.023	0.023
A19	7.5	0.008	0.008	0.008
A20	7.5	0.007	0.007	0.007

		Project Contribution, µg/m ³		
ASR ID	Height, m	Highest 24-h average * & **	10th highest 24-h average	Annual average * & **
A21	7.5	0.007	0.007	0.007
A22	7.5	0.010	0.010	0.010
A23	7.5	0.043	0.043	0.043
A24	7.5	0.035	0.035	0.035
A25	7.5	0.021	0.021	0.021
A26	7.5	0.009	0.009	0.009
A27	7.5	0.022	0.022	0.022
A28	7.5	0.021	0.021	0.021
A29	7.5	0.021	0.021	0.021
A30	7.5	0.053	0.053	0.053
A31	7.5	0.031	0.031	0.031
A32	7.5	0.079	0.079	0.079
A33	7.5	0.036	0.036	0.036
A34	7.5	0.023	0.023	0.023
A35	7.5	0.023	0.023	0.023
A36	7.5	0.024	0.024	0.024
A1Pa	7.5	0.055	0.055	0.055
A2Pa	7.5	0.027	0.027	0.027
A3Pa	7.5	0.032	0.032	0.032
A4Pa	7.5	0.044	0.044	0.044
A5Pa	7.5	0.037	0.037	0.037
V01	7.5	0.012	0.012	0.012
V02	7.5	0.032	0.032	0.032
V03	7.5	0.013	0.013	0.013
V04	7.5	0.055	0.055	0.055
Range		0.007 - 0.103	0.007 - 0.103	0.007 - 0.103
Max.		0.103	0.103	0.103
AQO Criteria		-	75	35

Remark: * Estimated based on the worst case meteorological condition, wind speed, and wind angle taking account the peak hour traffic flow generated and attracted by this Project. As a conservative approach, it has been assumed that the estimated pollutant concentration during the peak hour would persist for 8760 hours of a year when calculating the daily and annual concentrations. This is considered very conservative and is unlikely to occur. In reality, the traffic flow during most time of the day during non-peak hours would be much smaller, thus it is expected that the actual air pollutants concentrations generated by the traffic of this Project would be much smaller than the above predicted results

** The FSP concentration is calculated by multiply a ratio of 90% of the estimated RSP level. It shall be noted that even the determined RSP level is adopted as FSP level, the contribution of FSP is still insignificant and negligible.

Annex 2-3 Summary Table of NO₂ Concentration Due to Traffic Generated by this Project

ASR ID	Height, m	Project Contribution, µg/m ³		
		Highest 1-h average NOx *	19th highest 1-h average NOx *	Annual average NOx *
A01	1.5	1.12	1.12	1.12
A01A	1.5	1.04	1.04	1.04
A02	1.5	1.25	1.25	1.25
A02A	1.5	1.37	1.37	1.37
A03	1.5	1.69	1.69	1.69
A04	1.5	2.06	2.06	2.06
A05	1.5	1.32	1.32	1.32
A05A	1.5	1.48	1.48	1.48
A05B	1.5	1.15	1.15	1.15
A06	1.5	1.7	1.7	1.7
A06A	1.5	1.4	1.4	1.4
A07	1.5	1.93	1.93	1.93
A08	1.5	0.49	0.49	0.49
A09	1.5	0.42	0.42	0.42
A10	1.5	1.5	1.5	1.5
A10A	1.5	1.37	1.37	1.37
A11	1.5	2.22	2.22	2.22
A12	1.5	0.75	0.75	0.75
A13	1.5	0.99	0.99	0.99
A14	1.5	0.91	0.91	0.91
A15	1.5	2.18	2.18	2.18
A16	1.5	1.61	1.61	1.61
A16A	1.5	1.8	1.8	1.8
A17	1.5	1.01	1.01	1.01
A18	1.5	0.99	0.99	0.99
A19	1.5	0.36	0.36	0.36
A20	1.5	0.32	0.32	0.32
A21	1.5	0.31	0.31	0.31
A22	1.5	0.43	0.43	0.43
A23	1.5	1.96	1.96	1.96
A24	1.5	1.54	1.54	1.54
A25	1.5	0.89	0.89	0.89
A26	1.5	0.39	0.39	0.39
A27	1.5	0.99	0.99	0.99
A28	1.5	0.92	0.92	0.92
A29	1.5	0.91	0.91	0.91
A30	1.5	2.5	2.5	2.5
A31	1.5	1.34	1.34	1.34
A32	1.5	4.09	4.09	4.09
A33	1.5	1.56	1.56	1.56
A34	1.5	0.96	0.96	0.96
A35	1.5	1	1	1
A36	1.5	1.06	1.06	1.06
A1Pa	1.5	3.18	3.18	3.18
A2Pa	1.5	1.44	1.44	1.44
A3Pa	1.5	1.58	1.58	1.58
A4Pa	1.5	2.26	2.26	2.26
A5Pa	1.5	1.76	1.76	1.76
V01	1.5	0.54	0.54	0.54
V02	1.5	1.98	1.98	1.98
V03	1.5	0.6	0.6	0.6
V04	1.5	2.71	2.71	2.71
A01	4.5	1.08	1.08	1.08
A01A	4.5	1.01	1.01	1.01
A02	4.5	1.22	1.22	1.22
A02A	4.5	1.34	1.34	1.34
A03	4.5	1.6	1.6	1.6
A04	4.5	1.93	1.93	1.93
A05	4.5	1.27	1.27	1.27
A05A	4.5	1.43	1.43	1.43
A05B	4.5	1.12	1.12	1.12
A06	4.5	1.65	1.65	1.65
A06A	4.5	1.36	1.36	1.36
A07	4.5	1.83	1.83	1.83

Project Contribution, $\mu\text{g}/\text{m}^3$				
ASR ID	Height, m	Highest 1-h average NOx *	19th highest 1-h average NOx *	Annual average NOx *
A08	4.5	0.48	0.48	0.48
A09	4.5	0.42	0.42	0.42
A10	4.5	1.43	1.43	1.43
A10A	4.5	1.32	1.32	1.32
A11	4.5	2.1	2.1	2.1
A12	4.5	0.73	0.73	0.73
A13	4.5	0.96	0.96	0.96
A14	4.5	0.88	0.88	0.88
A15	4.5	2.05	2.05	2.05
A16	4.5	1.56	1.56	1.56
A16A	4.5	1.75	1.75	1.75
A17	4.5	0.99	0.99	0.99
A18	4.5	0.96	0.96	0.96
A19	4.5	0.35	0.35	0.35
A20	4.5	0.32	0.32	0.32
A21	4.5	0.3	0.3	0.3
A22	4.5	0.4	0.4	0.4
A23	4.5	1.88	1.88	1.88
A24	4.5	1.49	1.49	1.49
A25	4.5	0.87	0.87	0.87
A26	4.5	0.38	0.38	0.38
A27	4.5	0.95	0.95	0.95
A28	4.5	0.89	0.89	0.89
A29	4.5	0.88	0.88	0.88
A30	4.5	2.36	2.36	2.36
A31	4.5	1.3	1.3	1.3
A32	4.5	3.74	3.74	3.74
A33	4.5	1.52	1.52	1.52
A34	4.5	0.95	0.95	0.95
A35	4.5	0.97	0.97	0.97
A36	4.5	1.04	1.04	1.04
A1Pa	4.5	2.8	2.8	2.8
A2Pa	4.5	1.21	1.21	1.21
A3Pa	4.5	1.47	1.47	1.47
A4Pa	4.5	2.08	2.08	2.08
A5Pa	4.5	1.66	1.66	1.66
V01	4.5	0.52	0.52	0.52
V02	4.5	1.71	1.71	1.71
V03	4.5	0.56	0.56	0.56
V04	4.5	2.52	2.52	2.52
A01	7.5	1.02	1.02	1.02
A01A	7.5	0.95	0.95	0.95
A02	7.5	1.14	1.14	1.14
A02A	7.5	1.25	1.25	1.25
A03	7.5	1.43	1.43	1.43
A04	7.5	1.71	1.71	1.71
A05	7.5	1.18	1.18	1.18
A05A	7.5	1.32	1.32	1.32
A05B	7.5	1.05	1.05	1.05
A06	7.5	1.54	1.54	1.54
A06A	7.5	1.27	1.27	1.27
A07	7.5	1.65	1.65	1.65
A08	7.5	0.44	0.44	0.44
A09	7.5	0.4	0.4	0.4
A10	7.5	1.3	1.3	1.3
A10A	7.5	1.22	1.22	1.22
A11	7.5	1.89	1.89	1.89
A12	7.5	0.67	0.67	0.67
A13	7.5	0.89	0.89	0.89
A14	7.5	0.83	0.83	0.83
A15	7.5	1.82	1.82	1.82
A16	7.5	1.47	1.47	1.47
A16A	7.5	1.63	1.63	1.63
A17	7.5	0.95	0.95	0.95
A18	7.5	0.89	0.89	0.89
A19	7.5	0.32	0.32	0.32
A20	7.5	0.3	0.3	0.3

Project Contribution, µg/m ³				
ASR ID	Height, m	Highest 1-h average NOx *	19th highest 1-h average NOx *	Annual average NOx *
A21	7.5	0.29	0.29	0.29
A22	7.5	0.38	0.38	0.38
A23	7.5	1.72	1.72	1.72
A24	7.5	1.39	1.39	1.39
A25	7.5	0.83	0.83	0.83
A26	7.5	0.36	0.36	0.36
A27	7.5	0.87	0.87	0.87
A28	7.5	0.84	0.84	0.84
A29	7.5	0.83	0.83	0.83
A30	7.5	2.11	2.11	2.11
A31	7.5	1.23	1.23	1.23
A32	7.5	3.14	3.14	3.14
A33	7.5	1.43	1.43	1.43
A34	7.5	0.91	0.91	0.91
A35	7.5	0.93	0.93	0.93
A36	7.5	0.97	0.97	0.97
A1Pa	7.5	2.19	2.19	2.19
A2Pa	7.5	1.09	1.09	1.09
A3Pa	7.5	1.27	1.27	1.27
A4Pa	7.5	1.76	1.76	1.76
A5Pa	7.5	1.48	1.48	1.48
V01	7.5	0.47	0.47	0.47
V02	7.5	1.31	1.31	1.31
V03	7.5	0.49	0.49	0.49
V04	7.5	2.19	2.19	2.19
Range		0.29 - 4.09	0.29 - 4.09	0.29 - 4.09
Max.		4.09	4.09	4.09
AQO Criteria		-	200	40

Remark: * Estimated based on the worst case meteorological condition, wind speed, and wind angle taking account the peak hour traffic flow generated and attracted by this Project. As a conservative approach, it has been assumed that the estimated pollutant concentration during the peak hour would persist for 8760 hours of a year when calculating the daily and annual concentrations. This is considered very conservative and is unlikely to occur. In reality, the traffic flow during most time of the day during non-peak hours would be much smaller, thus it is expected that the actual air pollutants concentrations generated by the traffic of this Project would be much smaller than the above predicted results