# Ocean Park Master Redevelopment Project

# EP-249/2006/A – Condition 2.25 Glare Impact Assessment Report May 2010

Certified by	<u> </u>	on 9 June 2010
	Lindsay Pickles (FTL)	

Verified by Independent Environmental Checker on 8 June 2010 IEC Certificate attached in the submission? Yes

Ocean Park Master Redevelopment Project

Environmental Permit No. EP-249/2006/A - Condition 2.25

Glare Impact Assessment Report

Submitted by ERM-Hong Kong, Limited dated 31-05-2010

This is to verify that

Glare Impact Assessment Report

Submitted by ERM-Hong Kong, Limited

dated 31-05-2010

Has been verified by the undersigned.

Signed

Dr Anne F Kerr

Independent Environmental Checker (IEC)

Retained by Ocean Park Corporation

pursuant to Environmental Permit No. EP-249/2006/A

Date

8 June 2010

# FINAL REPORT

Ocean Park Corporation, Hong Kong

# Ocean Park Symbio Show: *Glare Impact Assessment*

May 2010

# **Environmental Resources Management**

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# FINAL REPORT

Ocean Park Corporation, Hong Kong

# Ocean Park Symbio Show: *Glare Impact Assessment*

May 2010

Reference 0108721

For and on behalf of										
ERM-Hong Kong, Limited										
Approved by: Dr Andrew P Jackson Signed:										
Position: Managing Director										
Date: 31 May 2010										

This report has been prepared by ERM-Hong Kong, Limited with all reasonable skill, care and diligence within the terms of the Contract with the client, incorporating our General Terms and Conditions of Business and taking account of the resources devoted to it by agreement with the client.

We disclaim any responsibility to the client and others in respect of any matters outside the scope of the above.

This report is confidential to the client and we accept no responsibility of whatsoever nature to third parties to whom this report, or any part thereof, is made known. Any such party relies on the report at their own risk.

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# 1 INTRODUCTION

### 1.1 BACKGROUND

Ocean Park Corporation, Hong Kong (OPC) is in the process of redeveloping its educational and recreational attractions as part of the Ocean Park Master Redevelopment Plan (MRP).

An open-air lagoon night show will be hosted at the Aqua City as one of the new attractions of the Ocean Park. The most up-to-date layout plan of the lagoon and design drawings of the audio poles and audio speakers are presented in *Annex A*. Detailed description of the show and updated design details are presented in *Section 1.3*.

The potential environmental impacts of the MRP have been assessed and presented in the Environmental Impact Assessment Report for "Repositioning and Long Term Operation Plan of Ocean Park" (Register No. AEIAR-101/2006) (the approved EIA Report), and an Environmental Permit (EP-249/2006) for the MRP was granted on 28 July 2006. EP-249/2006 was replaced by EP-249/2006/A (EP) on 23 October 2006. Under the requirements of Condition 2.25 of the EP, a detailed design of night-time functional and thematic lighting is required. The design shall take into account the possible light pollution and night-time glare.

# 1.2 PURPOSE OF THE REPORT

This report presents the Glare Impact Assessment (GIA) undertaken by ERM-Hong Kong, Ltd (ERM) and its sub-consultant, CSA (M&E) Ltd, of the lagoon night show at the Ocean Park, Hong Kong. This report is to outline the study approach of the impact assessment for the night-time functional and thematic lighting of the show. Potential impacts of light pollution and negative glare impact to the nearby sensitive receivers have been assessed and compared with relevant guidelines.

# 1.3 THE LAGOON NIGHT SHOW

The lagoon night show, *Symbio*, is an open-air entertainment event to be hosted at the Aqua City featuring a combination of audio and visual effects.

The show will be held in an exterior area of about 4,000 m<sup>2</sup>, and a medium level of pollution has been assumed. A light loss factor of 0.75 has been employed in the assessment.

The duration of the show will be around 10 to 20 minutes. There will only be one show every night, and it will end before 22:00 hours, ie before Ocean Park closes daily.

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# 2 POTENTIAL SOURCES OF LIGHTS AND ASSUMPTIONS

With respect to the latest layout plan of the show (see *Annex A*), the light sources that have the potential to cause adverse glare impact to the nearby sensitive receivers are:

- Lighting poles with 3 rotating spot lights each around the lagoon;
- Underwater LED up lights mounted on the water screen pumps, water jet pumps, and water cannons;
- Theatrical flame effect jet up to 10 m within the lagoon;
- Theatrical flame on water effect around the centre circular water wall screen;
- Projector lights on the circular water wall screen; and
- Pyrotechnic Special Effects Material (PSEM) (1) within the lagoon.

The potential glare impact was assessed using a computer simulation based on the following assumptions.

- All spot lights with an output of 17,800 lumen and a 70 degree vertical beam angle directly pointing outward along the show area;
- Underwater LED up lights with an output of 810 lumen and no shielding by the water wall screen, to simulate the worst-case scenario;
- Theatrical flame jet effects assumed as upward light fixtures with an output of 50,000 lumen;
- The light impact of the theatrical flame on water effect will be at low level and blocked by the adjacent building. It is expected that the potential glare impact will be insignificant and therefore has not been included in the computer simulation;
- The projector lights with an output of 17800 lumen, a vertical beam angle of 45 degree upward and pointing outward from the show. The potential shading by the water projection screen has been neglected to simulate the worst-case scenario; and
- PSEM assumed as upward light fixtures with an output of 10,000 lumen.

A lighting schedule, including power, number and types of lighting is given in *Table 2.1*.

ENVIRONMENTAL RESOURCES MANAGEMENT

<sup>(1)</sup> The show proposes to use close proximity theatrical pyrotechnics, produced by Pyrotechnic Special Effects Material (PSEM), that have been developed for indoor use for stage shows and concerts.

Table 2.1 Lighting Schedule

Lur	ninaire Type	Power	Mounting Height	Beaming Direction	Nos.	Type	Lumen Output
1	Lighting pole with 3 head rotating spot light	3x1200W	6 m <sup>[Note]</sup>	70 degree	17	MSI metal halide	17800
2	Under water LED light	18x4.5W	Under water	90 degree upward	84	LED	810 (assumed)
3	Projector light on water wall screen	300W	Level to water surface	45 degree upward	5	NSH	17800 (assumed)
4	Theatrical flame effect	-	Level to water surface	90 degree upward	14	-	50000 (assumed)
5	PSEM	-	Level to water surface	90 degree upward	12	-	10000 (assumed)

# Note:

Each lighting pole will hold 3 intelligent lighting fixtures, each housed within its own enclosure. All lighting enclosures will be located at the same elevation around the lagoon. The top of all lighting enclosures will be at +23.5 mPD ( $Annex\ A$ ). All lighting poles are assumed at 6 m above ground, ie about the same level as the  $1^{\rm st}$  floor of the nearest sensitive receiver, to represent the worst-case scenario.

# 3 REPRESENTATIVE SENSITIVE RECEIVERS

Details of the representative sensitive receivers are presented in *Table 3.1* and their locations are shown in *Annex B*.

 Table 3.1
 Rrepresentative Sensitive Receivers

Ser	sitive Receiver	Type of Sensitive Receiver	Approximate Distance from the Show	Type of View
1	Mini Range Complex and Petrol Station	Commercial / Municipal	87 m	Obstructed view toward site, blocked by building inside Ocean Park
2	Wong Chuk Hang Road Garden	Municipal	290 m	Clear view, no significant obstruction
3	Buildings near Shouson Hill Road	Residential	270 m	Clear view, no significant obstruction
4	Country Villa	Residential	225 m	Clear view, no significant obstruction

# 4 ASSESSMENT METHODOLOGY

The potential glare impacts were assessed using the *Dialux 4.6* computer simulation programme.

Rectangular 'solid objects' have been used to simulate the representative sensitive receivers (see *Annex B*).

The assessment parameters, including glare, source intensity and light entry through windows are defined as follows:

- glare, occurs when a bright light source enters the visual field;
- source intensity, the luminance intensity extending beyond the area being lit from any single source in the potentially obstructive direction; and
- light entry through windows, (Ev), represents the vertical illuminance in Lux perpendicular to the window glazing.

The degrees of impacts on the representative sensitive receivers have been simulated as follows:

- Glare: the observer calculation points for the assessment of veil luminance have been included at the same strategic locations as the source intensity calculation points at the sensitive receivers;
- Source intensity: a luminous intensity calculation point has been included at 6m above ground level, pointing toward the show, at each of the sensitive receivers. The calculation points have been levelled to the light poles to represent the worst-case scenario; and
- Light entry through window: a calculation surface is created at the surface of each of the 'solid objects' that are facing the show.

# 5 ASSESSMENT CRITERIA

There is no legislative criterion for glare impact assessment in the *Technical Memorandum on Environmental Impact Assessment Process* (*EIAO-TM*). References have been made to relevant guidelines issued by the Highways Department (HyD) and The Chartered Institution of Building Services Engineers (CIBSE).

### 5.1 MAXIMUM ESTIMATED ALLOWABLE VEIL LUMINANCE

With reference to the *Public Lighting Design Manual* issued by the HyD, it is proposed to use the threshold increment for the assessment of the disability glare caused by the show. The threshold increment (% T.I.) will depend on both the background luminance and the veil luminance observed by the sensitive receivers. The maximum allowable veil luminance caused by the show is 3.64 candela (cd)/m², assuming an interior lighting arrangement of 200 Lux, a relative wall illuminance of 0.5, a wall reflectance of 0.5 and a maintenance factor of 0.8. Details of the calculation of maximum allowable veil luminance are presented in *Annex D*.

### 5.2 SOURCE INTENSITY

In accordance with the *Environment Consideration for Exterior Lighting* issued by the CIBSE, the source luminance shall be limited to 30 kilocandela (kcd) for Environmental Zone E3, Medium district brightness areas.

### 5.3 LIGHT ENTRY THROUGH WINDOW

In accordance with the *Environment Consideration for Exterior Lighting* issued by the CIBSE, the suggested maximum Lux level entering the window shall be less than 10 Lux for Environmental Zone E3, Medium district brightness areas.

# 6 ASSESSMENT RESULTS

The predicted glare, source intensity and light entry through window are presented below.

# 6.1 DISCOMFORT AND DISABILITY GLARE

The veil luminance will be caused by the show to the representative sensitive receivers. The veil luminance will reduce the contrast between the interior illuminance and the objects observed by the receivers, which may cause distraction and discomfort to the sensitive receivers.

The predicted maximum veil luminance is  $3.15 \text{ cd/m}^2$  at the Mini Range Complex, which is lower than the maximum allowable veil luminance of  $3.64 \text{ cd/m}^2$  as stated in *Section 5.1*. The predicted veil luminance was lower than  $0.91 \text{ cd/m}^2$  at other sensitive receivers, ie far lower than the maximum allowable veil luminance. Details of the supporting calculations are given in *Annex C*.

# 6.2 SOURCE INTENSITY

The predicted maximum source intensity of each light source at the calculation points (1 to 4) is 3.72kcd, which is well within the CIBSE 's requirement, as stated in *Section 5.2*. Results indicate that only Luminaire Type 1 (lighting poles) will have potential to impact the sensitive receivers, other Luminaire Types 2 to 5 will not have any impact on the sensitive receivers as they are either beaming upward or have insignificant lighting power. The predictions are summarised in *Table 6.2*.

Table 6.2 Summary of Predicted Source Intensity

Luminaire Type [1]	Luminous Intensity [cd] [2]	
Sensitive Receiver 1: Mi	ni range complex and petrol station	
Type 1	76	
Type 1	75	
Type 1	73	
Type 1	37	
Type 1	36	
Type 1	36	
Type 1	3652	
Type 1	3656	
Type 1	3670	
Type 1	3075	
Type 1	3090	
Type 1	3104	
Sensitive Receiver 2: Wo	ong Chuk Hang Road Garden	
Type 1	3621	
Type 1	3623	
Type 1	3625	
Type 1	10	
Type 1	10	

Luminaire Type [1]	Luminous Intensity [cd] [2]
Type 1	10
Type 1	3692
Type 1	3692
Type 1	3691
Type 1	3690
Type 1	3691
Type 1	3691
Type 1	3643
Type 1	3645
Type 1	3646
Type 1	3691
Type 1	3692
Type 1	3693
Type 1	3478
Type 1	3482
Type 1	3486
Type 1	3331
Type 1	3333
Type 1	3337
Type 1	1868
	918
Type 1	
Sensitive Receiver 3: Building	
Type 1	3660
Type 1	3661
Type 1	3662
Type 1	187
Type 1	186
Type 1	185
Type 1	3290
Type 1	3295
Type 1	3300
Type 1	3718
Type 1	3719
Type 1	3721
Type 1	2937
Type 1	2944
Type 1	2952
Type 1	3716
Type 1	3718
Type 1	3719
Type 1	2453
Type 1	2460
Type 1	2469
Type 1	2183
Type 1	2193
Type 1	2204
Type 1	2366
Type 1	290
Sensitive Receiver 4: Country	
Type 1	3160
Type 1	3169
Type 1	3178
Type 1	1844
Type 1	1835
Type 1	1826
Type 1	1040
Type 1	1046
Type 1	1053
Type 1	3350

Luminous Intensity [cd] [2]
3353
3361
568
573
577
3349
3352
3355
274
277
279
222
223
224
34
2460

### Notes:

- [1] In accordance with *Table 2.1*, Luminaire Type 1 refers to lighting pole with 3 head rotating spot light, ie a total of 51 nos. of Type 1 sources with 17 nos. of lighting poles.
- [2] Only luminaries with source intensity exceeded 1 cd have been shown.

# 6.3 LIGHT ENTRY THROUGH WINDOW

The predicted maximum Lux level is 1.30 at the Mini Range Complex, which is much lower than the CIBSE's requirement of 10 Lux, as stated in *Section 5.3*. Details of the calculations are given in *Annex C*.

# 7 RECOMMENDATIONS

In accordance with the EP Condition 2.26, a specialist with training and practical experience in outdoor sport lighting and illumination had been employed to design, manage and oversee the implementation and maintenance of the illumination requirements and system for the proposed nightly Ocean Park show.

Although the assessment results indicate no significant glare impact at the representative sensitive receivers, it is still recommended to undertake at least two rounds of monitoring prior to the nightly show tests and the performance. During each monitoring event, the Lux levels should be measured with a Lux Meter or Light Meter at one of the most affected sensitive receivers before and during the show. The increase in the Lux level with the show should be compared with that before the show. The Lux level measured during the show should also be compared with the recommended CIBSE's requirement of 10 Lux.

In case the monitoring results indicate measured Lux level higher than 10 Lux, an investigation of the exceedance is required to be conducted by the specialist. Recommendations should be given for any necessary adjustments to the lighting schedule of the show.

The specialist is also required to conduct regular checks, at least once a month, on the lights for the show to ensure that all lights are fixed at not more than 70 degree vertical beam angle and all lights being used are under the lighting schedule.

# 8 CONCLUSIONS

The predicted maximum veil luminance (ie  $3.15 \text{ cd/m}^2$ ) at all representative sensitive receivers is lower than the maximum allowable veil luminance of  $3.64 \text{ cd/m}^2$ .

The predicted source intensities of all lighting used for the show at the representative sensitive receivers are well below the criterion of 30kcd recommended by the CIBSE.

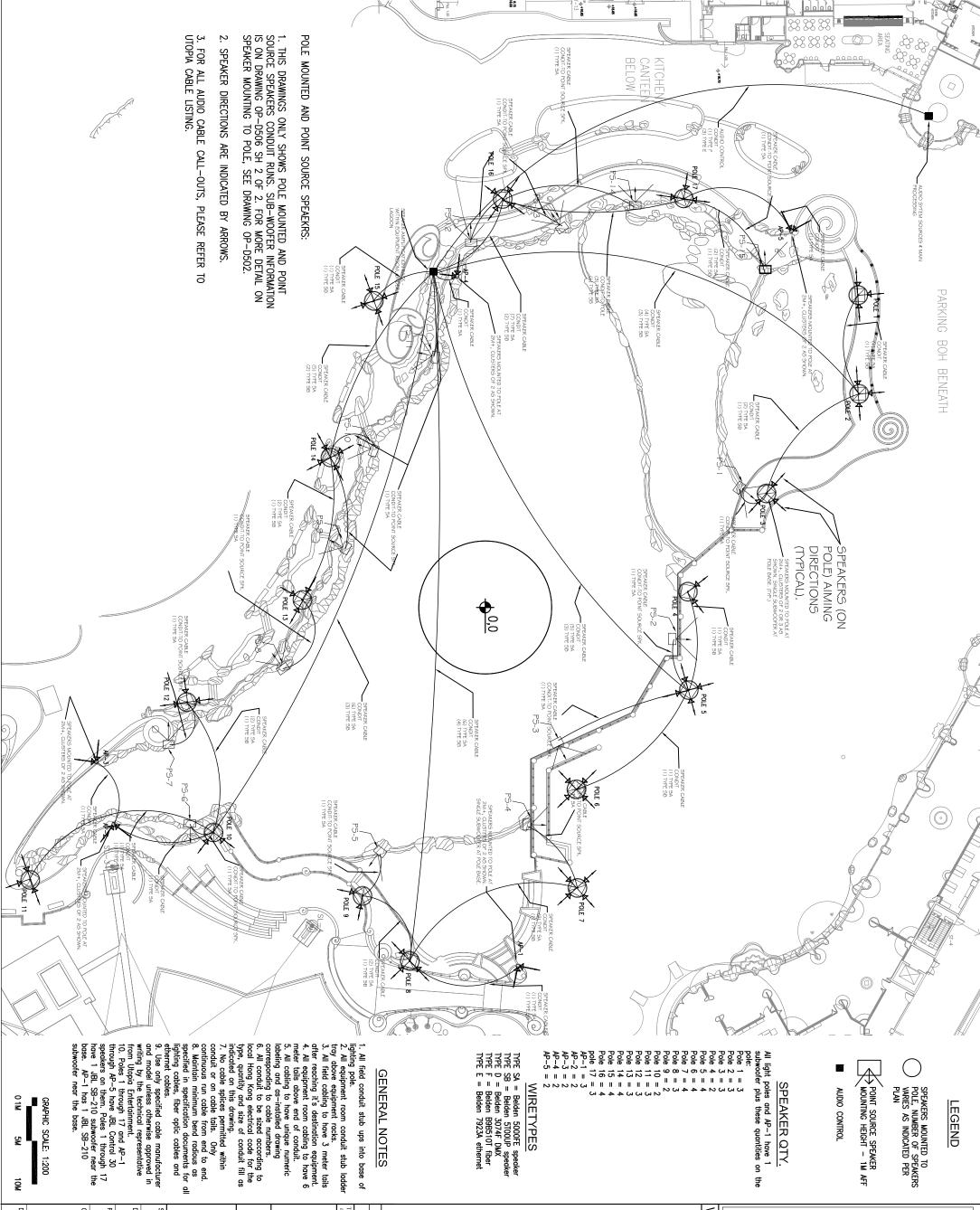
For light entry through window, the predicted Lux levels at all representative sensitive receivers are well below the CIBSE's recommendation of 10 Lux.

The potential glare impacts of the spot lights, underwater LED lights, theatrical flame effects, projectors, lights and PSEM effects of the lagoon night show to the representative sensitive receivers are considered insignificant.

The potential night-time glare impacts are expected to be further mitigated by its absorption into the overall operational lighting of the Ocean Park.

# Annex A

# Updated Design Layout Plans and Drawings



POINT SOURCE SPEAKER
MOUNTING HEIGHT - 1M AFF

# SPEAKER QTY.

light poles and AP-1 have 1 woofer plus these quantities on the

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# WIRETYPES

# GENERAL NOTES

æv.

DESCRIPTION

P.E. DATE

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SHOW FACILITY INPUT DRAWING

GRAPHIC SCALE: 1:200

10M

DRG. NO.

OP-0506 - SH 1 OF 2

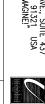
香港海洋公園 OCEAN PARK HONG KONG

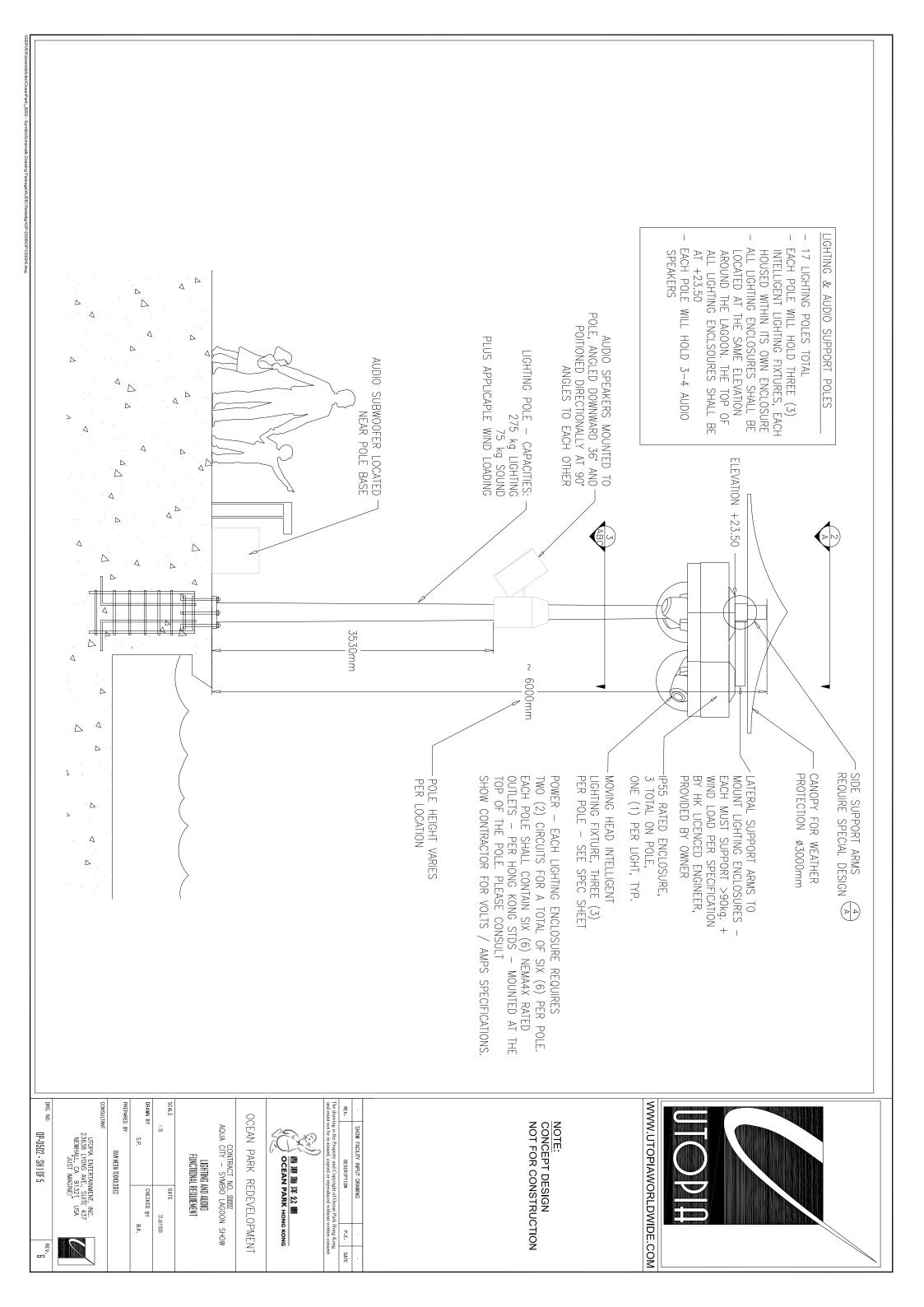
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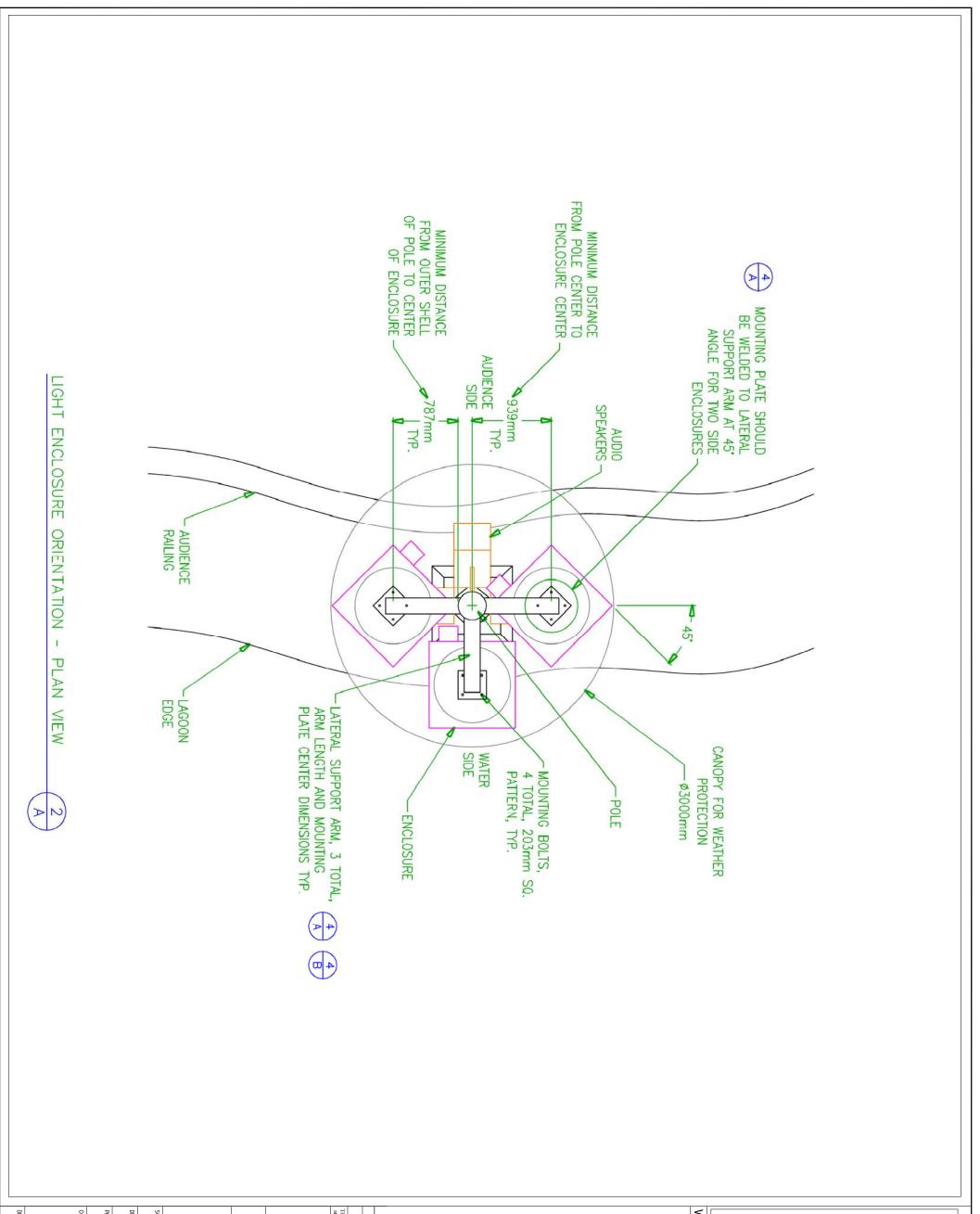
DRAWN BY PREPARED BY 1:200 S.P. RAW MEDIA TEKNOLOGIES SPEAKER CONDUIT SITE PLAN DATE Вү 23 JULY 2009 B.K.

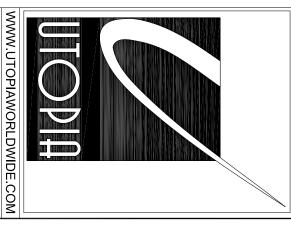


CONSULTANT









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OCEAN PARK REDEVELOPMENT

CONTRACT NO. SUZZZZ AQUA CITY — SYMBIO LAGOON SHOW LIGHTING AND AUDIO FUNCTIONAL REQUIEMENT

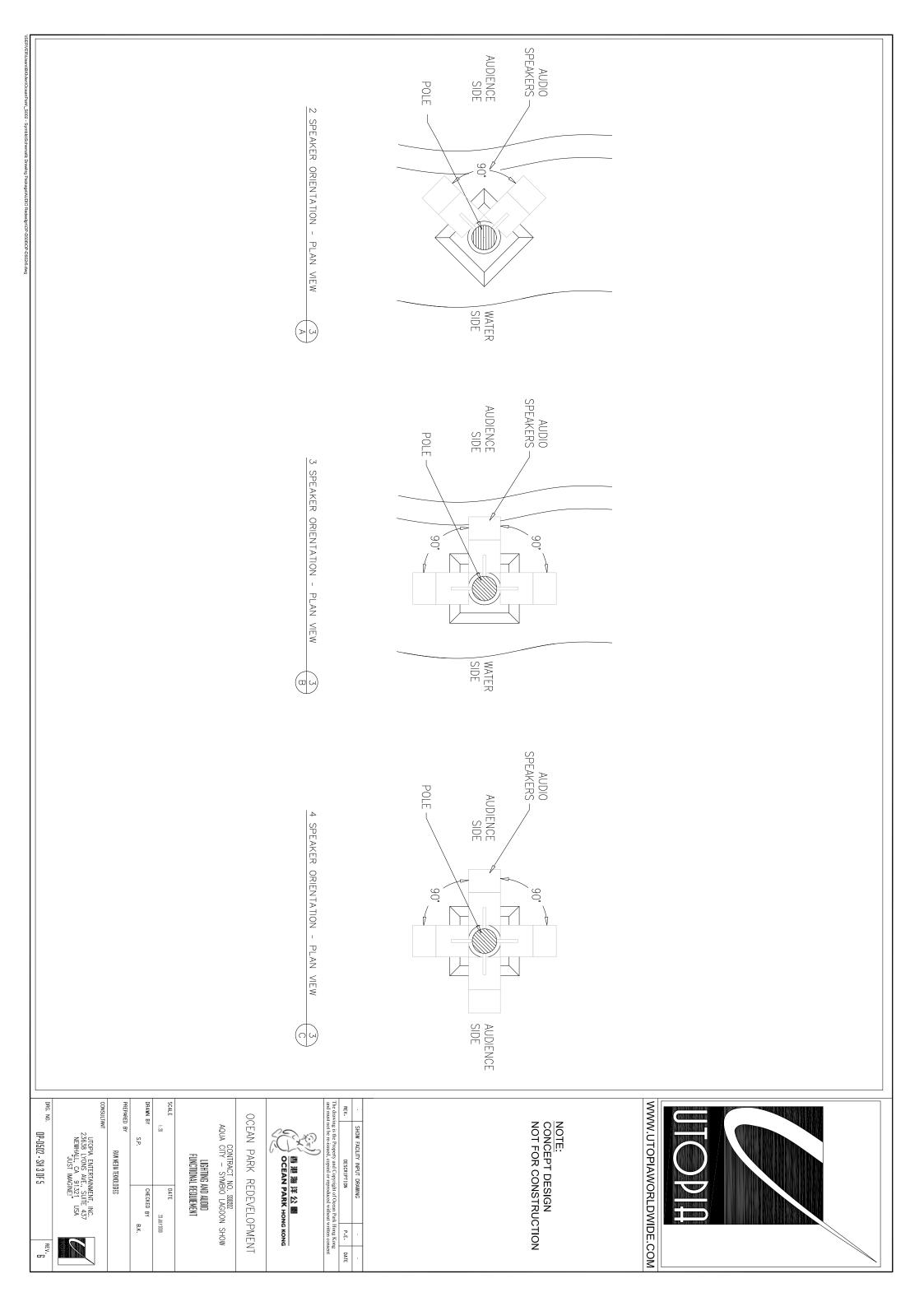
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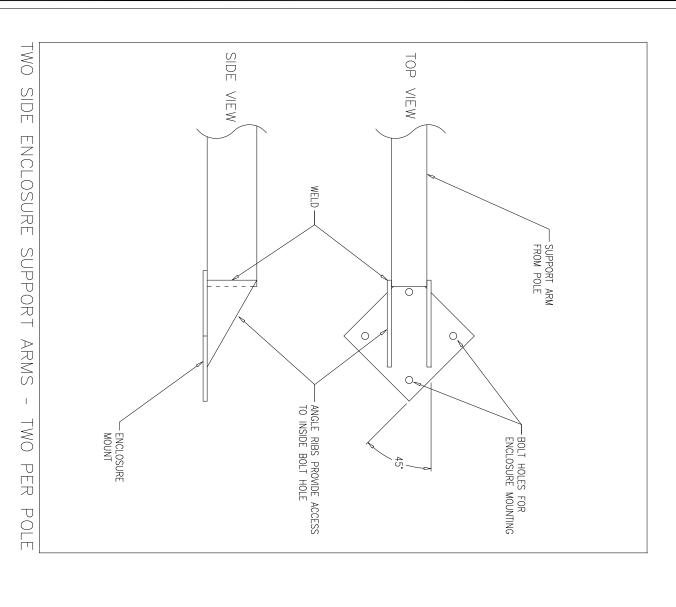
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OP-0502 - SH 2 OF 5



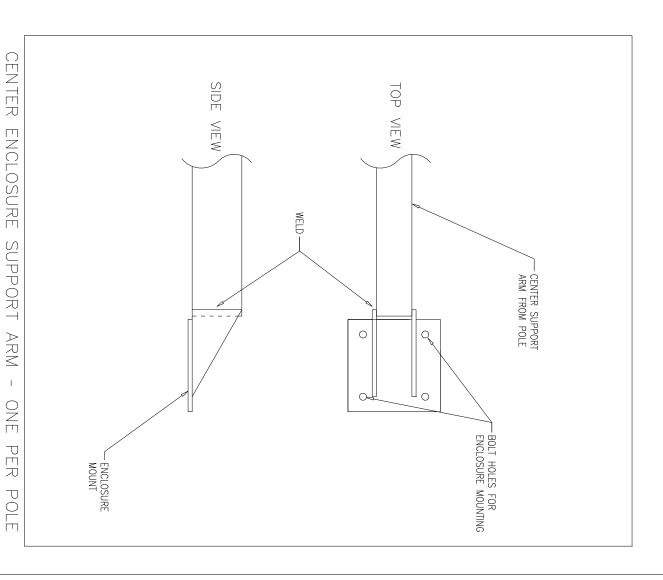




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SUGGESTED ANGLED SUPPORT ARM DESIGN





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SHOW FACILITY INPUT DRAWING

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OCEAN PARK REDEVELOPMENT

CONTRACT NO. SUZZIZ AQUA CITY — SYMBIO LAGOON SHOW

LIGHTING AND AUDIO FUNCTIONAL REQUIEMENT

NOT FOR CONSTRUCT

CONCEPT ONLY

SUGGESTED CENTRAL SUPPORT ARM DESIGN





PREPARED BY

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S.P.

CHECKED BY

B.K.

23 JULY 2009

- 20

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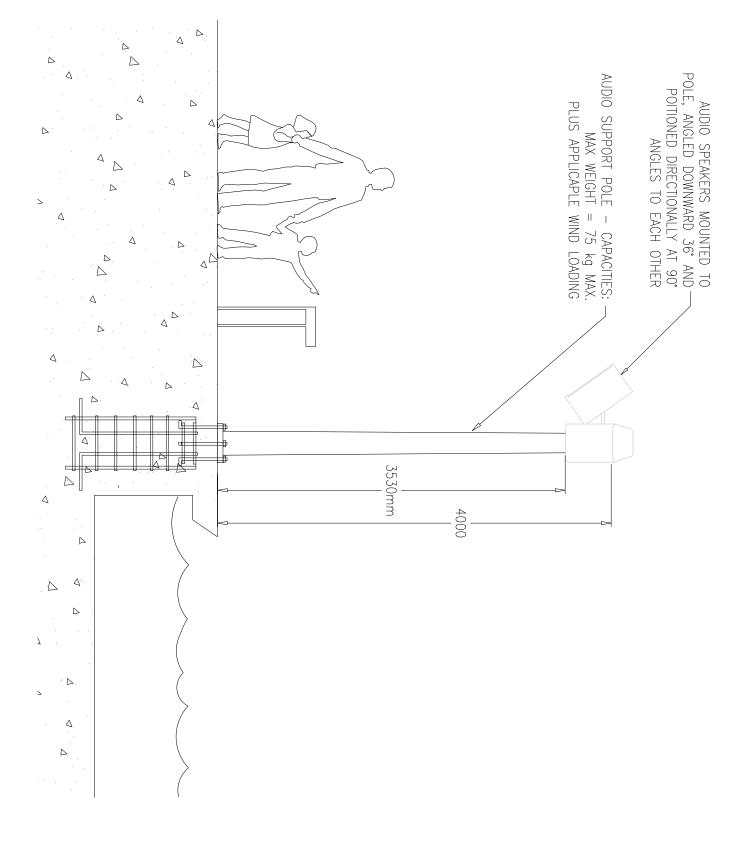
OP-D502 - SH 4 OF 5



# CONCEPT ZFOR CONSTRUCTION

SUPPORT POLES

5 AUDIO ONLY POLES TOTAL EACH POLE WILL HOLD 2-3 AUDIO SPEAKERS





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OCEAN PARK REDEVELOPMENT

CONTRACT NO. SUZZIZ AQUA CITY — SYMBIO LAGOON SHOW

AUDIO SUPPORT POLE - "AUDIO ONLY" FUNCTIONAL REQUIEMENT

PREPARED BY .20 S.P. CHECKED BY 23 JULY 2009 B.K.

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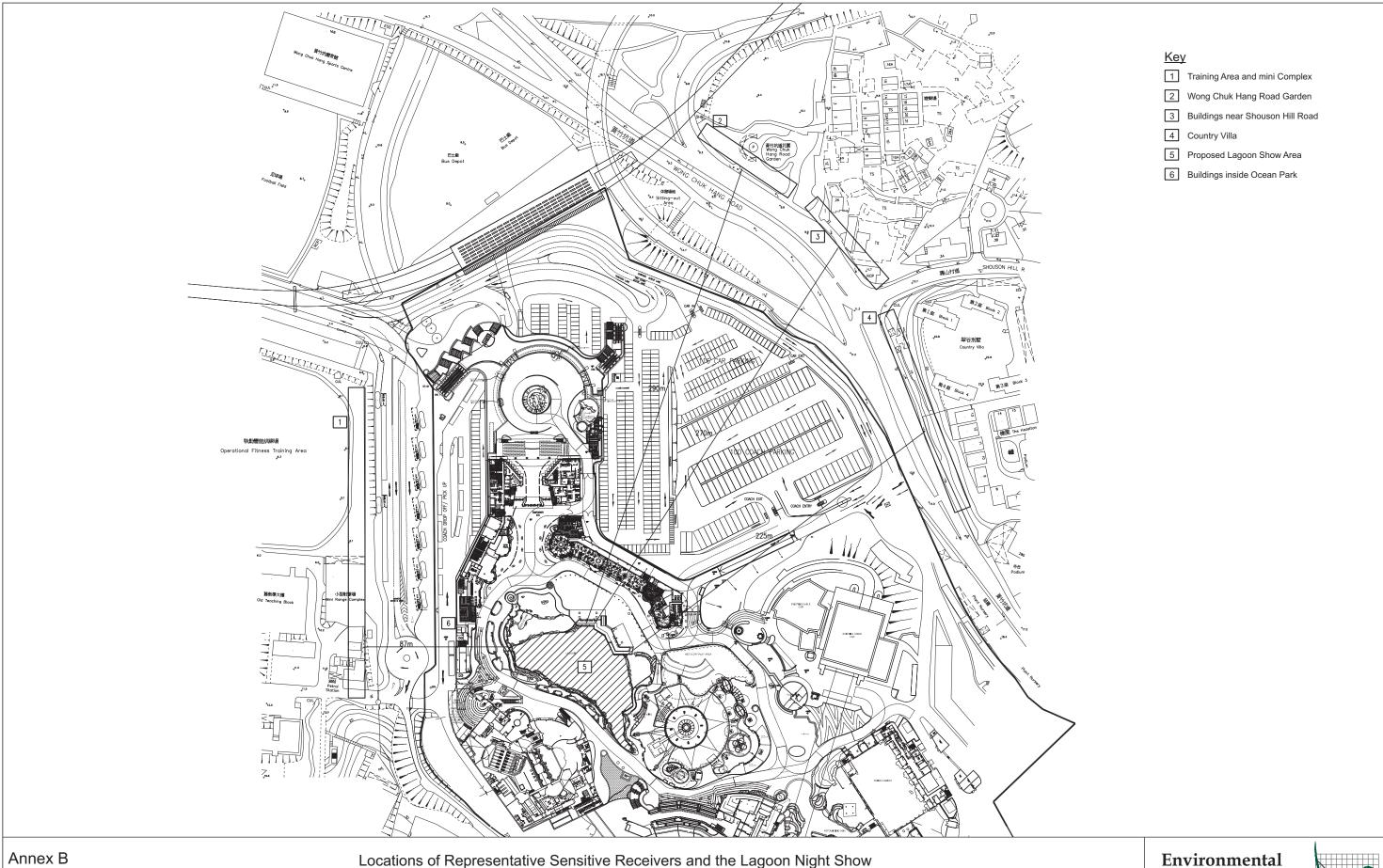
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OP-D502 - SH 5 OF 5



# Annex B

Locations of Representative Sensitive Receivers and the Lagoon Night Show



Locations of Representative Sensitive Receivers and the Lagoon Night Show

Resources Management

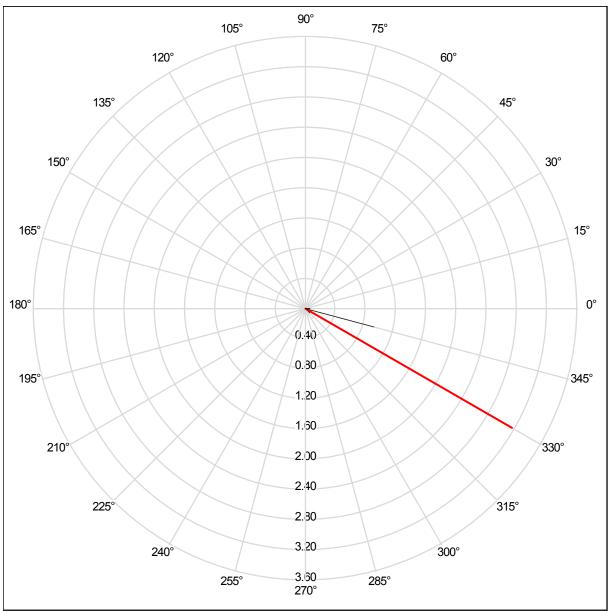


# Annex C

# Dialux Study Simulation

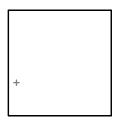


# Lagoon Show / Normal / GR Observer at Mini Range / Veil Luminances



Values in Candela/m²

Position of observer in external scene:

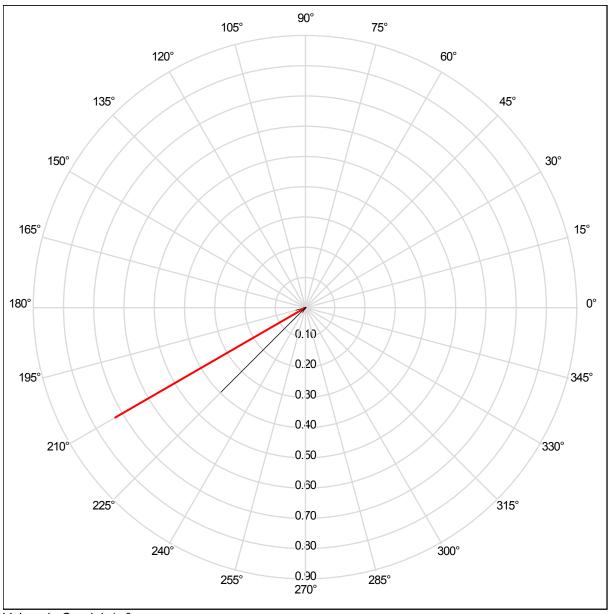


Position: (-35.117 m, 156.252 m, 6.000 m) Viewing sector: 0.0  $^\circ$  - 360.0  $^\circ$ , Increment: 15.0  $^\circ$ , Angle of inclination: -2.0  $^\circ$ 

Veil Luminance: Min: 0.00 cd/m², Max: 3.15 cd/m² The equivalent veil luminance of the environment has been calculated precisely.

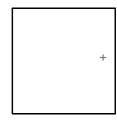


# Lagoon Show / Normal / GR Observer at Coutry Villa / Veil Luminances



Values in Candela/m²

Position of observer in external scene:



Position: (297.223 m, 249.424 m, 6.000 m)

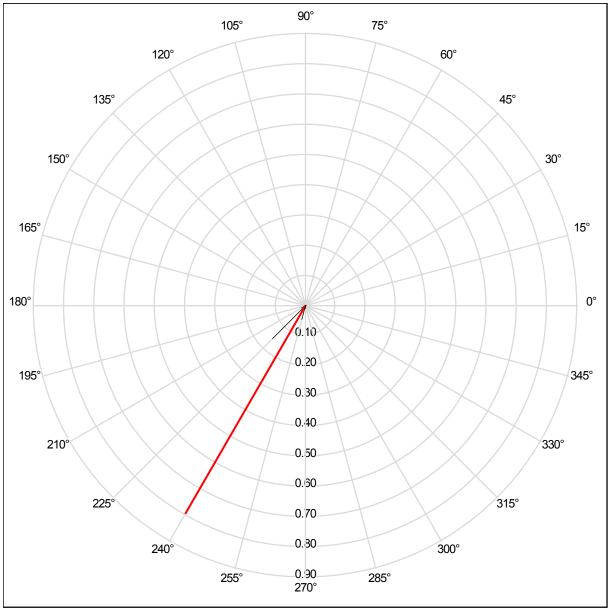
Viewing sector: 0.0  $^{\circ}$  - 360.0  $^{\circ}$  , Increment: 15.0  $^{\circ}$  , Angle of inclination: -2.0  $^{\circ}$ 

Veil Luminance: Min: 0.00 cd/m², Max: 0.73 cd/m²

The calculated equivalent veil luminance of the environment is based on the assumption of a complete diffuse reflection behavior of the environment (acc. EN 12464-2).

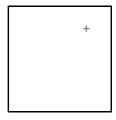


# Lagoon Show / Normal / GR Observer at Building / Veil Luminances



Values in Candela/m²

Position of observer in external scene:



Position: (245.863 m, 357.780 m, 6.000 m)

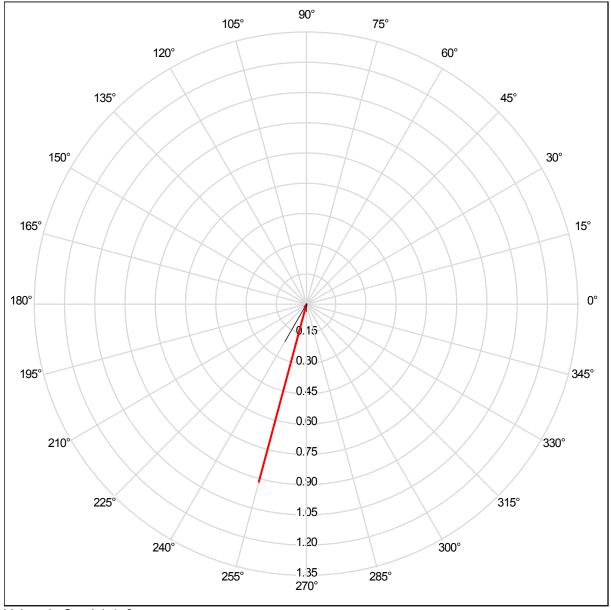
Viewing sector: 0.0  $^{\circ}$  - 360.0  $^{\circ}$  , Increment: 15.0  $^{\circ}$  , Angle of inclination: -2.0  $^{\circ}$ 

Veil Luminance: Min: 0.00 cd/m², Max: 0.79 cd/m²

The calculated equivalent veil luminance of the environment is based on the assumption of a complete diffuse reflection behavior of the environment (acc. EN 12464-2).

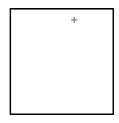


# Lagoon Show / Normal / GR Observer at Wong Chuk Hang Road Garden / Veil Luminances



Values in Candela/m²

Position of observer in external scene:



Position: (189.089 m, 403.264 m, 6.000 m)

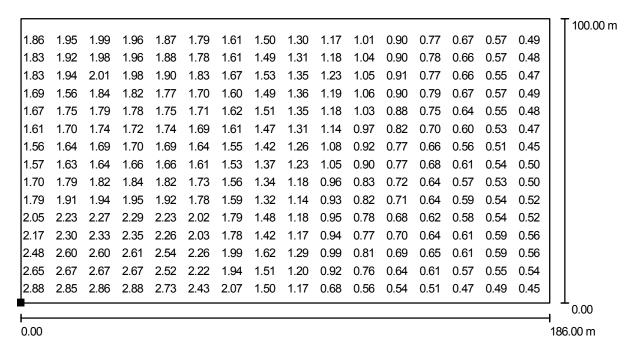
Viewing sector: 0.0 ° - 360.0 °, Increment: 15.0 °, Angle of inclination: -2.0 °

Veil Luminance: Min: 0.00 cd/m², Max: 0.91 cd/m²

The calculated equivalent veil luminance of the environment is based on the assumption of a complete diffuse reflection behavior of the environment (acc. EN 12464-2).



# Lagoon Show / Normal / Mini Range and Traning Area / face to Ocean Park / Value Chart (E)

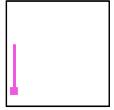


Values in Lux, Scale 1: 1330

Not all calculated values could be displayed.

Position of surface in external scene: Marked point:

(-35.117 m, 83.516 m, 0.000 m)

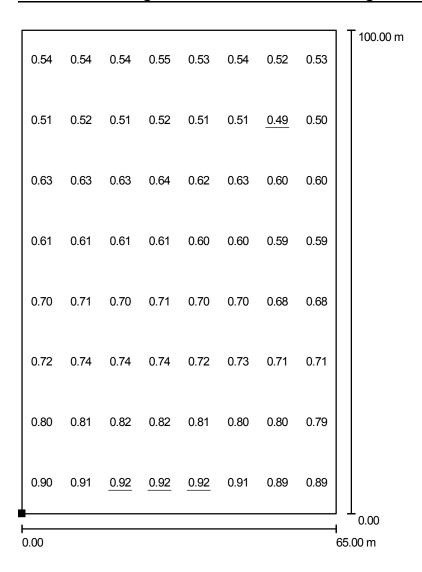


Grid: 64 x 32 Points

 $E_{av}[Ix]$   $E_{min}[Ix]$   $E_{max}[Ix]$  u0  $E_{min}/E_{max}$  1.30 0.26 3.07 0.197 0.083



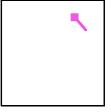
# Lagoon Show / Normal / Building / face to Ocean Park / Value Chart (E)



Values in Lux, Scale 1:782

Position of surface in external scene: Marked point:

(228.636 m, 377.528 m, 0.000 m)



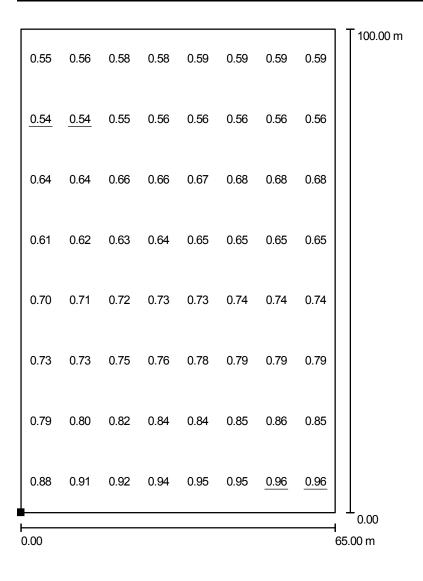
Grid: 8 x 8 Points

E<sub>av</sub> [lx] 0.68  $\mathsf{E}_{\mathsf{min}}\left[\mathsf{Ix}\right]$ 0.49  $\mathsf{E}_{\mathsf{max}}\left[\mathsf{Ix}\right]$ 0.92

u0 0.730  $\mathrm{E_{min}\,/\,E_{max}}$ 0.534



# Lagoon Show / Normal / Wong Chuk Hang Garden / face to Ocean Park / Value Chart



Values in Lux, Scale 1:782

Position of surface in external scene: Marked point: (164.243 m, 419.709 m, 0.000 m)

Grid: 8 x 8 Points

E<sub>av</sub> [lx] 0.71 E<sub>min</sub> [lx] 0.54 E<sub>max</sub> [lx] 0.96

u0 0.757  $E_{min}$  /  $E_{max}$  0.560



# Lagoon Show / Normal / Country Villa / face to Ocean Park / Value Chart (E)

0.47         0.49         0.50         0.51         0.50         0.51         0.52         0.53         0.52         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.54         0.51         0.52         0.53         0.52         0.53         0.52         0.53         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.51         0.52         0.51         0.51         0.52         0.51         0.53         0.52         0.51         0.52         0.51         0.53         0.52         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.53         0.53         0.53         0.53         0.53         0.53 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></td<>																	
0.49         0.50         0.52         0.53         0.52         0.53         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.53         0.54         0.51         0.51         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.51         0.51         0.52         0.51         0.52         0.51         0.51         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.56         0.55         0.56         0.55         0.56         0.55         0.56         0.56         0.56         0.55         0.53         0.53         0.53         0.53         0.53         0.53         0.55 <td< td=""><th>0.47</th><td>0.49</td><td>0.50</td><td>0.51</td><td>0.50</td><td>0.51</td><td>0.52</td><td>0.53</td><td>0.52</td><td>0.53</td><td>0.53</td><td>0.53</td><td>0.53</td><td>0.53</td><td>0.53</td><td>0.53</td><td>_</td></td<>	0.47	0.49	0.50	0.51	0.50	0.51	0.52	0.53	0.52	0.53	0.53	0.53	0.53	0.53	0.53	0.53	_
0.48         0.49         0.50         0.51         0.50         0.51         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.51         0.51         0.52         0.51         0.52         0.51         0.51         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.51         0.51         0.52         0.50         0.51         0.51         0.52         0.51         0.52         0.51         0.52         0.51         0.51         0.51         0.52         0.56         0.57         0.56         0.55         0.58         0.55         0.56         0.55         0.56         0.55         0.56         0.55         0.56         0.55         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.53         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.55 <td< td=""><th>0.46</th><td>0.47</td><td>0.48</td><td>0.49</td><td>0.48</td><td>0.50</td><td>0.50</td><td>0.51</td><td>0.50</td><td>0.51</td><td>0.51</td><td>0.51</td><td>0.50</td><td>0.51</td><td>0.51</td><td>0.51</td><td></td></td<>	0.46	0.47	0.48	0.49	0.48	0.50	0.50	0.51	0.50	0.51	0.51	0.51	0.50	0.51	0.51	0.51	
0.56         0.57         0.58         0.59         0.59         0.60         0.57         0.58         0.55         0.56         0.55         0.56           0.54         0.55         0.56         0.57         0.57         0.57         0.58         0.55         0.56         0.55         0.53         0.53         0.53         0.53           0.58         0.58         0.60         0.61         0.60         0.61         0.62         0.60         0.61         0.60         0.57         0.57           0.57         0.57         0.59         0.60         0.62         0.60         0.61         0.60         0.61         0.62         0.60         0.61         0.63         0.59         0.59         0.59         0.60         0.58         0.59         0.59         0.59         0.60         0.58         0.59         0.59         0.60         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.66         0.66         0.66         0.65         0.65         0.63         0.64         0.63         0.60         0.60         0.65         0.63 <th>0.49</th> <td>0.50</td> <td>0.52</td> <td>0.53</td> <td>0.52</td> <td>0.53</td> <td>0.53</td> <td>0.54</td> <td>0.53</td> <td>0.54</td> <td>0.53</td> <td>0.54</td> <td>0.53</td> <td>0.54</td> <td>0.54</td> <td>0.54</td> <td></td>	0.49	0.50	0.52	0.53	0.52	0.53	0.53	0.54	0.53	0.54	0.53	0.54	0.53	0.54	0.54	0.54	
0.54         0.55         0.56         0.57         0.56         0.57         0.57         0.58         0.55         0.55         0.55         0.53         0.53         0.53         0.53           0.58         0.58         0.60         0.61         0.60         0.61         0.62         0.60         0.61         0.58         0.59         0.57         0.57           0.57         0.57         0.59         0.60         0.62         0.60         0.61         0.60         0.61         0.62         0.60         0.61         0.58         0.57         0.57           0.57         0.59         0.60         0.59         0.60         0.58         0.59         0.58         0.59         0.58         0.59         0.58         0.59         0.58         0.59         0.58         0.59         0.58         0.59         0.58         0.59         0.59         0.59         0.59         0.60         0.65         0.65         0.65         0.65         0.66         0.66         0.66         0.66         0.66         0.66         0.66         0.65         0.65         0.63         0.63         0.63         0.60         0.60         0.60         0.60         0.65         0.65 <th>0.48</th> <td>0.49</td> <td>0.50</td> <td>0.51</td> <td>0.50</td> <td>0.51</td> <td>0.51</td> <td>0.52</td> <td>0.51</td> <td>0.52</td> <td>0.51</td> <td>0.51</td> <td>0.51</td> <td>0.51</td> <td>0.51</td> <td>0.52</td> <td></td>	0.48	0.49	0.50	0.51	0.50	0.51	0.51	0.52	0.51	0.52	0.51	0.51	0.51	0.51	0.51	0.52	
0.58         0.58         0.60         0.61         0.61         0.62         0.60         0.61         0.62         0.60         0.61         0.62         0.60         0.61         0.62         0.60         0.61         0.62         0.60         0.61         0.62         0.60         0.61         0.62         0.61         0.62         0.61         0.62         0.61         0.62         0.63         0.58         0.58         0.58         0.58         0.55         0.55         0.55         0.55         0.55         0.55         0.55         0.62         0.62         0.62         0.60         0.60         0.60         0.66         0.66         0.66         0.66         0.66         0.65         0.65         0.65         0.66         0.65         0.65         0.65         0.66         0.66         0.60         0.65         0.65         0.63         0.64         0.63         0.63         0.60         0.60         0.60         0.65         0.65         0.63         0.64         0.63         0.63         0.60         0.60         0.62         0.62         0.62         0.62         0.62         0.62         0.62         0.62         0.62         0.62         0.62         0.62 <td< td=""><th>0.56</th><td>0.57</td><td>0.58</td><td>0.59</td><td>0.58</td><td>0.59</td><td>0.59</td><td>0.60</td><td>0.57</td><td>0.58</td><td>0.57</td><td>0.58</td><td>0.55</td><td>0.56</td><td>0.55</td><td>0.56</td><td></td></td<>	0.56	0.57	0.58	0.59	0.58	0.59	0.59	0.60	0.57	0.58	0.57	0.58	0.55	0.56	0.55	0.56	
0.57         0.59         0.60         0.58         0.59         0.59         0.60         0.58         0.59         0.60         0.58         0.59         0.58         0.59         0.58         0.59         0.58         0.58         0.58         0.56         0.56         0.55         0.55           0.64         0.65         0.66         0.66         0.66         0.66         0.65         0.65         0.66         0.65         0.65         0.65         0.65         0.65         0.65         0.65         0.63         0.64         0.63         0.60         0.60         0.67         0.65         0.63         0.64         0.63         0.60         0.60         0.60         0.65         0.65         0.63         0.64         0.63         0.63         0.60         0.60         0.60         0.65         0.65         0.63         0.64         0.63         0.63         0.60         0.60         0.65         0.65         0.63         0.69         0.69         0.65         0.65         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.69         0.	0.54	0.55	0.56	0.57	0.56	0.57	0.57	0.58	0.55	0.56	0.55	0.55	0.53	0.53	0.53	0.53	ì
0.64       0.65       0.65       0.66       0.66       0.66       0.67       0.65       0.66       0.65       0.62       0.62       0.62       0.60       0.60         0.63       0.64       0.64       0.65       0.65       0.65       0.63       0.64       0.63       0.63       0.60       0.60       0.57       0.57         0.69       0.69       0.70       0.71       0.71       0.71       0.71       0.71       0.69       0.69       0.69       0.65       0.65       0.62       0.62       0.62       0.62         0.68       0.69       0.69       0.69       0.69       0.70       0.71       0.71       0.71       0.71       0.71       0.71       0.71       0.72       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.60 <t< td=""><th>0.58</th><td>0.58</td><td>0.60</td><td>0.61</td><td>0.60</td><td>0.61</td><td>0.61</td><td>0.62</td><td>0.60</td><td>0.61</td><td>0.60</td><td>0.61</td><td>0.58</td><td>0.58</td><td>0.57</td><td>0.57</td><td>ì</td></t<>	0.58	0.58	0.60	0.61	0.60	0.61	0.61	0.62	0.60	0.61	0.60	0.61	0.58	0.58	0.57	0.57	ì
0.63         0.64         0.64         0.65         0.65         0.65         0.65         0.63         0.64         0.63         0.63         0.63         0.63         0.63         0.60         0.60         0.57         0.57           0.69         0.69         0.69         0.71         0.71         0.71         0.71         0.71         0.71         0.69         0.60         0.60         0.60         0.60         0.60         0.60         0.60         0.60         0.60         0.60         0.60         0.60         0.67         0.71         0.71         0.71         0.72         0.75         0.75         0.74         0.69         0.69         0.65         0.	0.57	0.57	0.59	0.60	0.58	0.59	0.59	0.60	0.58	0.59	0.58	0.58	0.56	0.56	0.55	0.55	ì
0.69       0.69       0.70       0.71       0.71       0.71       0.71       0.71       0.69       0.69       0.69       0.69       0.65       0.65       0.62       0.62         0.68       0.68       0.69       0.69       0.69       0.69       0.70       0.70       0.68       0.68       0.67       0.67       0.63       0.63       0.60       0.60         0.76       0.77       0.78       0.78       0.79       0.78       0.78       0.77       0.77       0.75       0.74       0.71       0.71       0.67       0.67         0.75       0.75       0.77       0.77       0.77       0.77       0.77       0.75       0.75       0.74       0.69       0.69       0.65       0.65         0.85       0.87       0.86       0.88       0.86       0.87       0.87       0.85       0.84       0.82       0.82       0.78       0.77       0.74	0.64	0.65	0.65	0.66	0.66	0.66	0.66	0.67	0.65	0.66	0.65	0.65	0.62	0.62	0.60	0.60	ì
0.68       0.68       0.69       0.69       0.69       0.70       0.70       0.68       0.68       0.67       0.67       0.63       0.63       0.60       0.60         0.76       0.77       0.78       0.78       0.79       0.78       0.78       0.77       0.77       0.75       0.74       0.71       0.71       0.67       0.67         0.75       0.75       0.77       0.77       0.77       0.77       0.77       0.75       0.75       0.74       0.69       0.69       0.65       0.65         0.85       0.87       0.86       0.88       0.86       0.87       0.87       0.85       0.84       0.82       0.82       0.78       0.77       0.74	0.63	0.64	0.64	0.65	0.64	0.65	0.65	0.65	0.63	0.64	0.63	0.63	0.60	0.60	0.57	0.57	ì
0.76     0.77     0.78     0.78     0.79     0.78     0.78     0.77     0.77     0.75     0.74     0.71     0.71     0.67     0.67       0.75     0.75     0.77     0.77     0.77     0.77     0.77     0.75     0.75     0.74     0.69     0.69     0.65     0.65       0.85     0.87     0.86     0.88     0.86     0.87     0.87     0.87     0.85     0.84     0.82     0.82     0.78     0.77     0.75     0.74	0.69	0.69	0.70	0.71	0.71	0.71	0.71	0.71	0.69	0.69	0.69	0.69	0.65	0.65	0.62	0.62	ì
0.75  0.75  0.77  0.77  0.77  0.77  0.77  0.75  0.75  0.75  0.74  0.69  0.69  0.65  0.65  0.85  0.87  0.86  0.88  0.86  0.87  0.87  0.87  0.85  0.84  0.82  0.82  0.78  0.77  0.75  0.74	0.68	0.68	0.69	0.69	0.69	0.69	0.70	0.70	0.68	0.68	0.67	0.67	0.63	0.63	0.60	0.60	ì
0.85 0.87 0.86 0.88 0.86 0.87 0.87 0.87 0.85 0.84 0.82 0.82 0.78 0.77 0.75 0.74	0.76	0.77	0.78	0.78	0.78	0.79	0.78	0.78	0.77	0.77	0.75	0.74	0.71	0.71	0.67	0.67	ì
	0.75	0.75	0.77	0.77	0.77	0.77	0.77	0.77	0.75	0.75	0.75	0.74	0.69	0.69	0.65	0.65	
0.87 0.89 0.90 0.92 0.90 0.92 0.92 0.92 0.89 0.89 0.89 0.89 0.85 0.83 0.78 0.77	0.85	0.87	0.86	0.88	0.86	0.87	0.87	0.87	0.85	0.84	0.82	0.82	0.78	0.77	0.75	0.74	
	0.87	0.89	0.90	0.92	0.90	0.92	0.92	0.92	0.89	0.89	0.89	0.89	0.85	0.83	0.78	0.77	1 _

100.00 m

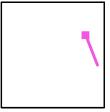
0.00

0.00 127.00 m

Values in Lux, Scale 1:908

Position of surface in external scene: Marked point:

(272.471 m, 312.912 m, 0.000 m)



Grid: 16 x 16 Points

E<sub>av</sub> [lx] 0.64 E<sub>min</sub> [lx] 0.46  $\mathsf{E}_{\mathsf{max}} \left[\mathsf{lx}\right] \\ 0.92$ 

u0 0.723  $\mathsf{E}_{\mathsf{min}}$  /  $\mathsf{E}_{\mathsf{max}}$  0.500

# Annex D

# Calculation of Maximum Allowable Veil Luminance

# CSA (M&E) Limited

# **Calculation Sheet**



Project: Ocean Park Glare Impact Assessment File Ref: 1329/Calc/Veil\_Lum

Service: Electrical Initial: TL Date: 8/12/2009

**Checked By**: BP **Dated**: 09/02/2010

# <u>To Calculate the Maximum Allowable Veil Luminance for a Limited Threshold</u> Increment of 15%:

### 1. Parameters and Assumptions:

Consider a Flat located at the sensitive receivers with interior illuminance level of 200 lux Relative illuminance at wall = 0.5 of work plane
Wall Reflectance = 0.5
Maintenance factor = 0.8

### 2. To calculate the wall luminance:

Illuminance Level at work plane = 200 Lux Wall Reflectance = 0.5 Wall illuminance (Eav) = 0.5 x 200 Lux = 100 Lux

Wall Luminance = 
$$\frac{R \times Eav}{p}$$
  
=  $\frac{0.5 \times 100}{3.1416}$  = 15.9 cd/ m<sup>2</sup>

Where:

R = Reflectance of the wall Eav = Illuminance level in Lux

### 3. To calculate the maximum allowable veil luminance for a limited threshold increment of 15%:

Threshold Increment (% T.I.) = 15 = 
$$\frac{95 \times LV}{(L/MF)^{1.05}}$$

$$15 = \frac{95 \times LV}{(15.9/0.8)^{1.05}}$$

$$LV = 3.644 \text{ cd/m}^2$$

Where:

Lv = Veil Luminance in cd/m<sup>2</sup> L= Background Luminance (Wall luminance) MF = Maintenance Factor

I.E. The veil luminance shall be limited to  $3.644 \text{ cd/m}^2$  for 15% threshold increment with 200 Lux interior lighting arrangement at the sensitive receivers assumed.

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