

# FINAL ASSESSMENT REPORT Environmental Impact Assesment

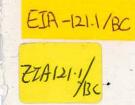
# Territory Development Department (Agreement No. CE34/93)

Yuen Long - Tuen Mun Corridor, Engineering Works for Hung Shui Kiu

# **EHS Consultants Limited**

Consultants in Environmental Protection, Health and Safety

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Yuen Long - Tuen Mun Corridor, Engineering Works for Hung Shui Kiu

Reference : R1383.97

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Client

Territory Development Department Hong Kong Government

Date :

August 1997

For and on behalf of EHS Consultants Limited:

Consultant

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# 1. INTRODUCTION

#### 1.1 Background

According to the North West New Territories Base Development Strategy, Hung Shui Kiu was recommended to be developed into a District Centre with "Medium Density Urban Development" to serve the population of the Corridor. With the existing Light Rail Transport and a proposed public transport terminus in the area, Hung Shui Kiu will provide government, institution and community facilities which include schools, a transport interchange, car parks and open space, for the population in the area. Land is also retained for commercial and residential uses. The Hung Shui Kiu District Centre will be implemented according to three newly gazetted outline zoning plans (OZPs).

Whilst numerous residential developments such as Parkview Garden and Meadowlands have already been developed by private sectors in the area, a high density rural public housing estate has also been scheduled at Area 13, which is expected to be completed in 2002. In order to provide supporting engineering infrastructure works to cope with the increasing demand from both existing and proposed developments at Hung Shui Kiu, it is necessary to implement the works included under Agreement No. CE34/93 : "Yuen Long - Tuen Mun Corridor - Engineering Works for Hung Shui Kiu" (PWP Items 225CL (Ph.2) and 253CL (Ph.1)). This Agreement involves the construction of a network of roads with associated services, and site formation for. various government and public uses in the area, with the scope of work shown in Figure 1-1 (the proposed works). The consultancy agreement also includes an Environmental Impact Assessment (EIA) which should address the environmental impact associated with the proposed works to be carried out under CE34/93, and the roadworks to be undertaken by the Highways Department independently under a separate project "Yuen Long - Tuen Mun Corridor - Engineering Works for Commercial/ Residential Areas at Hung Shui Kiu, Stage II, Phase I" (PWP Item 225CL (Ph.1)) as shown in Figure 1-2. The scope of the EIA is as shown in Figure 1-3.

EHS Consultants Limited (the Consultant) has been commissioned by Territory Development Department as sub-consultant to Ho Tin & Associates Consulting Engineers Limited (Ho Tin) to carry out this Environmental Impact Assessment (EIA) to identify and assess the nature and extent of environmental impacts associated with the construction and operation of the two proposed projects and all related activities taking place concurrently. Data on traffic flows on the proposed road scheme were predicted by the Project Traffic Consultant, MVA ASIA Limited.

### 1.2 Objective of the EIA

Section 3.1 (a) of the Study Brief presents the objectives for this EIA for the proposed projects. These are presented below:-

- (i) to describe the proposed project and associated works together with the requirements for carrying out the proposed project;
- (ii) to identify and describe the elements of the community and environment likely to be affected by the proposed project, and/or likely to cause adverse impacts upon the proposed project, including both the natural and man-made environment;
- (iii) to identify and quantify emission sources and determine the significance of impacts on sensitive receivers and potential affected uses;
- (iv) to propose the provision of infrastructure or mitigation measures so as to minimise pollution, environmental disturbance and nuisance during construction and operation of the project;

- (v) to identify, predict and evaluate the residual (i.e. after practicable mitigation) environmental impacts and cumulative effects expected to arise during the construction and operation phases of the project in relation to the sensitive receivers and potential affected uses;
- (vi) to identify, assess and specify methods, measures and standards, to be included in the detailed design, construction and operation of the project which are necessary to mitigate these impacts and reduce them to acceptable levels;
- (vii) to design and specify the environmental monitoring and audit requirements necessary to ensure the implement and the effectiveness of the environmental protection and pollution control measures adopted;
- (viii) to investigate the extent of side-effects of proposed mitigation measures that may lead to other forms of impacts;
- (ix) to identify constraints associated with the mitigation measures recommended in the study; and
- (x) to identify any additional studies, including ecological surveys, necessary to fulfill the objectives to the requirements of this Environmental Impact Assessment Study.

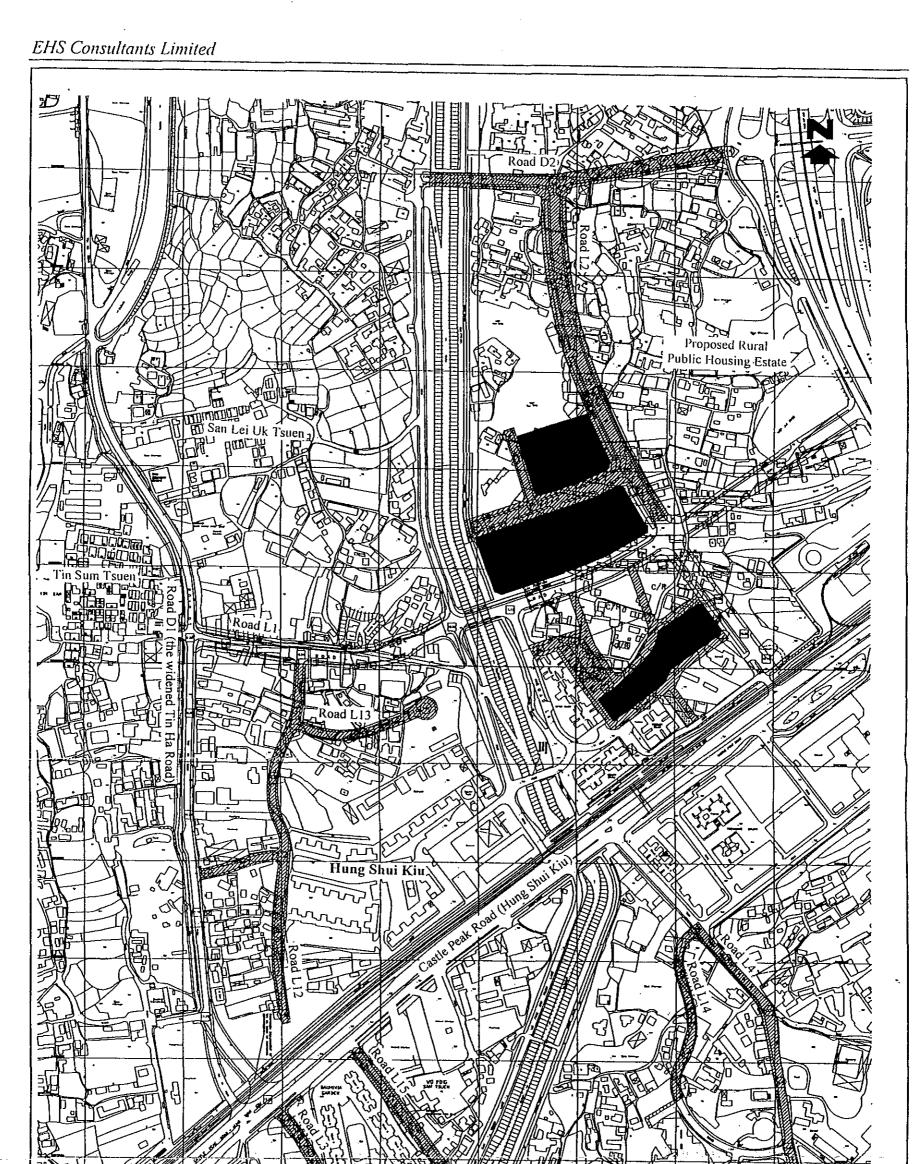
#### 1.3 Scope of Works

The scope of the EIA as stipulated in Figure 1-3 covers the assessment of the proposed works to be carried out under CE34/93 (PWP Items 225CL (Ph.2) and 253CL (Ph.1)) and the proposed roadworks to be undertaken by the Highways Department under a separate project (PWP Item 225CL (Ph.1)).

In the following sections of this EIA report, the proposed works to be carried out under CE34/93 and the separate roadworks to be undertaken by the Highways Department will be collectively referred to as the "proposed projects" for simplicity.

This EIA study focuses on the following environmental issues :-

- (i) Background Environmental Quality :-
  - ambient TSP, NO<sub>2</sub> and CO level monitoring; and
  - existing industrial emissions affecting the study area.
- (ii) Construction phase:-
  - air quality impact due to fugitive dust emission;
  - noise impact generated from construction activities; and
  - review the standard pollution control clauses provided with the Study Brief and advise the appropriate clauses to be included in the Contract Documents.
- (iii) Operational phase:-
  - air quality impact resulted from vehicular emission; and
  - traffic noise impact
- (iv) Environmental Monitoring & Audit (ref.: R817/0896; a stand-alone document as required by the study brief) :-
  - construction phase consideration; and
  - operational phase consideration.

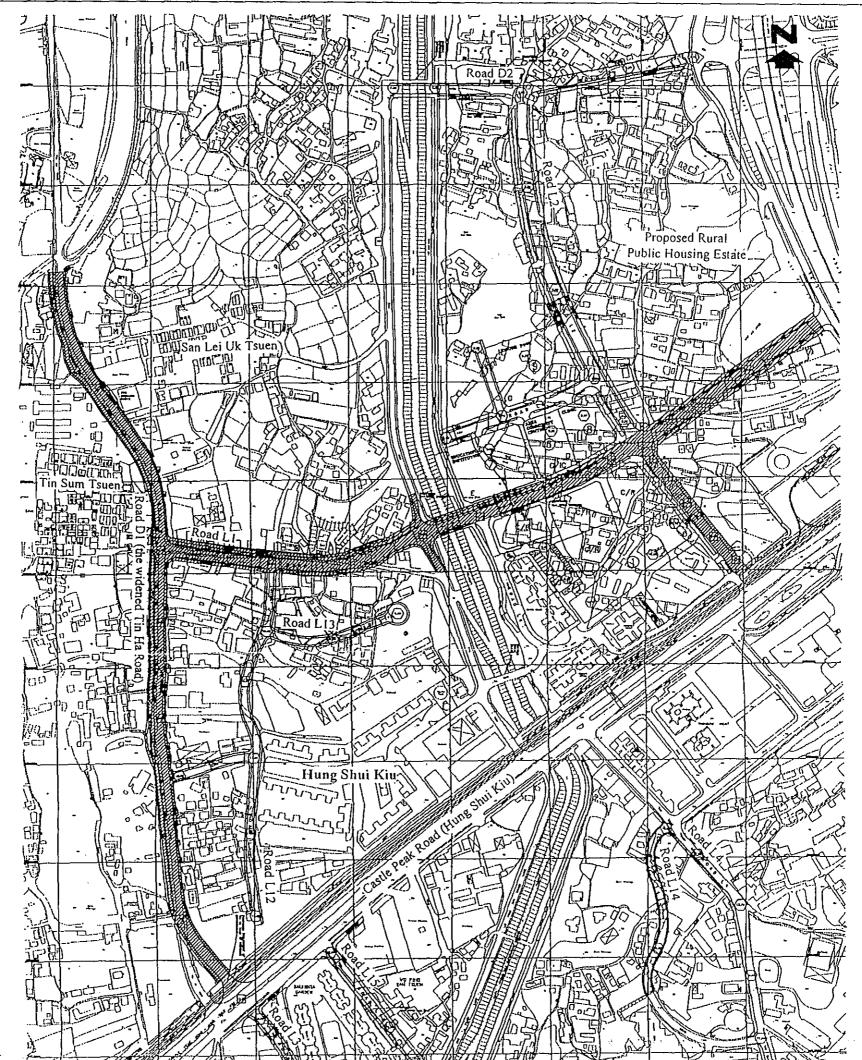


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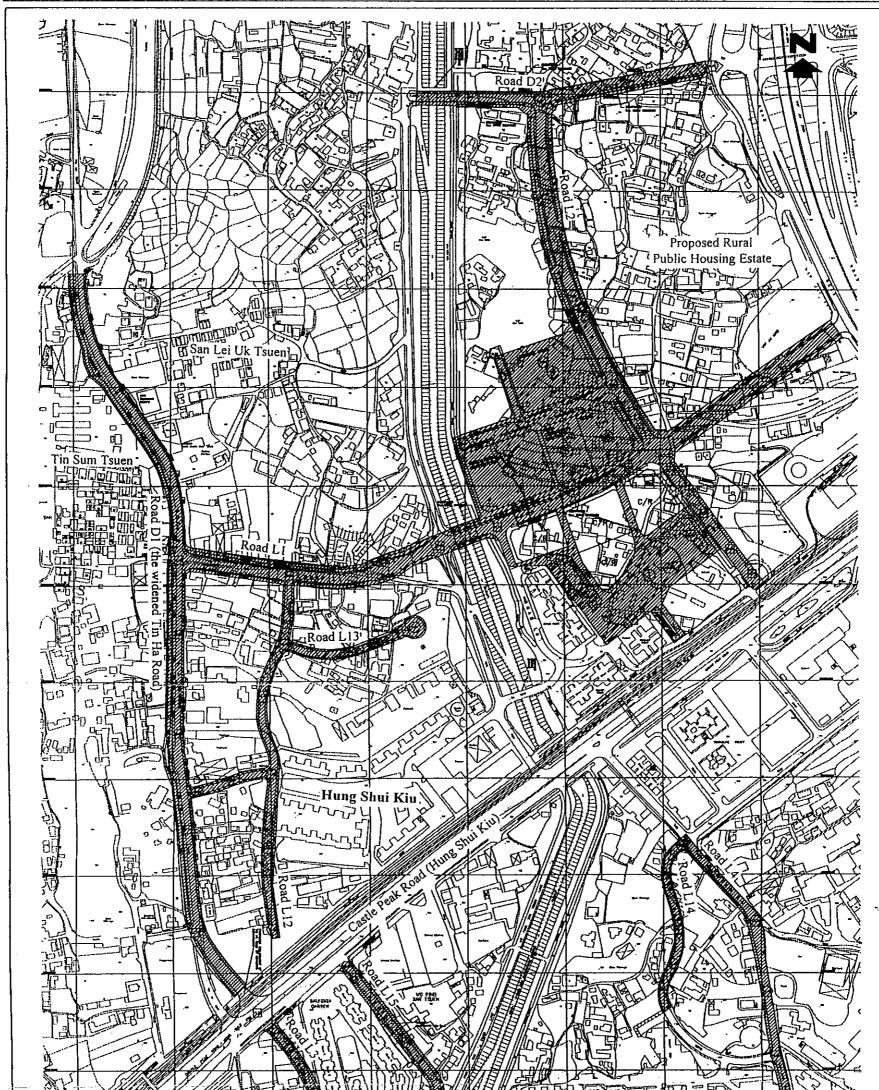


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PROJECT : Territory Development Department (CE 34/93) EIA Study for Hung Shui Kiu	
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# 2. PROJECT DESCRIPTION

#### 2.1 General Description

As mentioned in Section 1.3, this EIA will address the potential environmental impact associated with the construction and operational phases of the proposed projects, which involves the proposed works to be carried out under CE34/93 and the roadworks to be undertaken by the Highways Department.

The scope of the engineering works to be carried out under CE34/93 as shown in Figure 1-2 includes:-

- site formation of about 2.2 hectare of land for various government and public uses (Planning Areas 1, 6 to 9 as marked on Figure 1-1) and for a lorry/car park, footpaths and bicycle parks;
- (ii) construction of about 3.4 km of access roads;
- (iii) construction of cycle tracks and footpaths;
- (iv) construction of road drainage, sewers and associated works; and
- (v) landscaping and any environmental impact abatement works.

The proposed works will mainly involve the construction of local access roads whilst site formation will provide land for a district open space, a community centre, a primary school, a clinic and a leisure pool to be developed at Area Nos. 1, 6, 7, 8, and 9 respectively.

The scope of the proposed roadworks to be undertaken by the Highways Department as shown in Figure 1-2 includes:-

- (i) construction of road L1 and the associated cycle tracks and footpaths;
- (ii) construction of the section of road L2 not covered under CE34/93 and the associated cycle tracks and footpaths;
- (iii) widening of a section of the existing Tin Ha road from the existing 6.75m to the future 10.3m (the road will remain a single two-lane carriageway with an unchanged speed limit of 50km/hr) and the construction of the associated cycle tracks and footpaths; and
- (iv) realignment of a section of Tin Ha road adjacent to Castle Peak road.

The design, layout and level of the proposed new roads (D2, L1 to L6, and L12 to L15) and improved road (D1; formed from the existing Tin Ha Road) to be constructed under the two projects are shown in Figures 2-1.

### 2.2 Construction Phase Consideration

In the absence of a concrete construction schedule and equipment lists at this early planning stage for the proposed projects, assessment of air quality and noise impact during the construction phase has been based on reasonably assumed construction activities and schedules which are comparable to the normal practices, but with due consideration of the local situation and site constraints. This tentative construction schedule is shown in Table 2-1 below :

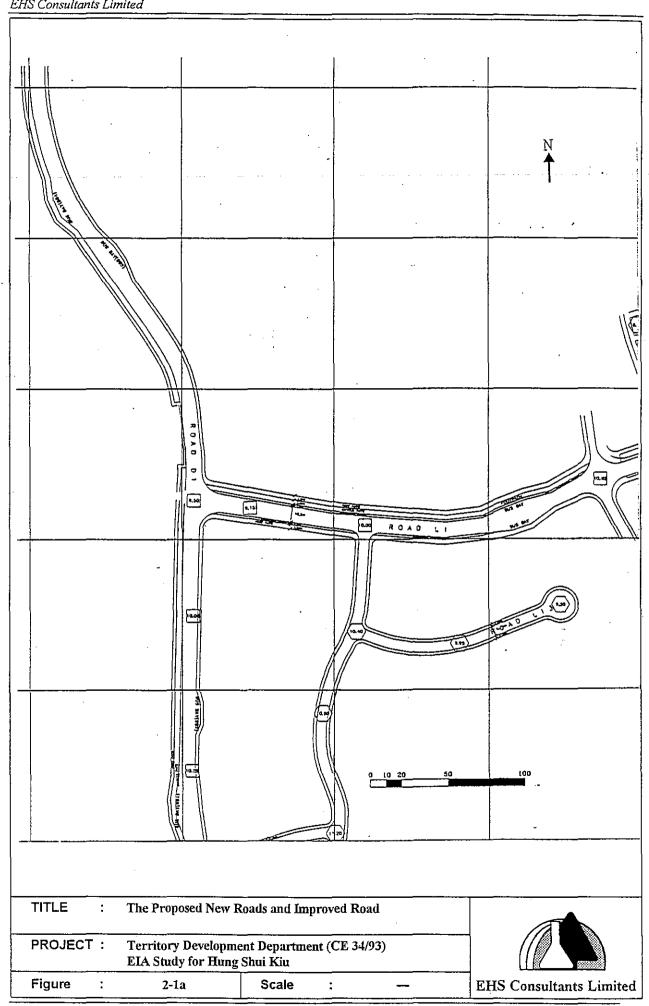
Stage	Description
1	Site clearance, excavation and earthworks for alignment and site formation;
2	Percussive piling at foundation locations for nullah crossing plus its formation;
3	Installation of drainage, utilities and manhole plus construction of retaining walls;
4	Formation of road sub-base; and
5	Road surfacing and finishing works

Location of the nullah crossings (PL1 and PL2) at which percussive piling will be required under the proposed projects is shown in Figure 2-2.

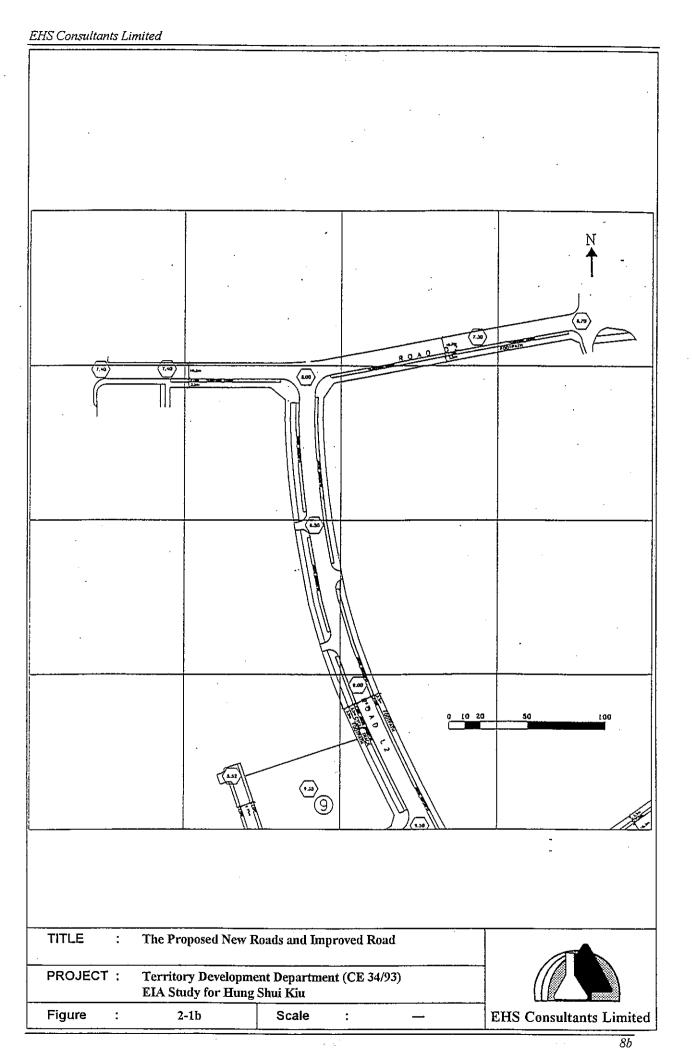
It is envisaged that the roadworks to be carried out by the Highways Department will commence earlier than the proposed works to be undertaken under CE34/93 so that the cumulative air quality and noise impacts would be lower than if they were taking place concurrently. However, in the absence of a concrete construction schedule, we have adopted a conservative approach and have assessed the worst case scenario by assuming that both roadworks operate at the same time.

#### 2.3 Operational Phase Consideration

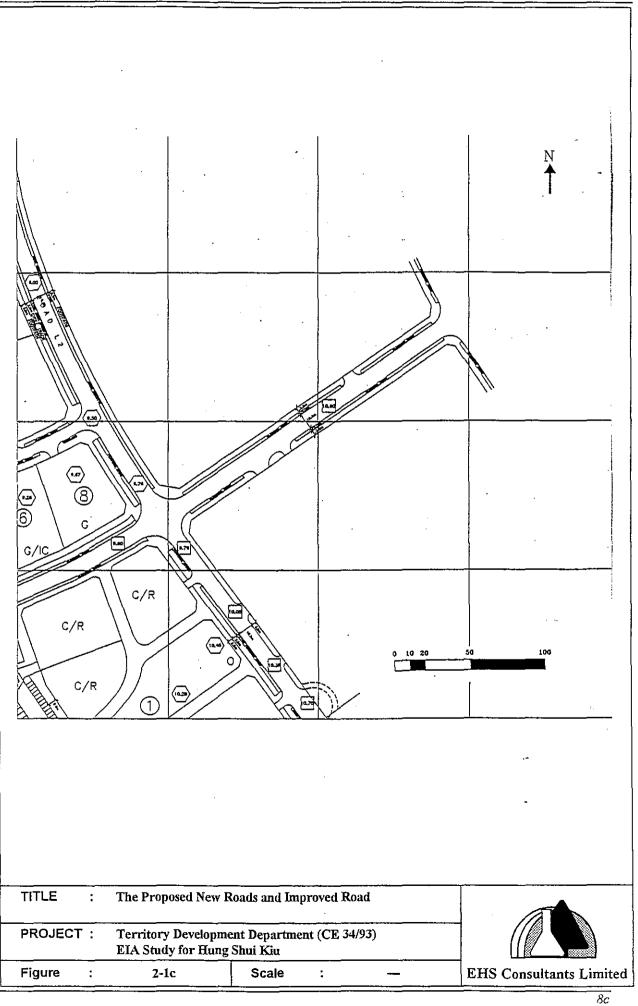
The major concerns related to the operational phase of the proposed road scheme are in terms of traffic noise and vehicular emission impacts. Technical assessments have been conducted to review the possible environmental effects with regard to the proposed road scheme upon existing sensitive receivers and future sensitive developments in the area. Traffic data for the assessment was provided by the Project Traffic Consultant.



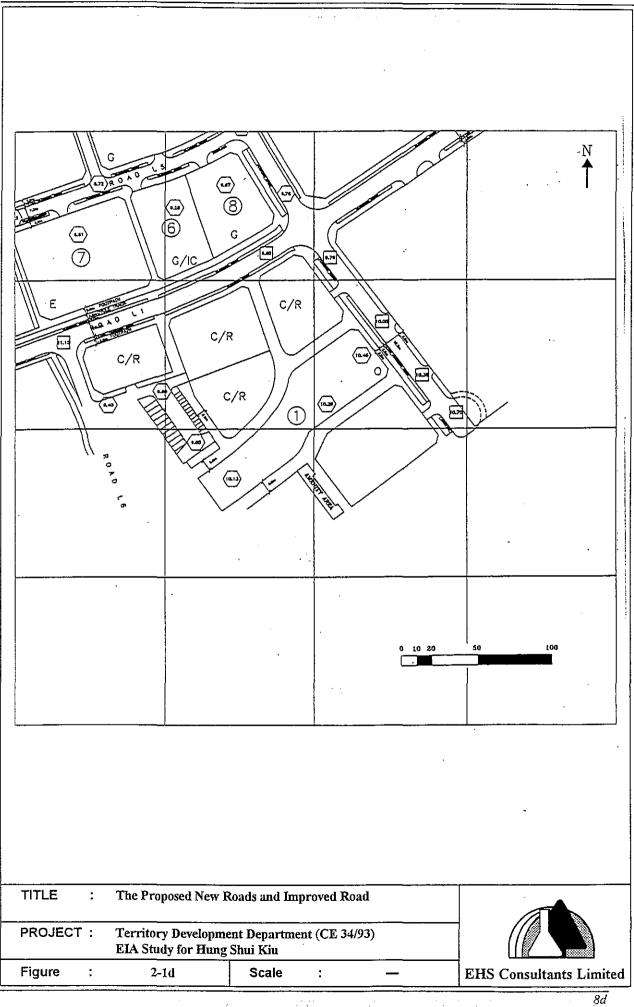
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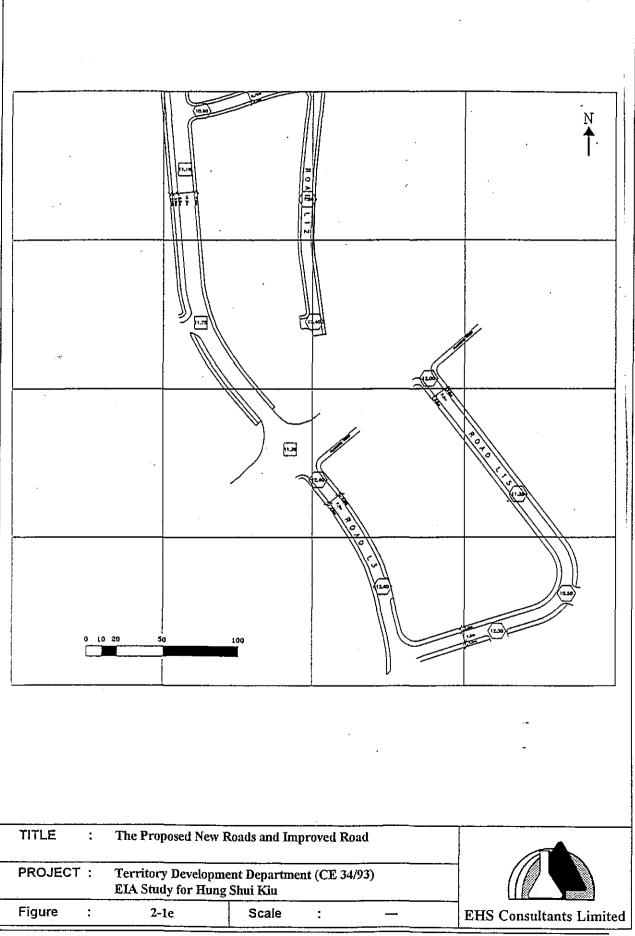
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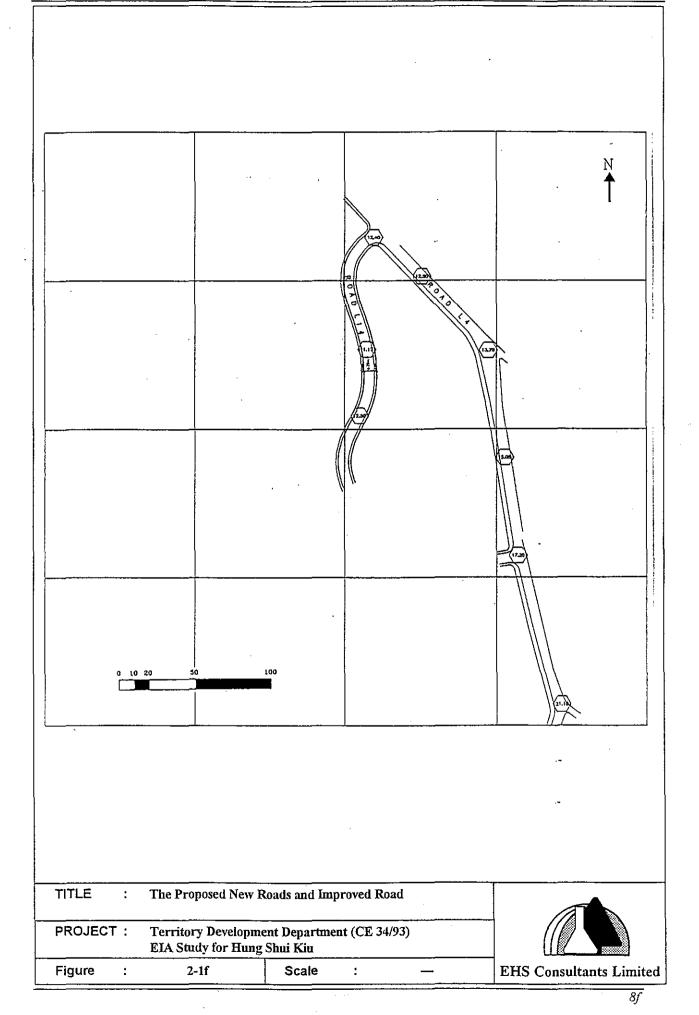
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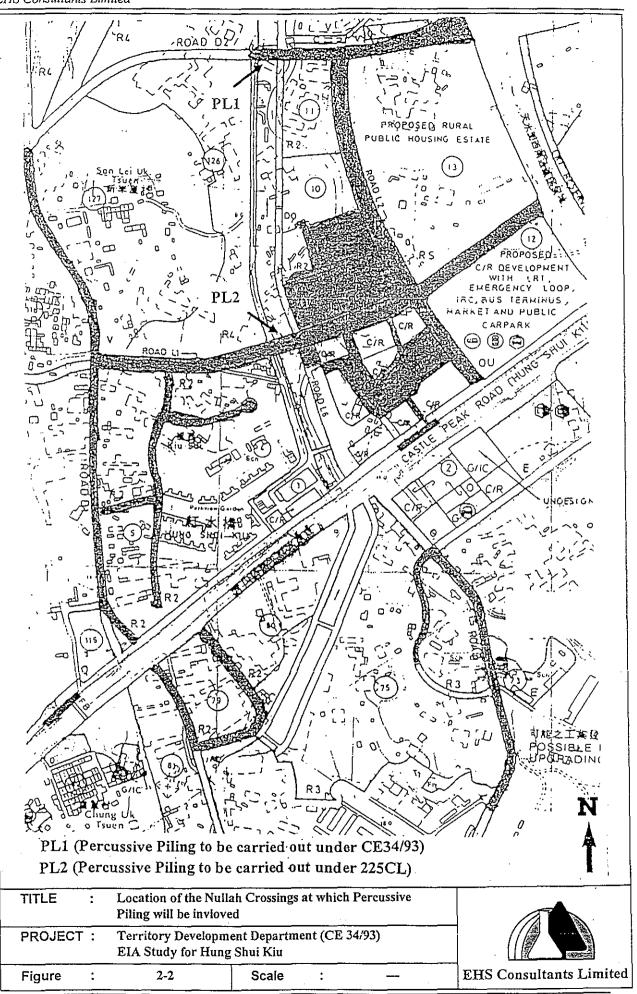
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### 3. EXISTING ENVIRONMENT

#### 3.1 Introduction

The existing and planned land uses and developments in the proximity of the proposed projects were conveyed by consulting District Lands Office, Planning Department, the Hong Kong Housing Society (HKHS) and through site inspections. The information obtained was used to identify existing and future sensitive receivers likely to be affected by the construction and operational phases of the proposed projects.

#### 3.2 General Description of the Study Area

#### 3.2.1 Existing Environment

The area around Hung Shui Kiu is in general topographically flat but is sloping gently at an inclination from south to north. Near Castle Peak Road the exiting ground level is about 12mPD whereas at the proposed road D2 the existing ground levels go down to about 7mPD. The existing population in the area is estimated to be about 4,200 with the majority of the population (about 53%) living in village houses, simple stone or temporary structures that are clustered together within villages. These include Chung Uk Tsuen, Wo Ping San Tsuen and Tan Kwai Tsuen that are located to the south of Castle Peak Road, and San Lei Uk Tsuen, Tin Sum Tsuen and Shek Po Tsuen situated to the north of the Road. Several private developments have been built in recent years in the area which include Parkview Garden, Coronet Court, the Bauhinlia Garden, and Meadowlands, etc. Other major land uses in the area include temporary industrial buildings and storage facilities, schools and agricultural land. The existing environment in the vicinity of the proposed project is shown in Figure 3-1.

#### 3.2.2 Scheduled Future Land Uses

Despite the recent rapid development by private sectors in the area, Hung Shui Kiu is still mostly occupied by village houses, temporary industrial buildings, storage facilities and agricultural land. However, with continuous rapid development, especially after the operation of the proposed road scheme, it is anticipated that the existing rural features will soon be replaced by new designated land uses.

The scheduled future land uses in the neighbourhood of the proposed projects are well specified in three recently gazetted OZPs, namely, the Ping Shan OZP No. S/YL-PS/1 and the Tong Yan San Tsuen OZP No. S/YL-TYST/1 gazetted on 14th June 1996, and the Lam Tei Yick Yuen OZP No. S/TM-LTYY/1 gazetted on 7th June 1996. The population capacity of the Hung Shui Kiu area is expected to be around 34,000. The future land uses in Hung Shui Kiu have been extracted from the relevant OZPs and summarised in Figure 3-2.

#### 3.3 Existing Industrial Sources

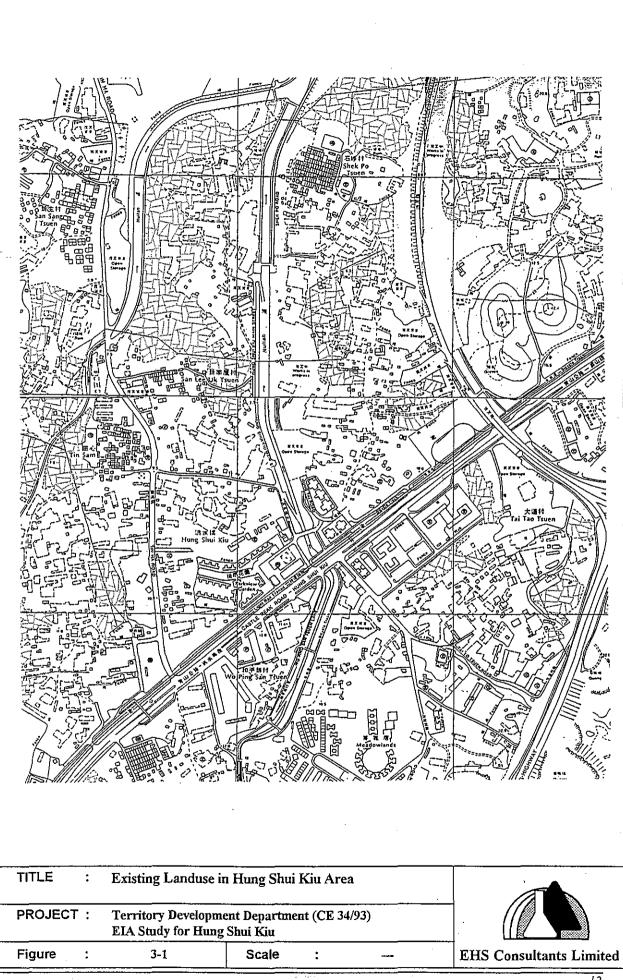
Industrial operations involving the burning of fuel are major emission sources of anthropogenic  $SO_2$ . The concentration and dispersion level of  $SO_2$  emission are related to the type and age of the boiler, as well as the type and quantity of fuel consumption, chimney height and size, and the exit temperature of the emission. A total of 18 operating diesel fuel consuming stacks were identified in the proximity of the study area according to EPD's (Air Management Group) record in August 1995.

### 3.4 Existing and Committed Sensitive Receivers

From the above analysis of existing and scheduled land uses, sensitive receivers situated in the proximity of the proposed projects have been identified, based on definition as laid down in the Hong Kong Planning Standards and Guidelines (HKPSG) and Technical Memoranda of the relevant Pollution Control Ordinances.

Existing and committed sensitive receivers to be considered in this EIA include :-

- nurseries;
- homes for the aged;
- schools, including kindergarten;
- active recreational activities (for air quality impact assessment only);
- all domestic premises including temporary housing; and
- institutional uses.



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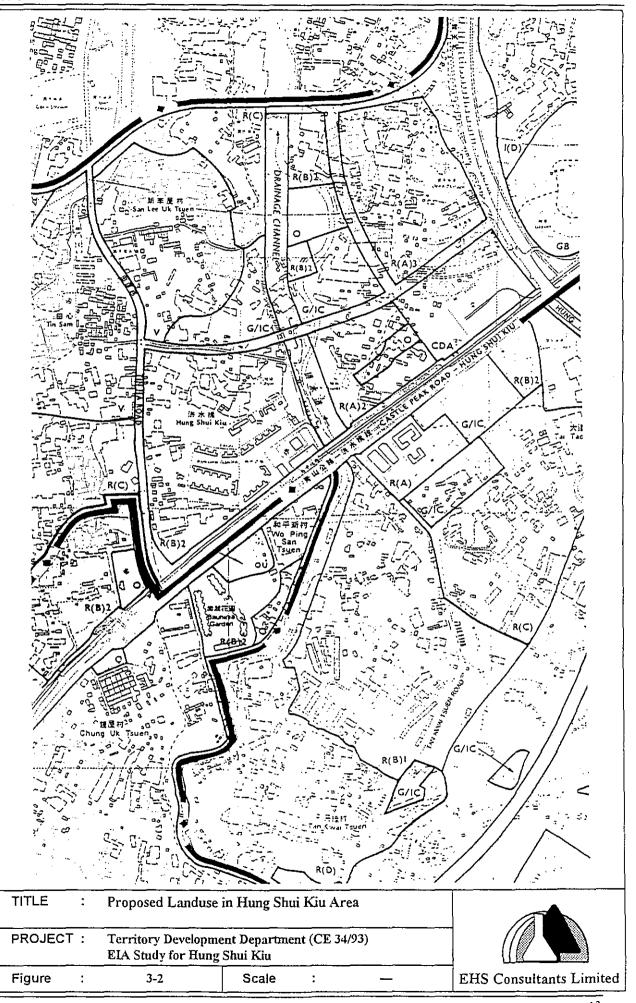
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# 4. AIR QUALITY IMPACT ASSESSMENT

#### 4.1 Introduction

This section contains discussion on the potential air quality impacts arising from the construction and operation of the proposed projects, and will include recommendations for mitigation measures if necessary. The assessment for the construction phase will concentrate on dust emission which is considered to be most appropriate. Impacts from nitrogen oxides (NO<sub>x</sub>), sulphur dioxide (SO<sub>2</sub>), and carbon monoxide (CO) will not be considered because significant emissions are unlikely. On the other hand, vehicular emissions will be considered during operational phase of the road scheme. Air pollutants of concern include CO, NO<sub>x</sub> and Respirable Suspended Particulate (RSP). Both construction and operational air quality impacts are calculated quantitatively using air pollution modelling techniques. Ambient air quality and existing industrial emission impact of the study area will also be established.

#### 4.2 Ambient Air Quality Monitoring

Since the Environmental Protection Department (EPD) does not operate any air quality monitoring stations in the vicinity of the study area, in order to establish the baseline condition, a temporary monitoring station was set up to measure the ambient level of the criteria pollutants in the area. The monitored pollutants include Total Suspended Particulate (TSP), Nitrogen Dioxide (NO<sub>2</sub>) and Carbon Monoxide (CO). The monitoring exercise was carried out from 12th February 1996 to 6th March 1996 at the roof level of Shung Tak Catholic English College located at Hung Shui Kiu as shown in Figure 4-1.

#### 4.2.1 Sampling Methodology

#### Total Suspended Particulate

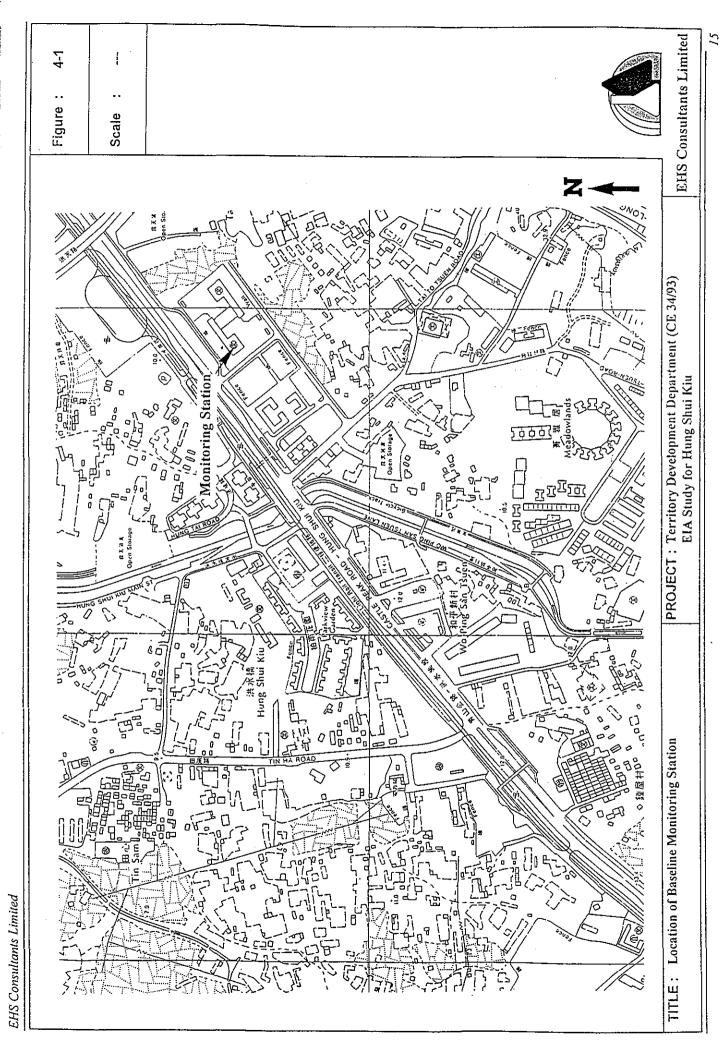
Procedures for measurement of TSP was made reference to Part 50 of Chapter 1 Appendix B of the Code of Federal Regulation of the USA. The mass concentration of TSP in ambient air was determined by a high volume air sampler which drew a measured quantity of air into a covered housing and through a filter during a specified sampling period (1 or 24 hours). The filter was weighed before and after use to determine the net weight gain. The total volume of air sampled was calculated form the measured flow rate and the sampling time.

#### Nitrogen Dioxide

Procedures for measurement of  $NO_2$  was made reference to ASTM Standard D1607. The air sample was drawn through an azo-dye-forming agent by using a constant low-flow air sampler (SKC Model No. 222-4). A red-violet colour was developed after sampling and the intensity of which was measured spectrophotometrically at 550mm.

#### Carbon Monoxide

Real-time Carbon Monoxide levels were monitored quantitatively by Brüel & Kjær Multi-gas Monitor Type 1302. Measurements were carried out during the monitoring period. Its measurement principle is based on photo-acoustic infra-red detection method.



#### 4.2.2 Monitoring Programme

The measurement of NO<sub>2</sub> and TSP was carried out in two phases. The first section (from 13 February 1996 to 28 February 1996) consisted of measurement of both NO<sub>2</sub> and TSP. NO<sub>2</sub> in ambient air was sampled during peak hours. Hourly TSP was measured 4 times per day by one high volume air sampler and continuously for 24 hours by another high volume sampler. Section 2 (from 29 February 1996 to 6 March 1996) involved monitoring of 24-hour average TSP level only. Real-time measurement of CO was carried out on both 9th February 1996 and 27th February 1996.

### 4.2.3 Summary of Results

The monitored ambient hourly and daily average concentration of TSP, CO and NO<sub>2</sub> monitored are summarized in Table 4-1.

Criteria	Time Period - Concentration (µg/m <sup>3</sup> )		
Pollutant	1 hour	Daily	
TSP	86.0	98.0	
CO	681	N.A.	
NO <sub>2</sub>	35.0	N.A.	

Table 4-1 Ambient Air Quality of the Study Area

The monitored 1-hour TSP levels were found to be on the low side when compared with the monitored daily average TSP level. This is probably due to the limited sampling frequency employed (4 times per day only) in measuring 1-hour TSP levels. The monitored average 1-hour TSP levels shall therefore be taken as a reference only.

#### 4.3 Anthropogenic Sulphur Dioxide Concentration

Industrial operations involving the burning of solid and fossil fuel are major emission sources of anthropogenic sulphur dioxide. The concentration and dispersion of  $SO_2$  are related to the type and age of the boiler, as well as the type and quantity of fuel consumption, chimney height and size, and the exit temperature of the emission.

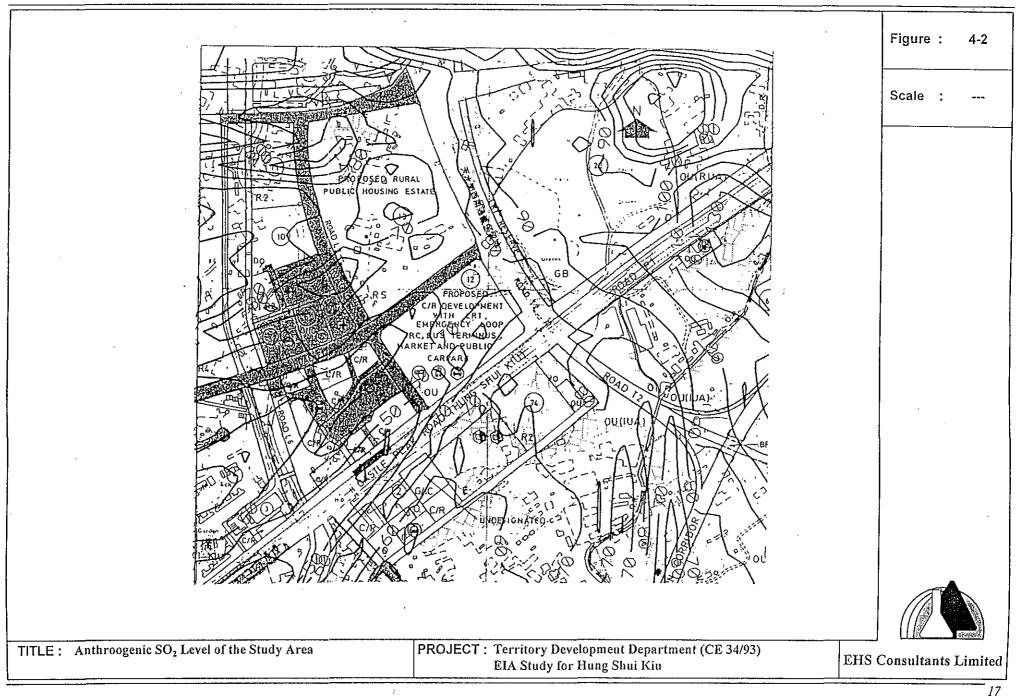
The locations and details of all licensed fuel consuming stacks within 1km radius of the subject site were obtained from the Air Management Group of the EPD. A total of 18 diesel fuel consuming stacks were identified in the proximity of the subject and the data obtained was mostly updated from November 1990 to August 1995.

#### 4.3.1 Computer Modelling and Assessment Results

The dispersion of SO<sub>2</sub> from the identified chimneys was studied to indicate the level of anthropogenic SO<sub>2</sub> of the study area. Modelling was carried out using the software "Industrial Source Complex Short Term (ISCST)" developed by Trinity Consultants Incorporated. This model is based on the principle of Gaussian dispersion and is broadly acceptable to authorities worldwide including the United States Environmental Protection Agency (USEPA) and the Hong Kong Environmental Protection Department (EPD). Meteorological data for the year 1994 from the Royal Observatory's Lau Fau Shan Weather Station was employed in the modelling.

According to the Air Pollution Control (Fuel Restriction) regulation introduced on 25th January 1990 under Regulation 43 of the Air Pollution Control Ordinance, Sulphur content of liquid fuel is not allowed to exceed 0.5% w/w and a viscosity under 6 centistokes at 40°C. This restriction was applied and used as a supposition in the calculation of the emission strength of the stacks.

The predicted highest hourly  $SO_2$  concentration at 1.5m above ground level was superimposed onto survey map of the study area as shown in Figure 4-2. The predicted results were well within the relevant AQO Standards. The ISCST result file is enclosed in Appendix 1 for reference.



### 4.4 Construction Phase Impact

#### 4.4.1 Introduction

The major air quality impact during the construction phase of the proposed projects will be dust emissions from various dust-generating processes. Since all construction activities situated close to existing residential areas can cause some degree of nuisance to the residents, effective mitigation measures must be adopted through the use of statutory powers and implemented by contract requirements overseen by the resident engineer.

The impact of dust on ASRs depends primarily on the drift distance of dust particles which are in turn governed by the initial injection height, the terminal settling velocity, atmospheric turbulence and settling rates of the particulate under both calm and windy conditions. Particles with a size greater than 30µm can be settled within a few metres from source under typical wind conditions. Smaller particles have much slower rates of settling and are therefore more readily affected by wind turbulence.

Emissions from diesel trucks for the haulage of materials and construction plants will contain high percentage of smoke particulate and unburnt hydrocarbons in comparison with petrol driven vehicles. However, as the anticipated traffic volume and the number of construction plants that will result from the construction works are unlikely to be high, no significant impacts on the existing air quality are envisaged.

#### 4.4.2 Identification of Major Dust Sources for Modelling

With the construction activities divided into 5 stages as shown in section 2.2, the major dust emitting processes during the various construction stages are expected to fall into the following main categories.

- excavation/ earthworks for road alignment and site formation;
- vehicle movement on unpaved haul roads on site; and
- material handling.

It is assumed that there is no concrete batching plant and stockpile situated within the work site.

#### Excavation and Earthworks

As the area around Hung Shui Kiu is in general topographically flat, large scale excavations or earthworks will not be required for the proposed projects. It is anticipated that only about 0.5m of top soil along the proposed road network and site formation area will be excavated for road alignment and site formation.

#### Vehicles Movement over Site Roads

Dust generated from the movement of vehicles on the work area could be a major concern. The emission factor for dust emission from vehicle movement is highly variable, but determining factors include vehicle speed and weight, surface silt loading, moisture content, etc.

#### <u>Material Handling</u>

Excavated materials or spoil have to be removed from the construction site by lorries for disposal and significant dust emission could result during the loading and unloading of the material.

#### 4.4.3 Dust Emission Impact Assessment

#### Assessment Criteria

The principal legislation that is relevant to air pollution from construction sites is the Air Pollution Control Ordinance (APCO) (Cap. 311). The whole of the Hong Kong Territory is covered by the Hong Kong Air Quality Objectives (HKAQOs) which stipulate the statutory limits of TSP and RSP and the maximum allowable numbers of exceedance over specific periods. Relevant AQOs for TSP and RSP are extracted from Chapter 9, "Environment", of the Hong Kong Planning Standards and Guidelines (HKPSG) and are tabulated below. Besides, for construction dust, EPD recommends a maximum level of hourly TSP of  $500\mu g/m^3$  at the boundary of any construction site.

	Pollution Concentration Level (µg/m <sup>3</sup> )		
Averaging Time	Total Suspended Particulate	Respirable Suspended Particulate	
1 hour <sup>1</sup>	500*	N.A.	
24 hour <sup>2</sup>	260.0	180.0	
Annual <sup>3</sup>	80.0	55.0	

Table 4-2Hong	Kono Ai	r Oualitv	Ohiectives
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(1) Not to be exceeded more than three times per year.

(2) Not to be exceeded more than once per year.

(3) Arithmetic means.

N.A. Not available

Recommended by EPD

#### Assessment Methodology

The dispersion of dust resulting from the construction of the road scheme has been studied and modelled using the computer software "Fugitive Dust Model (FDM)" developed by Trinity Consultants Inc. The model is based on the principle of Gaussian dispersion and is widely recognized by HKEPD and USEPA for that purpose. The model is designed to predict fugitive dust concentration from point, line, area, and volume sources.

Particulate emission rates for the identified dusty sources were determined based on the US EPA publication *Complication of Air Pollution Emission Factors* (AP-42) and are given in Appendix 2 for reference. Dust sources resulting from excavation and material handling have been modelled as point sources with location, dust generation rate and particulate density provided as inputs whilst dust generation resulting from traffic movement on access roads were considered to be line sources. Average dust density of 2500 kg/m<sup>3</sup> has been assumed in the study.

The distribution of particulate size as shown in page one of *Appendix 3 Typical FDM Result File* for the Dust Emission Impact Assessment has been developed based on available information extracted from "Guide to Rock and Soil Descriptions" issued by the Geotechnical Control Office, Civil Engineering Services Department, Hong Kong, assuming that about 20% of the particulates are respirable with size equal to or less than 10µm.

Meteorological data (wind speed, wind direction, stability class, temperature and mixing height) of the year 1994 from the Lau Fau Shan Weather Station was obtained from the Royal Observatory and used in the modelling. Both the worst case scenario of one hour and twenty-four hour average TSP levels were calculated.

In the absence of a concrete construction programme at this stage of the assessment, a conservative approach has been adopted by assuming that all dusty construction activities would be carried out in parallel over a 12 hour working day to represent the worst case scenario. The working hours will be restricted to 0700 to 1900 hours, due to the requirement for minimising construction noise impact as presented in Section 5 of this report.

#### Background Air Quality for the Impact Assessment

The background dust level for the construction dust impact assessment was made reference to the monitored TSP levels in the study area (see Section 4.2.3) as well as those monitored in EPD's ambient monitoring stations located throughout the Territory. EPD recorded an annual average ambient TSP levels of about  $99.4\mu g/m^3$ ,  $109\mu g/m^3$ ,  $98\mu g/m^3$ , and  $87.2\mu g/m^3$  for Kwun Tong, Sham Shui Po, Tusen Wan and Kwai Chung respectively<sup>1</sup>, with an average of about  $98.4\mu g/m^3$ .

#### Air Sensitive Receivers (ASRs)

Existing village houses and recently built private developments located in close proximity to the proposed road network have been identified as the worst affected locations for the dust emission impact assessment. Representative locations were chosen and inputted into the "Fugitive Dust Model". As most of the sensitive receivers are low-rise buildings, dust level have been modelled at 1.5m, 3.0m and 5.0m above ground. Dust concentrations are expected to drop with increasing height and hence dust concentrations at high level are expected to be insignificant. Identity and location of the selected ASRs are shown in Table 4-3 and Figure 4-3, respectively.

Label	Air Sensitive Receivers	No. of Storeys	
A1	Playground	N/A	
A2	Parkview Garden	4	
A3	Village House	2	
A4	Village House	2	
A5	Coronet Court	10	
A6	Bauhinia Garden	7	
A7	Village House	1	
A8	Church	2	

Table 4-3 Identified worst-hit ASRs for the Dust Emission Impact Assessment

<sup>&</sup>lt;sup>1</sup> Averaged values for the years 1990 to 1994, extracted from "Air Quality in Hong Kong - Results from the Air Quality Monitoring Network" (Years 1990 to 1994) published by the Environmental Protection Department.

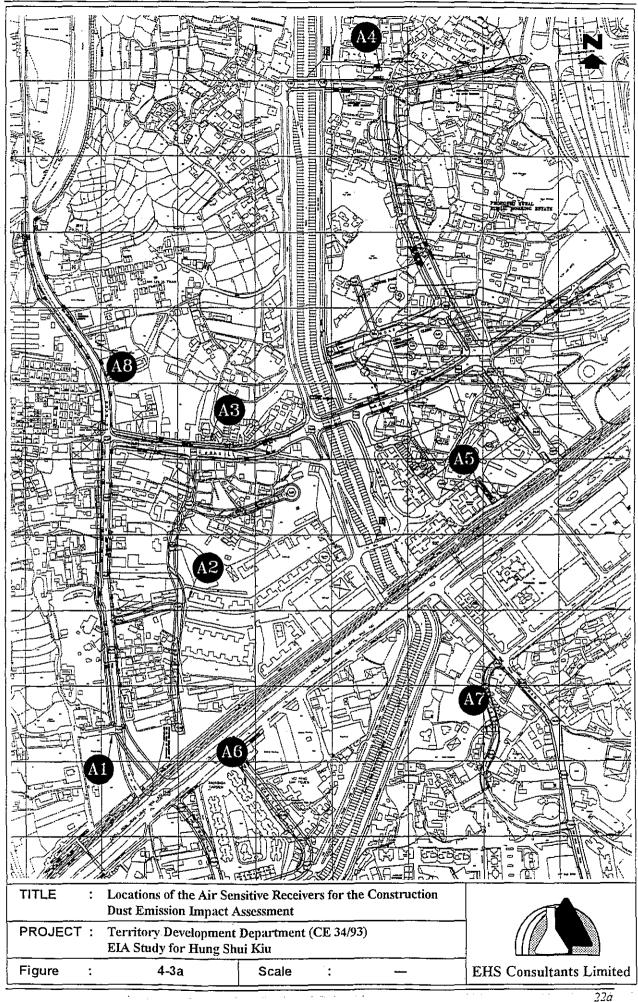
#### Modelling Results

The predicted highest hourly and daily dust level at the selected worst impacted ARSs at 1.5m, 3.0m and 5.0m from ground are shown in Table 4-4. Dust levels exceeding the AQOs are shown in bold. The modelled results indicates that, in the absence of any dust mitigation measure, the air quality criteria will likely be exceeded at some of the selected ASRs during the construction phase. Typical FDM result file is enclosed in Appendix 3 for information.

ASRs	Predicted TSP Concentration (µg/m³) at various distance from ground						
	Highest Hourly			Highest Daily			
	1.5m	3.0m	5.0m	1.5m	3.0m	5.0m	
A1	541	258	138	239	157	106	
A2	1088	235	116	383	156	101	
A3	653	261	129	294	161	103	
A4	542	244	136	225	153	107	
A5	333	191	145	145	130	114	
A6	995	249	121	. 360	156	101	
A7	924	235	124	334	155	103	
A8	888	259	128	328	168	105	

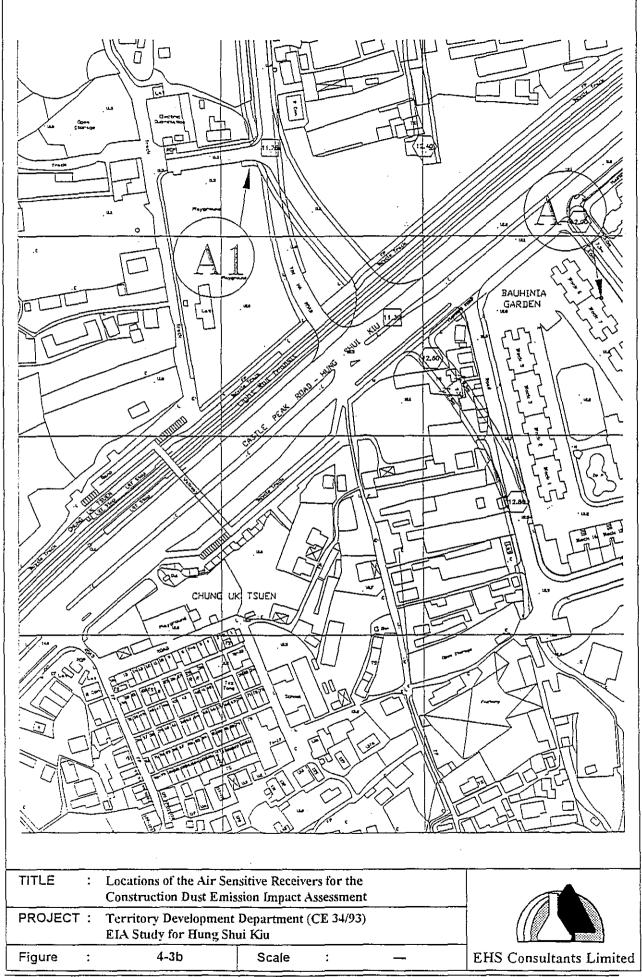
Table 4-4 Predicted TSP Level at the selected ASRs (Without Mitigation Measures)

N.B. : The background TSP of  $98\mu g/m^3$  is included in the results.

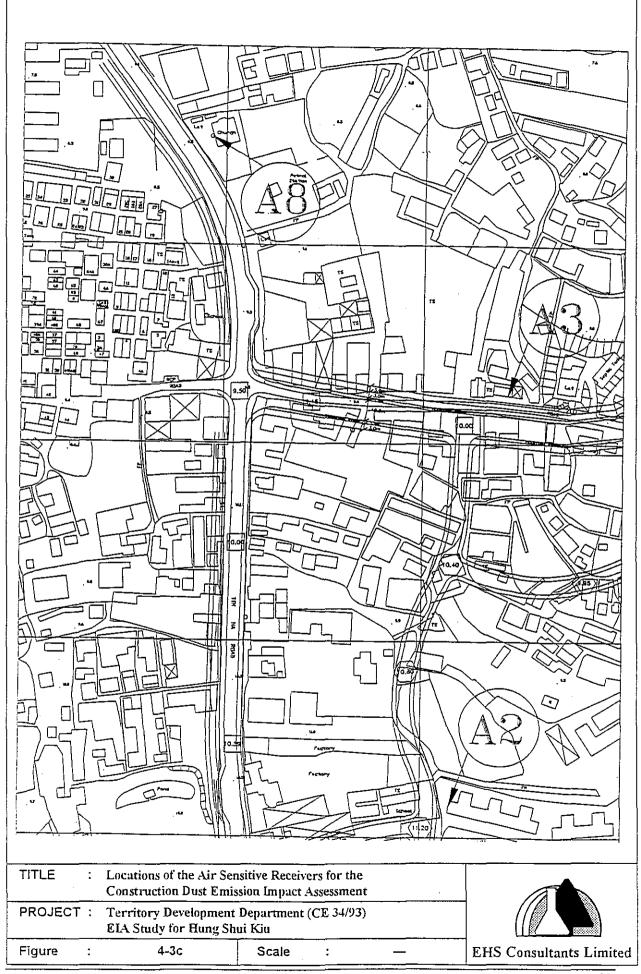


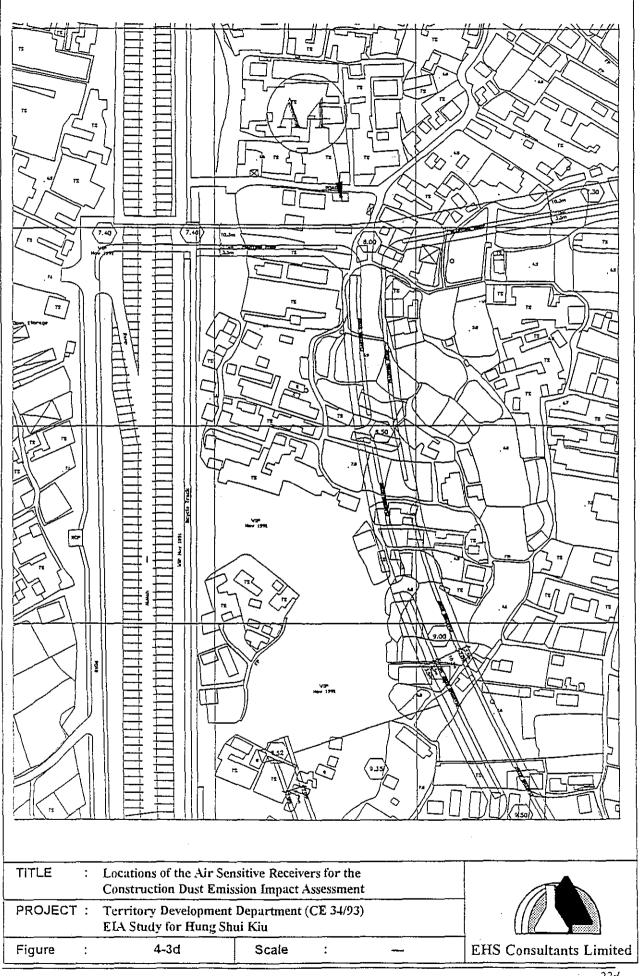
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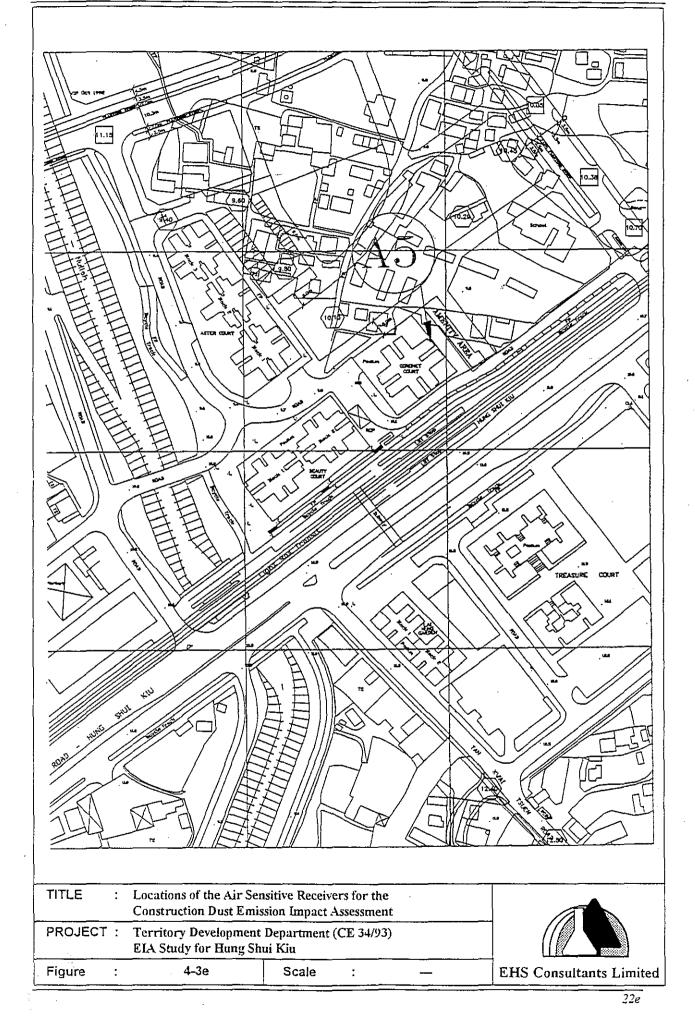
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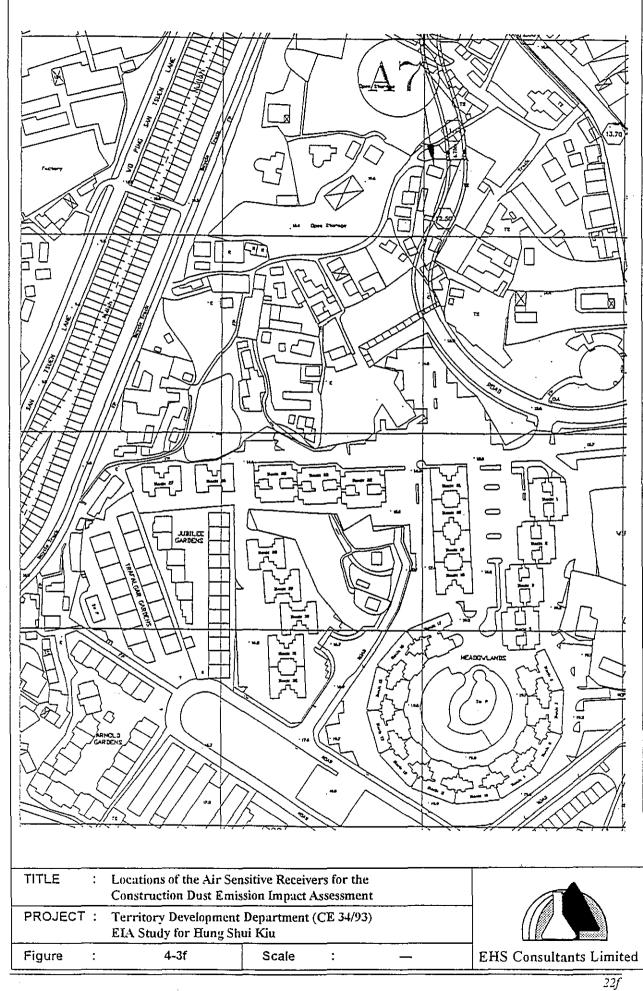


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### 4.4.4 Mitigation Measures

The dust concentrations at the selected ASRs were calculated by assuming the worst case situation with all dusty construction activities occurred concurrently. In reality, the activities are of limited duration and could vary in time. Besides, as mention in section 2.2, a conservative approach has been adopted in the assessment by assuming the concurrent commencement of the two separate projects to be undertaken by the Highways Department and Territory Development Department, respectively. Thus, it is expected that the actual dust level at the ASRs would be lower than the modelled values.

Nevertheless, the modelled results indicates that the construction work would likely to cause an unacceptable dust impact at some of the existing ASRs that are located along the proposed road alignments. In order to mitigate the dust impact, the following dust control measures should be incorporated into the Contract Specifications as part of good construction practice and implemented to minimise dust nuisance to within the acceptable levels.

- frequent watering for particularly dusty construction areas;
- side enclosure and covering where practicable of any aggregate or other dusty material storage piles to reduce emissions;
- all dusty vehicle loads transported to, from and between site locations should be covered by tarpaulin sheets;
- establishment and use of vehicle wheel and body washing stations at exit points of site and public roads, combined with cleaning of public roads where necessary and practical;
- where practicable, routing of vehicles and positioning of dust generating construction plant at maximum possible separation distances from ASRs;
- use of regular watering, with complete coverage, in dry periods to reduce dust emissions from unpaved roads;
- imposition speed limits of 5km/hr for vehicles on access roads; and
- instigation of a programme to monitor the construction process in order to enforce controls and modify methods of work if dusty conditions arise.

With a proper control system, dust emission of material handling and drilling would be reduced by 70%, as stated in US EPA AP-42. Considering a dust control efficiency of 60% for the effective dust control measures recommended above, the mitigated dust levels at the selected ASRs have been calculated and shown in Table 4-5 below. The results indicated that with the implementation of these proposed dust control measures, the dust criteria presented under Section 4.4.3 can be satisfied.

ASRs	Predict	ted TSP Conc	entration (µg/	m³) at various	s height levels f	from ground
ſ		Highest Hour	ly	y Highest Daily		
	1.5m	3.0m	5.0m	1.5m	3.0m	5.0m
Al	263	150	102	154	122	101
A2	482	141	93	212	121	99
A3	308	151	98	176	123	100
A4	264	144	101	149	120	101
A5	180	123	105	117	111	105
A6	445	146	95	203	121	99
A7	416	141	96	192	121	100
A8	402	150	98	190	126	101

Table 4-5 Mitigated TSP levels at the selected ASRs

Note : (i) The background TSP of  $98\mu g/m^3$  is included in the results.

(ii) Mitigated TSP level = unmitigated dust level arising from construction activities  $\times$  0.4 + background TSP level.

#### 4.4.5 Conclusions

Air dispersion model indicated without any effective dust control measures, it is likely that construction dust will pose an unacceptable impact upon the nearby ASRs. Dust mitigation measures, primarily the wetting and covering of exposed dust sources, have been recommended for inclusion in Contract Documents which should be implemented to minimize the dust impacts on the sensitive receivers. In addition, an ambient dust monitoring programme will be set up to oversee the effectiveness of the dust control measures, which is described in the Environmental Monitoring and Audit Report (R718/0696).

# 4.5 Operational Phase Impact

### 4.5.1 Introduction

This section deals with the potential air quality impact of vehicular emissions on potentially affected sensitive receivers in the area, arising from the operational phase of the proposed road scheme. The principal pollutants of concern include carbon monoxide (CO), nitrogen oxides  $(NO_x)$  and Respirable Suspended Particulate (RSP). The impact of vehicular emissions have been modelled using the program "CALINE4" developed by Trinity Consultants, Inc. and is recognized by HKEPD and USEPA for that purpose.

### 4.5.2 Assessment Criteria

Assessment Criteria have been based on the Hong Kong Air Quality Objectives (AQO) for air pollutants given in Chapter 9, "Environment", of the Hong Kong Planning Standards and Guidelines (HKPSG) for air pollution control. The standards used in the present assessment are tabulated below:

Pollutant	Pollutants concentration in µg/m <sup>3</sup>						
		Averaging Time					
	1 hour (i)	8 hours (ii)	24 hours (ii)	1 year (iii)			
со	30,000	10,000	<u>N.A.</u>	N.A.			
NO <sub>2</sub>	300	N.A.	150	80			
RSP	N.A.	N.A.	180	55			

Table 4-6	Hong	Kong A	4ir Oud	alitv (	Obiectives
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(i) Not to be exceeded more than 3 times per year

(ii) Not to be exceeded more than once per year

(iii) Arithmetic means

N.B. Concentrations are to be measured at 298 K and 101.325 kPa (one atmospheric pressure)

## 4.5.3 Vehicular Emission Dispersion Model

The pollutant concentrations at selected Air Sensitive Receivers (ASRs) generated from traffic emissions were evaluated by the computer dispersion model "Caline4" approved by EPD. Typical Caline4.LST files containing all the control parameters, input data and the calculated pollutants concentrations are enclosed in Appendix 5 for reference. The highest 1-hour pollutant's concentration at the day time (stability class D) and the night time (stability class F) are obtained directly from Caline4. The highest 24-hour RSP level would be obtained from the following equation:-

24-hour highest concentration = 2/3 highest 1-hour day-time concentration + 1/3 highest 1-hour night-time concentration

### 4.5.4 Traffic Data

Air pollutant levels experienced by Air Sensitive Receivers (ASRs) due to traffic emissions are related to factors such as engine operational mode, vehicle type and age, road characteristics, and the distance to allow dispersion of the emitted pollutants. The total emission thus depends on the vehicle speed, predicted flow rate and traffic mix. Predicted morning peak traffic flows are used in the modelling for both hourly  $NO_x$  and CO while morning as well as afternoon traffic volume are used in the modelling for daily RSP. Vehicle fleet average emission factor of the pollutants were provided by Vehicular Emission Control Section of EPD and are listed in Table 4-7. Vehicle speed modification factor was not applied in the calculation.

Morning and afternoon peak forecast traffic flows for the year 2011 at the proposed road networks has been predicted by the Project Traffic Consultant, MVA ASIA Limited and used in the assessment. These predicted traffic data are summarized in Appendix 4.

Vehicle Type	Emission Factor (g/km)-EURO2 MODEL		
	NO <sub>x</sub>	СО	RSP
Passenger car (Petrol)	1.321	13.508	0.041
Light Goods Diesel Vehicle	1.540	0.990	0.266
Heavy Goods Diesel Vehicle	7.061	8.410	0.568 .

Table 4-7 Emission Factors of the Vehicular Pollutants Concentration

The following assumptions were adopted throughout the study :

i. NO<sub>x</sub> is a mixture of NO and NO<sub>2</sub>;

ii. 20% of NO<sub>x</sub> is assumed to be NO<sub>y</sub>;

iii. NO<sub>2</sub> was modeled as "Inert Gas"; with a molecular weight of 46g;

v. The proportion of RSP in the vehicular emission is assumed to be 100% of the particulate matter which is, in general, less than 10 µm in the aerodynamic diameter.

# 4.5.5 Meteorological Data and Condition

Pasquill stability class D with wind speed of 1m/s and stability class F with wind speed of 1 m/s were used for the modelling of daytime and night-time results respectively. The average mixing height, according to data from the Lau Fau Shan Weather Station monitoring, was 500m. Wind direction standard deviation of 12° and 5° was applied to stability class D and F respectively. The parameter of worst case wind direction was predicted automatically by the model.

### 4.5.6 Background Air Pollutant Levels

With reference to EPD's monitored ambient dust levels, the Respirable Suspended Particulate (RSP) level is ranging approximately from about one third to almost half that of the TSP concentration. Considering a background TSP level of  $98\mu g/m^3$  (see section 4.4.3), the background RSP concentration for the study has been taken to be  $49\mu g/m^3$ .

Besides, the background CO and NO<sub>2</sub> levels have been taken to be  $681\mu g/m^3$  and  $35\mu g/m^3$  for the study area based on the monitored air pollutant levels given in section 4.2.3.

### 4.5.7 Air Sensitive Receivers

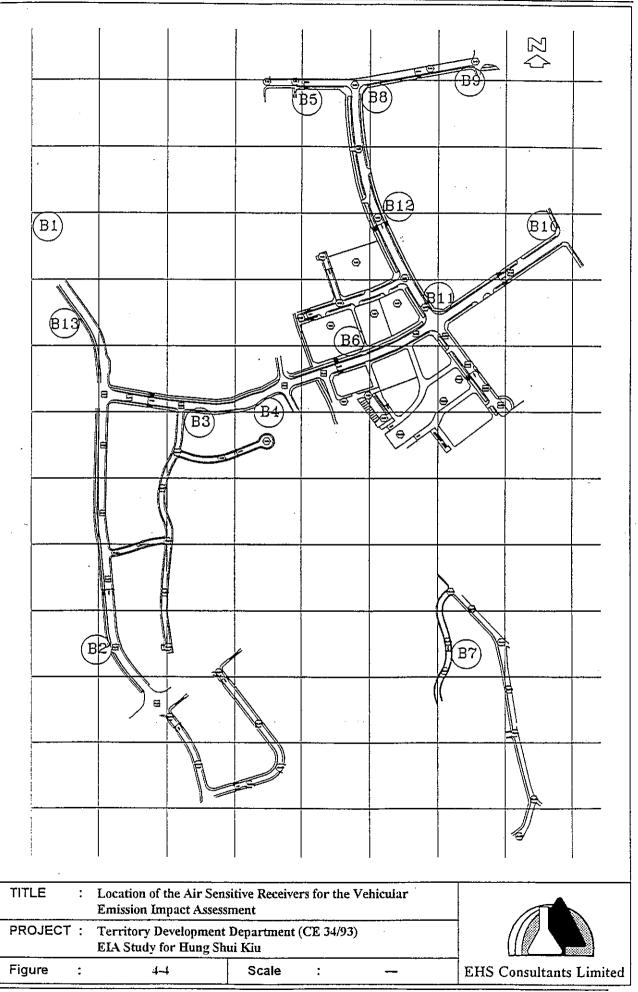
The proposed future land uses in the proximity of the road scheme have been discussed in Section 3. Most of the proposed Commercial/ Residential developments have not yet been planned and hence site layout plans are not available. However, as shown in Figures 2-1 and 5-2, existing and future sensitive receivers will be separated from the proposed road alignments by "designed buffer areas", which will form the footpaths, cycle tracks and roadside planting areas. The buffer distances provided along the kerbsides of road alignments range from 1.6m for L14, 2m for L12, etc. to a maximum of 10m for a section of road D2. The designed buffer distances provided along the selected Air Sensitive Receivers (ASRs) are shown below in Table 4-8 below.

Potential air quality impact resulted from vehicular emission has been assessed by predicting the air pollutant concentrations at different distances away from each road section for each of the selected ASRs B1 to B14. The locations of these ASRs are shown in Figure 4-4.

The modelled results would indicate whether the designed buffer distances along the various road sections will be adequate to ameliorate the potential air quality impact resulted from on-road traffic. The trend of pollutant concentration changes against distance from roads can also be observed. Further setback of existing and future sensitive land uses would be recommended should the assessment results indicate exceedance of the relevant Air Quality Objective criteria.

All selected ASRs have been taken to be situated at 1.5m above ground except for ASRs B5, B6, B8 and B9 near which roadside noise barriers have been proposed (see Figure 5-2 for location of proposed noise barriers). In view of the noise barrier construction, the potential secondary air quality impact on the concerned ASRs was assessed. Similar input parameters and assumption were used as in the open road options. In addition to that, it has been assumed that with the installation of noise barriers, all the traffic pollutants at the barrier sections would be emitted from the top of the noise barriers. The elevation of the road section with proposed roadside noise barrier were therefore set at the elevation of the barrier top. The assessment heights for the ASRs B5, B6, B8 and B9 were also taken to be at the same level so as to give the worst case scenario (i.e. 5m above ground for B5, B8 and B9; 3m above ground for B6). The option "Fill" is set in the Caline4 modelling for the vertical barriers.

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### 4.5.8 Results

The predicted highest 1-hour CO and  $NO_2$  levels, together with the predicted daily average RSP level at the selected locations are listed in Table 4-8 below. Typical Caline4 result files are enclosed in Appendix 5 for reference.

ASR	Assessment point - distance from nearest road kerb	Assessment height <sup>b</sup>	Road section concerned	Designed buffer distance <sup>c</sup>	CO (1 hr)	NO <sub>2</sub> (1 hr)	RSP (24 hr)
B1	2m	1.5m	D1	2m	4688	261	169
	<u>5m</u>	above			3886	223	147
	10m	ground			2398	148	99
B2	2m	1.5m	D1	5.5m .	3199	185	127
	<u>5m</u>	above			2971	148	122
·	10m	ground			2627	148	113
B3	<u>2m</u>	1.5m	L1 &	4.5m (for L1)	1482	73	67
	5m	above	L12	&	1368	73	64
	10m	ground		2m (for L12)	1253	73	63
B4	2m	1.5m	LI	4.5m	1139	73	58
ll II	5m	above			1139	73	57
	10m	ground			1024	73	58
B5	2m	5.0m	D2	5.5m	3428	185	87
	<u>5m</u>	above			2627	148	82
	10m	ground			1711	110	74
B6	_2m	3.0m	LI	10m	2398	110	72
	5m	above			1711	73	65
	10m	ground			1253	73	59
B7	2m	1.5m	L14	1.6m	910	73	53
	5m	above			796	73	53
	_10m	ground			796	73	53
B8	5.5m	5.0m	D2, L2	5.5m	2169	110	76
	10m	above ground			1711	73	71
B9	5.5m	5.0m	D2	5.5m	4802	260	98
	10m_	above ground			3199	148	88
B10	5.5m	1.5m	L1	5.5m	1368	73	62
	10m	above ground			1253	73	60
B11	5.5m	1.5m	L1, L2	5.5m (for both	1482	73	65
	10m	above ground		L1 & L2)	1368	73	62
B12	5.5m	1.5m	L2	5.5m	1253	73	59
	10m	above ground			1139	73	58
B13	2m	1.5m	D1	5.5m	3428	185	130
-	5m	above			2398	148	100
	10m	ground			1940	110	85
			Air	Quality Objectives	30,000	300	180

Table 4-8 Predicted Highest Pollutant Concentration (µg/m<sup>3</sup>) at the selected ASRs<sup>a</sup>

<sup>a</sup>Background air pollutant levels included in the results

(i.e. 681µg/m<sup>3</sup> for hourly CO, 35µg/m<sup>3</sup> for hourly NO<sub>2</sub> and 48µg/m<sup>3</sup> for daily RSP)

<sup>b</sup> Assessment height has been taken to be 1.5m above ground except for B5, B6, B8, B9 near which roadside noise barriers have been proposed (see Section 4.5.7).

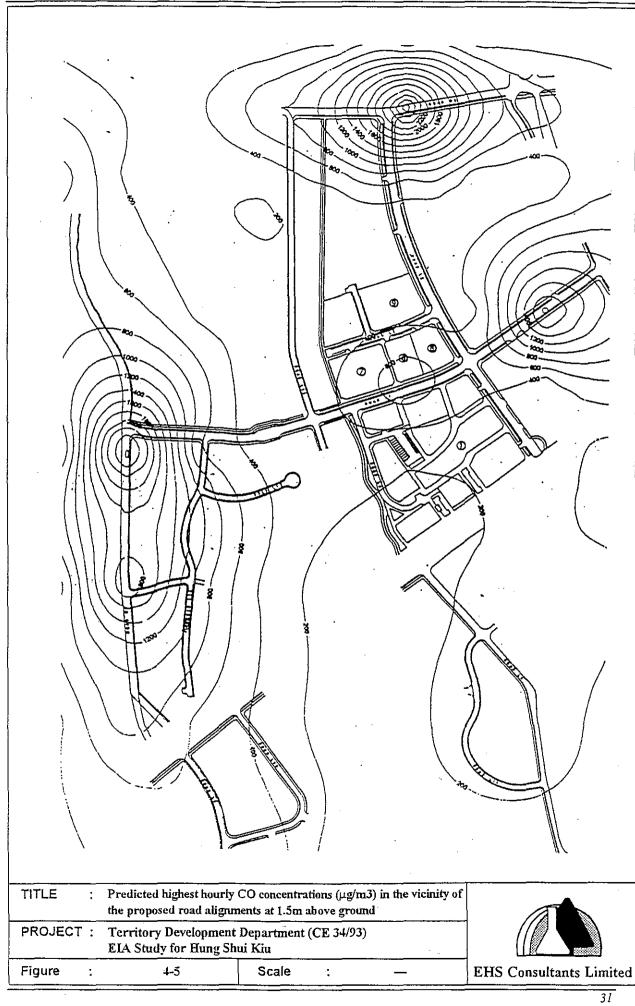
<sup>e</sup> The buffer distances given in this column indicate the width of roadside areas reserved for footpaths, cycle tracks and planting area along road sections adjacent to the selected ASRs.

The modelled air pollutant concentrations are all well within the relevant AQO standards. Therefore, with the designed buffer distances, which will be used as footpaths, cycle tracks and roadside planting areas, air pollutants emitted from future road traffic will not create any unacceptable air quality impact upon the existing and any future sensitive receivers along the proposed roads.

The predicted highest hourly concentrations of CO,  $NO_2$  and daily average concentrations of RSP in the vicinity of the proposed roads are also presented in form of contour maps as shown in Figures 4-5 to 4-7 below.

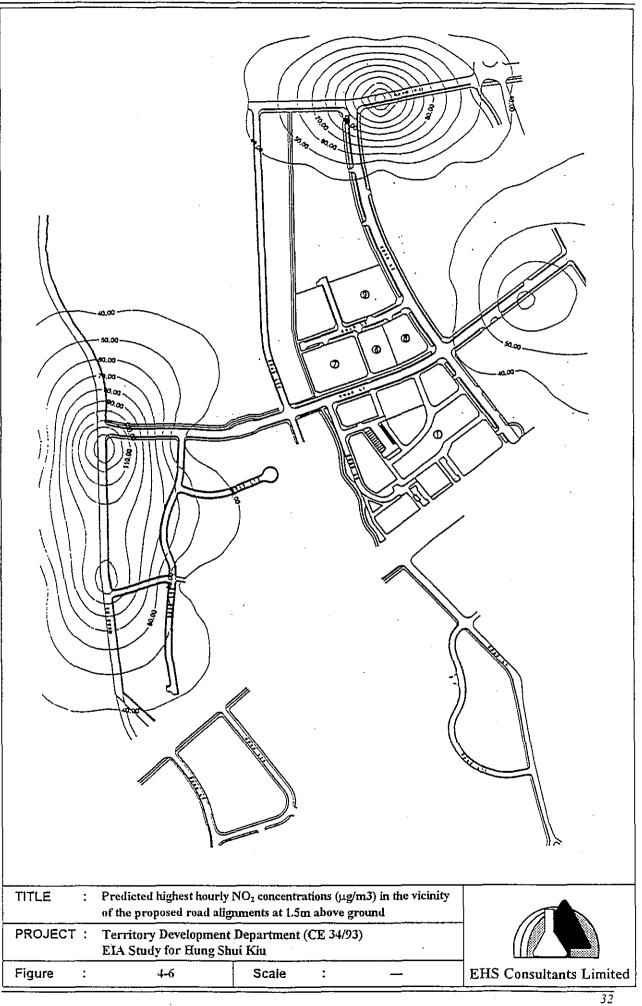
#### 4.5.9 Conclusions

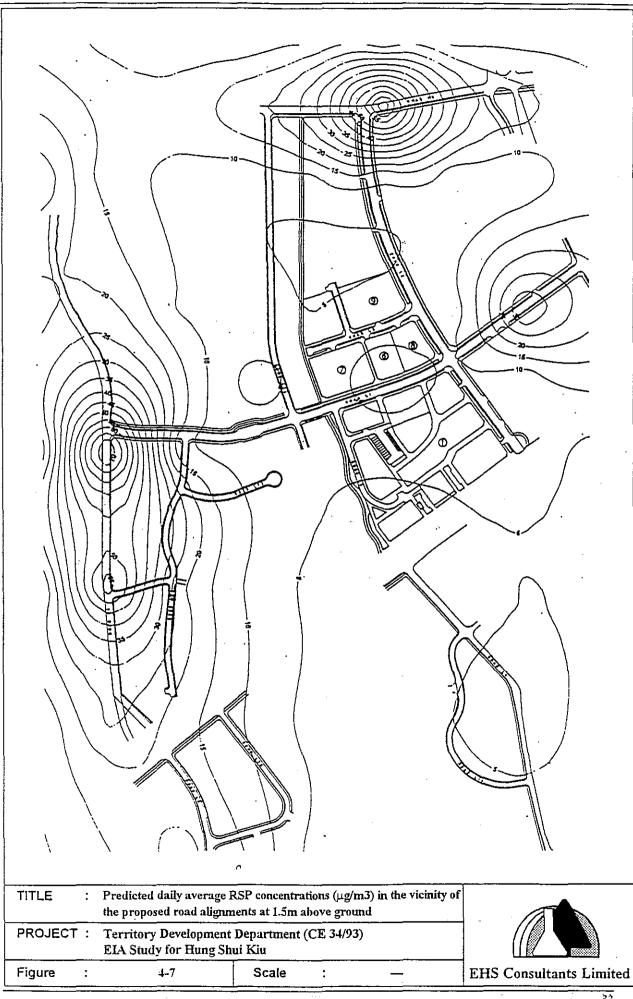
Air quality impact due to vehicular emissions from the proposed road scheme has been quantitatively assessed. Modelled results indicate that with the designed buffer distances along the proposed road alignments, the AQO criteria as stated in the HKPSG will be satisfied at the existing and future Air Sensitive Receivers in the vicinity. The buffer areas are preserved for footpaths, cycle tracks and roadside planting areas.



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# 5. NOISE IMPACT ASSESSMENT

#### 5.1 Introduction

This section describes the noise impact during the construction phase of the proposed projects as well as traffic noise impact from the operation of the proposed road scheme. The boundary of the "Study Area" for the purpose of this Noise Impact Assessment is defined by a distance of 300m from the proposed road alignments. Noise Sensitive Receivers (NSRs) are those as identified under section 3.4.

# 5.2 Construction Phase Impact

### 5.2.1 Introduction

The construction noise impact has been predicted in the following section. It has been made possible by considering a reasonably assumed construction schedule as shown in section 2.2 and is reproduced below for easy reference. The assumed schedule is subjected to change when it is to be carried out in the future. Nevertheless, the assessment can enable a test on the surmountability and hence the possible mitigation measures, if necessary, can be recommended and specified in the future contractual clauses.

Stage	Description
1	Site clearance, excavation and earthworks for alignment and site formation;
2	Percussive piling at foundation locations for nullah crossing plus its formation;
3	Installation of drainage, utilities and manhole plus construction of retaining walls;
4	Formation of road sub-base; and
5	Road surfacing and finishing works

Table 5-1 Construction	Activities a	and Schedules	for the	Proposed Projects
				· · · · · · · · · · · · · · · · · · ·

#### 5.2.2 Assessment Criteria

In Hong Kong, construction noise is controlled under the Noise Control Ordinance (NCO) through a Construction Noise Permit (CNP) system, and the three subsidiary Technical Memoranda, namely:

- Technical Memorandum (TM) on Noise from Construction Work Other Than Percussive Piling, TM(1), which details the assessment procedures on noise from construction work other than percussive piling involving the use of Powered Mechanical Equipment (PME) within "restricted hours", that is between 19:00 to 07:00 hours the next day for Mondays to Saturdays and any time for Sundays and public holidays, for the issuing of CNP.
- Technical Memorandum on Noise from Percussive Piling, TM(2), which details the procedures that generally adopted by the Authority for determining the permitted hours of operation for the issuing of CNP for percussive piling.
- Technical Memorandum on Noise from Construction Work in Designated Areas, TM(3), which governs the noise generated from the use of Specified Powered Mechanical Equipment (SPME) other than Percussive Piling and/or the carrying out of Prescribed Construction Work (PCW) within designated areas.

For construction works other than percussive piling, although the TM1 do not provide control over construction noise generated during normal working hours, a limit of  $L_{eq}(30\text{min})$  75dB(A) is proposed in the "Practice Note for Professional Persons Environmental Consultative Committee (ProPECC) in June 1993. This limit has been applied on major construction projects, and is now generally accepted in Hong Kong. For schools, the recommended noise levels during normal schools days is  $L_{eq}(30\text{min})$  70dB(A) and is lowered to  $L_{eq}(30\text{min})$  65 dB(A) during students examination periods.

For construction noise from percussive piling, a Construction Noise Permit (CNP) has to be applied from the EPD which will specify as a condition the permitted hours of operation and any other conditions that the Authority considers appropriate.

### 5.2.3 Construction Equipment Inventory

As the actual types and number of units of Powered Mechanical Equipment (PME) to be used during the five-stage construction phase are not certain at this stage, typical PME have been assumed with their corresponding sound power levels determined from Table 3 of the TM1. They are divided into groups that are unlikely to be used concurrently within their individual working stages as shown in Table 5-2.

Percussive piling is involved in stage 2 of the construction programme. The locations of the two nullah crossings (PL1 and PL2) at which percussive piling will be required for the two separate projects to be undertaken by the Highways Department and Territory Development Department respectively is shown in Figure 2-2. The most likely Piling Method and Pile Type that will be involved is known to be *Drop Hammer Driving Steel Pile* which has a Sound Power Level of 126dB(A) as specified in Table 2 of TM2. As the two pile locations are of great distance from each other and it is unlikely that percussive piling will take place concurrently at PL1 and PL2 (recalling that piling works at PL1 and PL2 are under two separate projects, with one project started earlier than the other), the assessment of noise from percussive piling has been conducted independently for piling works at each of the two nullah crossings.

### 5.2.4 The Approach and Methodology

### Noise from Construction Work Other Than Percussive Piling

As the construction activities given in Table 5-1 will unlikely be carried out during the restricted hours, the limit of  $L_{eq}(30min)$  75 dB(A) has been taken as the Acceptable Noise Level (ANL) for construction noise assessment for this study.

Construction noise other than percussive piling at noise sensitive receivers (NSRs) was determined and assessed in accordance with the procedures laid down in the TM1. However, before the appointment of a construction contractor, full details of the type and utilisation of construction plant will not be known. All calculations on construction noise other than percussive piling were therefore based on a set of assumptions summarised below :

- (a) Based on the tentative construction programme as shown in Table 5-1, a noise emission inventory of PME to be used and number of units for each of the construction activities are identified as shown in Table 5-2 below;
- (b) Each item of PME is assigned a Sound Power Level (SWL) based on the values given in the TM1;
- (c) Predicted Noise Level (PNL) for each of the five stages of construction activities are calculated by assuming :
  - (i) 100%, 50% or 25% on time of PME (within a typical 30 minutes period), which shall depend on the type of PME concerned and their normal usage frequency in roadworks;
  - (ii) the concurrent operation of the concerned noisy plant only for a particular activity;

- (iii) the PNLs obtained from various construction activities (grouped under different item nos. in Table 5-2) within the same construction stage are compared and the "maximum PNL" is taken to be the PNL for that construction stage.
- (d) Noise levels at each NSR resulted from each of the 5-stage construction activities are then corrected for distance attenuation and the effect of reflection to give a Corrected Noise Level (CNL) at the NSR.

On the other hand, due to the complexity of the proposed projects, it was considered appropriate to assess the construction phase noise impact by sub-dividing the construction area into linear road sections with each constitute one works area. Since each works area is linear in shape with a length to width ratio exceeding 5:1, according to Step 7 of the TM1, only the "dominant portion" of the zones that are closest to the identified NSRs and is having a length to width ratio of 5:1 would be selected for the construction noise impact assessment. As a result of this criteria, the assessment has been based on a conservative approach with the PME considered to be grouped at the nearest notional source position of each works area to the NSRs. This conservative approach will give the worst-case scenario of impact from construction activities.

#### Construction Noise from Percussive Piling

The assessment of noise from percussive piling has been conducted based on the TM2. In general, the methodology used is as follows :-

- (a) Locate the nearest NSRs that may be affected by percussive piling at each of the two nullah crossings (PL1 and PL2) and determine the appropriate Acceptable Noise Level (ANL);
- (b) Calculate distance attenuation to the NSRs from the pile location (taken to be on the piling zone boundary nearest to the NSR) and hence the Predicted Noise Level (PNL);
- (c) Correct the effect due to acoustic reflections to give the Corrected Noise Level (CNL); and
- (d) Determine the appropriate Permitted Hours of Operation for the Percussive Piling by comparing the CNL with the ANL.

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		Work, excavation for road alignmen		<u> </u>	· · · · · · · · · · · · · · · · · · ·
Item	I.D. Code	PME used	Nos. used	SWL, dB(A)	Assumed % on time
1.1	CNP 030	Buildozer	1	115	50
		-		· · · · · · · · · · · · · · · · · · ·	
1.2ª	CNP 023	Breaker, hand-held (pneumatic)	1	117	50
				· · · · · · · · · · · · · · · · · · ·	
1.3	CNP 141	Lorry	1	112	25
	CNP 081	Excavator	1	112	25
Stage <u>2:</u> 1	Percussive pilin	ig for nullah crossing and its formati	on <sup>b</sup>		
Stage 3: I	nstallation of	Underground Drains, Services Utiliti	es & Manhole		
Item	I.D. Code	PME used	Nos. used	SWL, dB(A)	Assumed % on time
3.1	CNP 141	Lorry	1	112	25
	CNP 170	Mobile crane	1	112	25
3.2	CNP 141	Concrete mixer	1	109	50
	CNP 048	Poker	1	113	50
	CNP 102	Generator	1	100	· 100
Stage 4: I	Formation of F	Road Subbase		· · · · · · · · · · · · · · · · · · ·	
Item	I.D. Code	PME used	Nos. used	SWL, dB(A)	Assumed % on time
4.1	CNP 030	Bulldozer	1	115	50
	CNP 141	Lorry	1	112	25
4.2	CNP 185	Road roller	1	108	50
Stage 5: ]	Road Surfacin	g and finishing works			
Item	I.D. Code	PME used	Nos. used	SWL, dB(A)	Assumed % on time
5.1	CNP 021	Bar bender	1	90	25
	CNP 141	Lorry	1	112	25
5.2	CNP 044	Concrete lorry mixer	1	109	25
	CNP 047	Concrete pump	1	109	25
	CNP 170	Poker	1	113	25
5.3	CNP 004	Asphalt paver	. 1	109	50
	CNP 185	Road roller	1	108	50

# Table 5-2 Typical PME to be used in Various Construction Stages

<sup>a</sup> Breaker will only be required at locations involving breaking of concrete (i.e. primarily along Tin Ha Road which will be widened.)

<sup>b</sup> Noise impact from percussive piling in Stage 2 is independently assessed in accordance with the methodology given in Section 5.2.4 Construction noise from Percussive Piling.

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### 5.2.5 Noise Sensitive Receivers

The NSRs that are worst impacted by noise from construction work other than percussive piling and noise from percussive piling are presented below in Table 5-3 and Table 5-4, respectively with their locations shown in Figure 5-1.

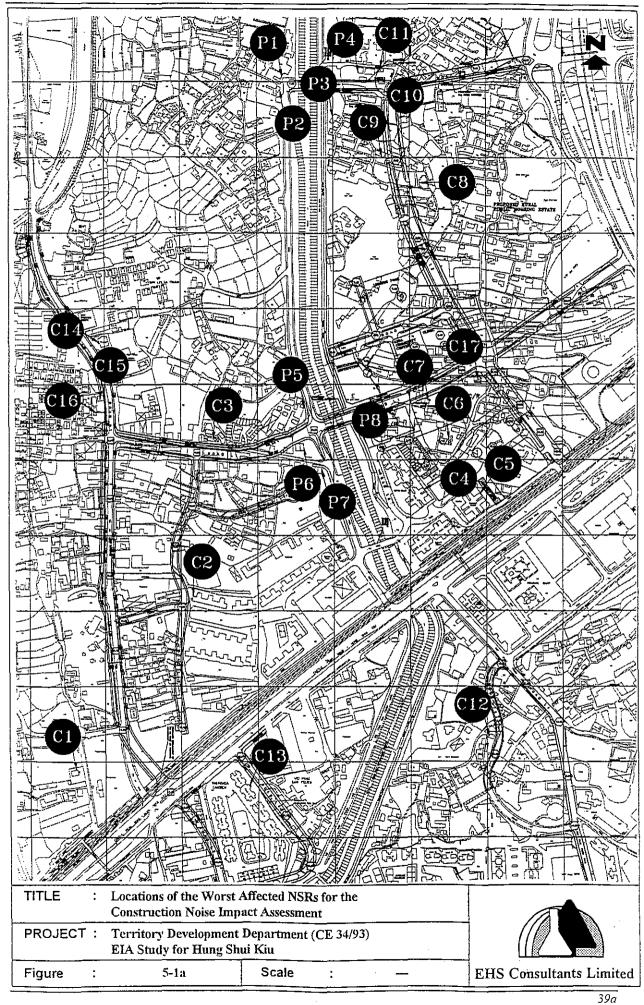
Label	Noise Sensitive Receiver	Distance (m) from Notional Source
C1	Village House	20
C2	Parkview Garden	6.5
C3	Village House	8.5
C4	Aster Court	59
C5	Coronet Court	34.5
C6	Village House	24.5
C7	Village House	20
C8	Village House	• 18
C9	Village House	- 12
C10	Village House	14
C11	Village House	14
C12	Village House	9
C13	Bauhinia Garden	10.5
C14	Church	11.0
C15	Village House	7.5
C16	Kindergarten	18
C17	Kindergarten	16

Table 5-3 NSRs worst impacted by Construction Noise Other Than Percussive Piling

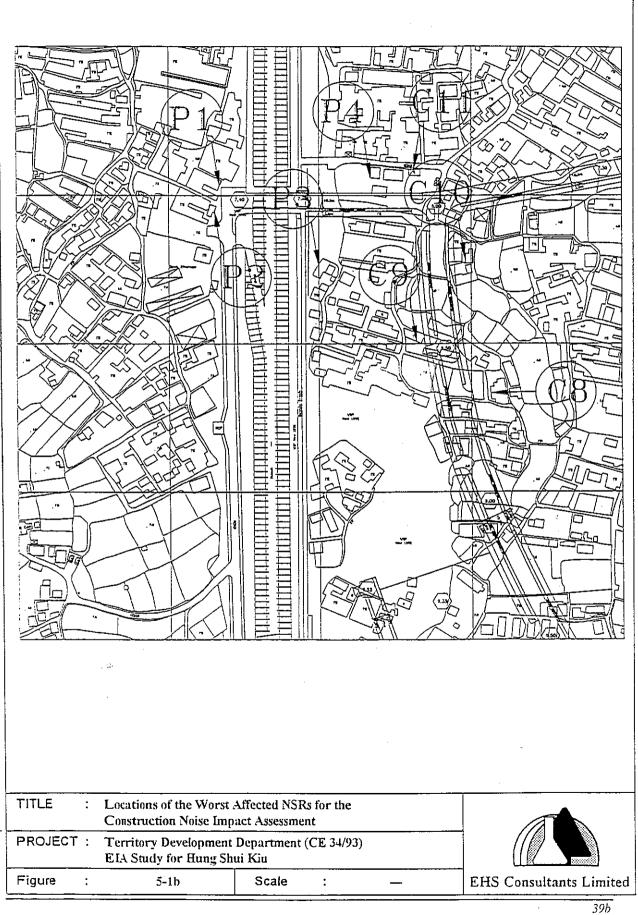
Table 5-4 NSRs worst impacted by Noise from Percussive Piling

Label	Noise Sensitive Receiver	Distance (m) from Notional Source
For Percu	issive Piling at PL1 :	
<b>P</b> 1	Village House	24m
P2	Village House	22m
P3	Village House	44m
P4	Village House	53m
For Percu	issive Piling at PL2 :	
P5	Village House	25m
P6	Village House	39m
P7	Village House	48m
	Aster Court (Block 3)	62m

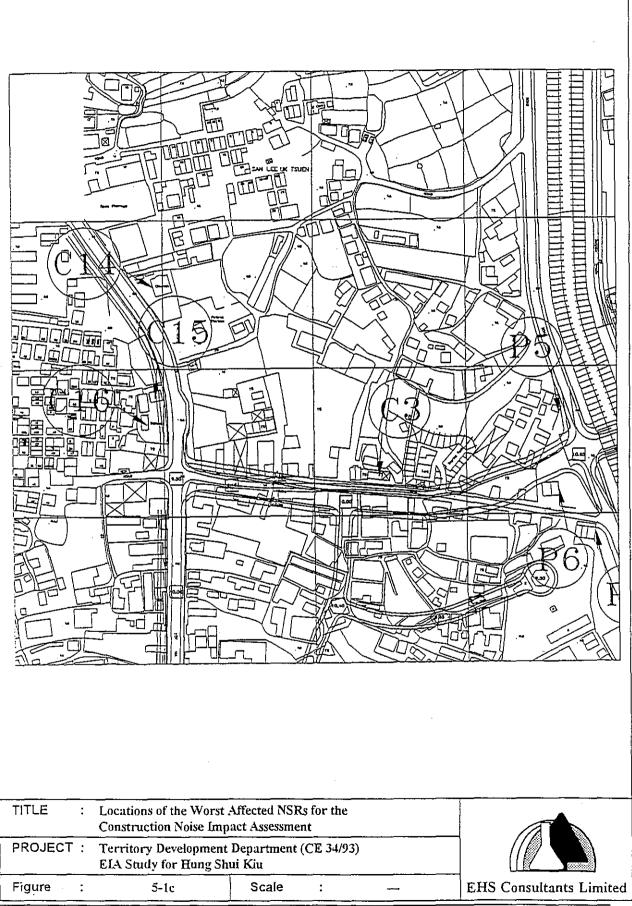
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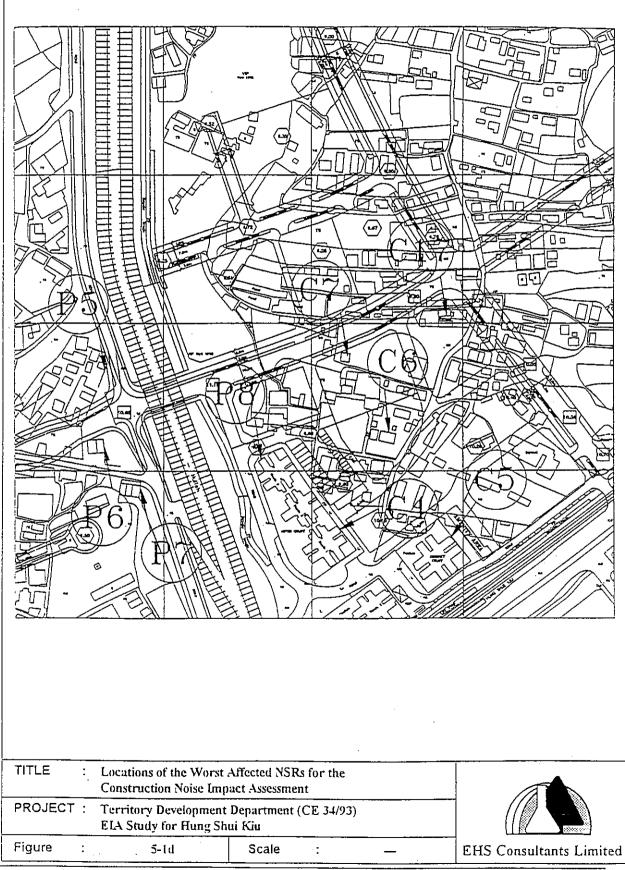


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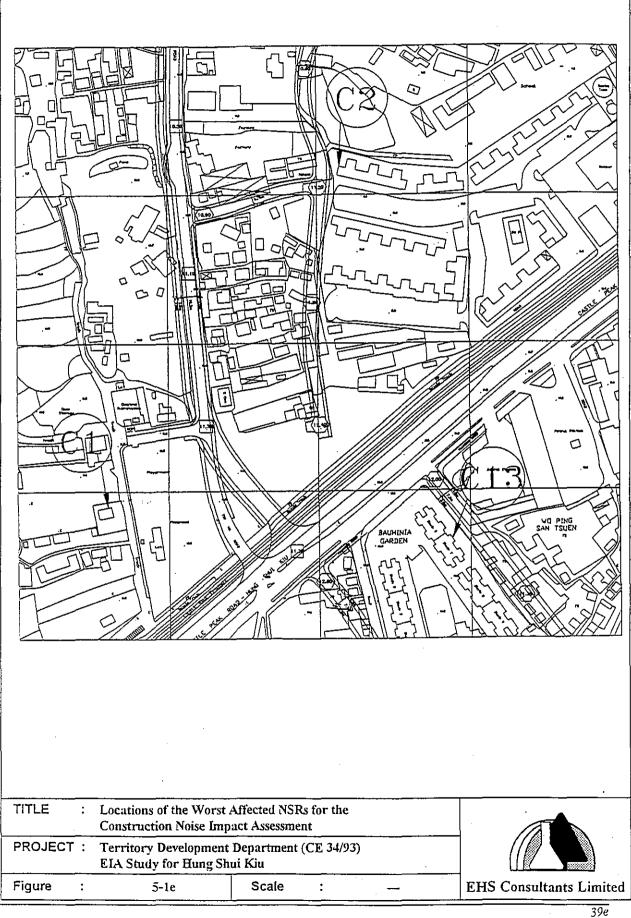
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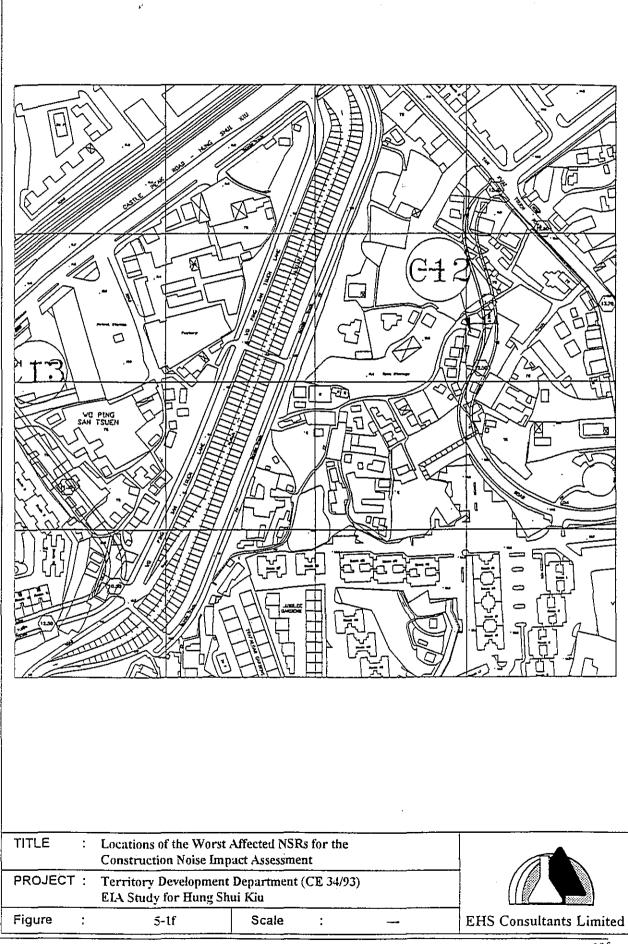
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### 5.2.6 Assessment Results - Noise from Construction Work other than Percussive Piling

#### <u>Un-mitigated Noise Impact</u>

The breakdown of calculation for construction noise impact other than percussive piling at a typical NSR has been given in Appendix 6 while the results obtained for all selected NSRs at various construction stages are summarised below in Table 5-5. Noise levels exceeding the daytime noise limits are shown in bold. Noise impact from the use of hand-held pneumatic breaker has been taken into account in the calculation of noise levels at NSRs C1, C14 to C16 located along Tin Ha Road.

				· · · · · · · · · · · · · · · · · · ·
NSRs	Stage 1	Stage 3	Stage 4	Stage 5
C1	83.0	80.7	81.9	78.5
C2	90.7	90.5	91.7	88.3
C3	88.4	88.1	89.4	85.9
C4	71.6	71.3	72.5	69.1
C5	76.2	76.0	77.2	73.8
C6	79.2	79.0	80.2	76.7
C7	81.0 ·	80.7	81.9	78.5
C8	81.9	81.6	82.8	79.4
C9	85.4	85.2	86.4	82.9
C10	84.1	83.8	85.0	81.6
C11	84.1	83.8	85.0	81.6
C12	87.9	87.6	88.9	85.4
C13	86.6	86.3	87.5	84.1
C14	88.2	85.9	87.1	83.7
C15	91.5	89.2	90.5	87.0
C16	81.9	81.6	82.8	79.4
C17	82.9	82.7	83.9	80.4

Table 5-5 Predicted Corrected Noise Level (No mitigation) at various stages, dB(A)\*

\* Noise impact from percussive piling in Stage 2 is independently assessed in accordance with the methodology given in Section 5.2.4 Construction noise from Percussive Piling.

#### Possible Noise Mitigation Measures

Table 5-4 indicates that noise impact from construction work other than percussive piling during the daytime period will be significantly above the  $L_{eq}(30 \text{ min})$  75dB(A) guideline at most selected NSRs. Noise mitigation measures are required, and the effectiveness of the following forms of mitigation have been considered.

- (i) selecting quiet equipment;
- (ii) use of temporary mobile noise barriers and enclosures;
- (iii) good site practice to limit noise emissions at source

#### (i) Selecting Quiet Equipment

The Contractor shall diligently source equivalent model of plants that are quieter than the standard types given in TM1. The actual benefits that can be achieved by this will depend on the details of the chosen methods of working by the appointed contractors.

It is considered too restrictive to the construction works to specify plants to be used for the construction operations. Instead, it would be preferable and practical to specify plant noise performance specification to apply to the total sound power level of all plants to be used so that the Contractor is allowed some flexibility to select the plants to suit his needs. Nevertheless, plants with lower noise levels than those given in the TM1 for the same type of equipment should be used whenever possible. Examples of SWL for specific silenced PME, which are known to be available in Hong Kong, are given below : -

Bulldozer	100 dB(A) max;
Concrete Pump	105 dB(A) max;
Dump Truck	110 dB(A) max;
Excavator	105 dB(A) max;
Hand-held Breaker	110 dB(A) max;
Lorry	110 dB(A) max;
Mobile Crane	105 dB(A) max;
Poker	110 dB(A) max;

#### (ii) Use of Temporary Mobile Noise Barriers and Machinery Enclosures

Mobile noise barriers can be effective in screening noise from reaching sensitive receivers, particularly for the low-rise buildings in this case. 3m high mobile barriers with skid footing and a small cantilevered upper portion can be located within a few meters of stationary plants and within about 5m of more mobile plant such as buildozers and excavators etc. The barriers should have no openings or gaps and preferably have a superficial surface density of at least 10 kg/m<sup>2</sup>. In addition, certain types of PME such as generators can be totally shielded by machine enclosure giving further noise reduction up to 10 dB(A).

Based on the NSR heights and the site geometry in this case, it is estimated that, if properly used, the barriers/ enclosures can achieve a noise reduction of 10 dB(A) for stationary sources and 5 dB(A) for mobile sources. The noise screening benefit for each plant considered in this assessment is listed as follows :

- Stationary plant 10 dB(A) reduction for mobile crane, bored piling machine, concrete pump, poker, and generator.
- Mobile plant 5 dB(A) reduction for bulldozer, dump truck, excavator, hand-held breaker, lorry, concrete lorry mixer, road roller, bar bender and asphalt paver.

### 5.2.7 Mitigated Noise Impact

The residual impacts after (i) the use of quiet plant only and (ii) the use of quiet plant and mobile noise barriers/ enclosures are shown in Table 5-6 and Table 5-7 respectively for construction stages 1 and 3 to 5.

Table 5-6 Predicted CNL (with silenced PME) at Various NSRs\*

NSRs	Stage 1	Stage 3	Stage 4	Stage 5
C1	76.0	77.8	74.0	77.5
C2	85.0	87.5	83.7	87.3
C3	82.7	85.2	81.4	84.9
C4	65.8	68.4	64.6	68.1
C5	70.5	73.0	. 69.2	72.8
C6	73.5	76.0	72.2	75.7
C7	75.2	77.8	74.0	77.5
C8	76.1	78.7	74.9	78.4
C9	79.7	82.2	78.4	81.9
C10	78.3	80.9	77.1	80.6
C11	78.3	80.9	77.1	80.6
C12	82.2	84.7	80.9	84.4
C13	80.8	83.4	79.6	83.1
C14	81.2	83.0	79.2	82.7
C15	84.5	86.3	82.5	86.0
C16	76.1	78.7	74.9	78.4
C17	77.2	79.7	75.9	79.4

\* Noise impact from percussive piling in Stage 2 is independently assessed in accordance with the methodology given in Section 5.2.4 Construction noise from Percussive Piling.

NSRs	Stage 1	Stage 3	Stage 4	Stage 5
C1	71.0	68.4	69.0	72.5
C2	80.0	78.1	78.7	82.3
C3	77.7	75.8	76.4	79.9
C4	60.8	59.0	59.6	63.1
C5	65.5	63.6	64.2	67.8
C6	68.5	66.6	67.2	70.7
C7	70.2	68.4	69.0	72.5
C8	71.1	69.3	69.9	73.4
C9	74.7	72.8	73.4	76.9
C10	73.3	71.5	72.1	75.6
C11	73.3	71.5	72.1	75.6
C12	77.2	75.3	75.9	79.4
C13	75.8	74.0	74.6	78.1
C14	76.2	73.6	74.2	77.7
C15	79.5	76.9	77.5	81.0
C16	71.1	69.3	69.9	73.4
C17	72.2	70.3	70.9	74.4

Table 5-7 Predicted CNL (with silenced PME & mobile barriers/ enclosures) at Various NSRs\*

\* Noise impact from percussive piling in Stage 2 is independently assessed in accordance with the methodology given in Section 5.2.4 Construction noise from Percussive Piling.

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As can be observed from Tables 5-5 and 5-6, using quiet plant and mobile barriers alone as noise mitigation measures is insufficient to lower noise levels at some of the selected NSRs to meet the assessment criteria for the worst case possible concurrent noisy activities. This is envisaged as some of the worst impacted NSRs are located in close proximity to the proposed road alignments. For the two affected kindergartens represented by NSRs C16 and C17, according to ProPECC PN 2/93, as a last resort, consideration should be given to provide acoustic insulation and air conditioning to these educational premises during the duration of the construction activities.

However, it must be realized that the assessment results can only represent the worst possible cases which theoretically could occur, but in reality are rare or unlikely. This is due to the requirement of assuming the concurrent operation of all concerned noisy plant, with all located at the same nearest notional point of each works area (except for the site formation area, all works areas are long and thin) to the NSR, and to all be fully active at exactly the same time. Even if these levels of construction noise impact, or impacts approaching these could occur, they will be of a very short duration only.

Based on the estimated construction rates for each stage of works, the period when the mitigated noise levels will still be exceeding the established noise guidelines for construction works between 7 a.m. to 7 p.m. have been estimated at each affected NSR. These are set out below in Table 5-8. Sample on calculation is provided in Appendix 7 for reference.

NSRs		Period of Exceed	ance (working day)	
	Stage 1	Stage 3	Stage 4	Stage 5
C1	N.A.	N.A.	N.A.	N.A.
C2	< 1.5 day	< 1.5 day	< 0.5 day	< 1 day
C3	< 1 day	< 0.5 day	< 0.5 day	< 1 day
C4	N.A.	N.A.	N.A.	N.A.
CS	N.A.	N.A.	N.A.	N.A.
C6	N.A.	N.A	N.A.	N.A.
C7	N.A.	N.A.	N.A.	N.A.
C8	N.A.	N.A.	N.A.	N.A.
C9	N.A.	N.A.	N.A.	< 1 day
C10	N.A.	N.A.	N.A.	< 0.5 day
C11	N.A.	N.A.	N.A.	< 0.5 day
C12	< 1 day	N.A.	< 0.5 day	< 1 day
C13	< 0.5 day	N.A.	N.A.	< 1 day
C14	< 1 day	N.A.	N.A.	< 1 day
C15	< 1.5 day	< 1 day	< 0.5 day	< 0.5 day
C16	< 0.5 day	N.A.	N.A.	< 1 day
C17	< 1 day	N.A.	< 0.5 day	< 1 day

Note : N.A. - Not applicable (Noise guidelines for construction noise during 7 am to 7 pm are satisfied)

Nevertheless, the predicted results indicated that additional noise mitigation measures are required. It is envisaged that the implementation of good site practice, avoidance of simultaneous noisy activities and reduction in numbers of plants operating in critical areas close to NSRs will bring about a further reduction in construction noise impact.

#### (iii) Management Approach and Good Site Practice

Good site practice and noise management can significantly reduce the impact of a construction site's activities on nearby NSRs. To provide significant noise reduction on site, the following measures should be followed during each phase of construction :

- the Contractor shall comply with and observe the Noise Control Ordinance (NCO) and its current subsidiary regulation in force in Hong Kong;
- before the commencement of any work, the Contractor shall submit to the Project Manager for approval the method of working, equipment and sound-reducing measures intended to be used at the site;

- the Contractor shall devise, arrange methods of working and carry out the works in such a manner so as to minimise noise impacts on the surrounding environment, and shall provide experienced personnel with suitable training to ensure that these methods are implemented;
- only well-maintained plant should be operated on-site and plant should be serviced regularly during the construction programme;
- machines that may be in intermittent use should be shut down between work periods or should be throttled down to a minimum;
- silencer and mufflers on construction equipment should be utilised and should be properly maintained during the construction programme;
- noisy activities can be scheduled to minimise exposure of nearby NSRs to high levels of construction noise. For example, noisy activities can be scheduled for midday or at times coinciding with periods of high background noise (such as during peak traffic hours);
- noisy equipment such as emergency generators shall always be sited as far away as possible from noise sensitive receivers;
- mobile plant should be sited as far away from NSRs as possible; and
- material stockpiles and other structures should be effectively utilised, where practicable, to screen noise from on-site construction activities.

# (iv) Avoid simultaneous noisy activities and reduction in no. of plants

Other noise mitigation measure such as avoidance of simultaneous noisy activities and a reduction in the numbers of plants operating in critical areas close to NSRs may be required from time to time.

Since it is difficult to provide quantitative predictions of the effect these further mitigation measures will have on noise levels, and it is not possible to identify when will they occur, the effectiveness of the introduced noise mitigation measures have to be monitored during the construction phase. This will enable the contractor to react if the assessment criteria are approached by reducing noise emission at specific areas. Details on noise monitoring requirements, methodology and action plan, etc. are described in the Environmental Monitoring and Audit (EM&A) Report (Report ref.: R718.96).

# 5.2.8 Assessment Results - Noise from Percussive Piling

The predicted CNL at the worst impacted NSRs for noise from percussive piling is presented below in Table 5-9. By comparing the obtained CNL at the worst impacted NSRs with the ANL, the appropriate permitted hours of operation was determined as shown in Table 5-10.

It should be noted that should the assumed piling method and pile type be changed, or additional number of percussive piling units are used, the noise impact from percussive piling should be reassessed to determine the appropriate permitted hours of operation, with the assessment criteria and procedure as stated in the TM2. In any case, however, the predicted "Appropriate Permitted Hours" for percussive piling in this EIA should be considered as a reference only. The actual Permitted Hours of Operation shall be determined by the Authority, with the restrictions on the hours during which percussive piling will be allowed specified in a Construction Noise Permit (CNP), will have to be applied from the Authority for percussive piling activities.

NSRs	Calculation	CNL (dB(A))	ANL (dB(A))	Exceedance = CNL - ANL (dB(A))
For Percu	ssive Piling at PL1 :			
P1	126 - 37 + 3	92	85	7
P2	126 - 37 + 3	92	85	7
P3	126 - 44 + 3	85	85	No exceedance
P4	126 - 45 + 3	84	85	No exceedance
For Percu	ssive Piling at PL2 :	••••••		• • • • • • • • • • • • • • • • • • • •
P5	126 - 38 + 3	91	85	6
P6	126 - 42 + 3	87	85	2
P7	126 - 44 + 3	85	85	No exceedance
P8	126 - 47 + 3	82	85	No exceedance

Table 5-9 Calculated CNL at the worst impacted NSRs

Table 5-10 Appropriate Permitted Hours of Operation for Percussive Piling

Pile Location	Amount by which CNL exceeds ANL	Appropriate hours of operation on any day not being a general holiday
PLI	Between 1 dB(A) to 10 dB(A)	0800 to 0930 AND 1200 to 1400 AND 1630 to 1800
PL2	Between 1 dB(A) to 10 dB(A)	0800 to 0930 AND 1200 to 1400 AND 1630 to 1800

### 5.2.9 Conclusion

The assessment shown that without any effective mitigation measures, noise from construction activities other than percussive piling of the proposed site formation and road works will likely exceed the assessment criteria at most of the selected worst impacted NSRs during weekday hours. Even with the use of silenced PME and mobile barriers/ enclosure as mitigation, it is predicted that the noise impact at some NSRs would still be exceeding the noise guidelines for construction works during the non-restricted hours. Additional mitigation measures such as noise insulation for the affected educational premises and good site practice have been recommended. Recommended construction noise mitigation measures shall be implemented through incorporation into contract specifications.

The effectiveness of the noise control measures shall be monitored by Environmental Monitoring and Audit requirements throughout the construction period which will ensure compliance with the noise criteria by providing feedback to the contractor to provide additional measures such as the reduction of the number of plants working simultaneously within a worksite near to an NSR as required. Detailed EM&A requirements are given in the Environmental Monitoring and Audit Report (R718/96).

Regarding noise impact from percussive piling, a Construction Noise Permit has to be applied from EPD. The appropriate permitted hours of operation has been determined for reference, based upon the likely piling method and pile type that will be used and the location of the nearest sensitive receivers in the vicinity in accordance with the procedure specified in the TM2.

#### 5.3 Operational Phase Impact

#### 5.3.1 Introduction

The potential noise impact after the commissioning of the proposed road scheme is presented in the following sections. With the current rapid pace of development in Hung Shui Kiu, it is envisaged that existing rural features will soon be replaced by new designated land uses. This process will take some time and will still be in progress after the completion of the proposed road scheme. Therefore, both existing and future sensitive receivers have been selected for the Traffic Noise Impact Assessment. A noise model has been employed to investigate the potential traffic noise impact. Effective mitigation measures have been recommended where necessary to reduce noise impacts to acceptable levels.

#### 5.3.2 Noise Assessment Criteria

Noise standards are recommended in the Hong Kong Planning Standards and Guidelines (HKPSG) for planning against noise impact from sources such as road traffic, railway and aircraft. According to the guidelines, the maximum noise level from road traffic, measured in terms of  $L_{10}(1-hr)$  is recommended to be 70 dB(A) at all domestic premises, 65 dB(A) at educational premises and places of public worship, and 55 dB(A) at clinics. The noise standards apply to uses which rely on opened windows for ventilation. These noise standards are used as the assessment criteria for the current study on potential traffic noise impact on existing and future NSRs.

Based on the general principle set down in the memorandum for Executive Council "Equitable Redress for Persons Exposed to Increased Noise Resulting from The Use of New Roads", direct noise mitigation measures shall be implemented wherever practicable to alleviate the noise impact at Noise Sensitive Receivers (NSRs) to meet the noise standards. Regarding existing NSRs, where there would still be residual noise impact exceeding the noise standards after the implementation of all practicable direct measures, indirect measures in the form of noise insulation and the provision of air conditioning should be considered. The following criteria have been used to determine which existing NSRs would be eligible for consideration for indirect measures. An existing NSR would need to meet all of the three criteria in order to be eligible for consideration of indirect measures.

- (i) the predicted overall noise level from the new road together with other traffic noise in the vicinity must be above a specified noise level [e.g. 70dB(A) L<sub>10</sub>(1 hour) for domestic premises];
- (ii) the predicted overall noise level is at least 1.0dB(A) more than the prevailing traffic noise level, i.e. the total traffic noise level existing before the works to construct the road were commenced; and
- (iii) the contribution to the increase in the predicted overall noise level from the new road must be at least 1.0dB(A).

### 5.3.3 Assessment Methodology

The assessment of noise impacts for the proposed roadworks presented here is based on standard acoustic principles. The assessment involved the prediction of the hourly  $L_{10}$  noise levels at the representative worst impacted existing and future Noise Sensitive Receivers (NSRs) generated from future traffic flows on the proposed road alignments. The methodology used were based upon the U.K. Department of Transport's procedure "Calculation of Road Traffic Noise" (CRTN). The predicted noise levels were then assessed by comparing with the noise assessment criteria given under section 5.3.2.

Figure 5-2 shows the design of the proposed road scheme and the existing surrounding environs. Width of roads, footpaths and bicycle paths are marked with road levels given in mPD height. The predicted 2011 A.M. peak hour traffic flows together with the percentage of heavy vehicles given in brackets are also presented. Location of existing NSRs (E1 to E19) and future NSRs (F1 to F22) selected for the noise impact assessment are given in the drawing. Height and location of existing solid fence walls, where present at the NSRs, are also marked.

Typical elevation view of the proposed new roads are shown in Figure 5-3. Planned land use zonings in the study area have been presented in Figure 3-2. Details of important parameters required for the traffic noise impact assessment are further discussed below.

### 5.3.4 Traffic Forecast During Operation

Traffic forecast on the proposed road network for the year 2011 has been predicted by the Project Traffic Consultant, MVA ASIA Limited based on Government's future land-use assumptions. These traffic data used for the traffic noise modeling have been agreed with Transport Department.

Predicted AM peak hour traffic flows in year 2011, together with the percentage of heavy vehicles shown in brackets are set out in Figure 5-2. Other parameters of road design are set out below in Table 5-11.

Road	Road Type	Speed Limit (km/hr)	Road Width <sup>a</sup> (m)	Surface Type
D1 <sup>6</sup>	single two-lane carriageway	50	10.3	Impervious
. D2	single two-lane carriageway	50	10.3	Impervious
L1	single two-lane carriageway	50	10.3	Impervious
L2	single two-lane carriageway	50	10.3	Impervious
L3	single two-lane carriageway	50	7.3	Impervious
L4°	single two-lane carriageway	50	7.3	Impervious
L5	single two-lane carriageway	50	7.3	Impervious
L6	single two-lane carriageway	50	7.3	Impervious
L12	single two-lane carriageway	50	6.75	Impervious
L13	single two-lane carriageway	50	6.75	Impervious
L14	single two-lane carriageway	50 .	6.75	Impervious
L15	single two-lane carriageway	50	7.3	Impervious

#### Table 5-11 Characteristics of the Proposed Road Network

<sup>a</sup> Excluding width of cycle track/ footpath, if any.

<sup>b</sup> Road D1 will be formed by widening of the existing Tin Ha road.

° L4 will be upgraded from the existing Tan Kwai Tsuen Road.

It can be observed from Figure 5-2 that except for the distributors Roads D1 and D2, future traffic flows on the proposed roads are relatively low.

For the proposed widening work at Tin Ha Road (Road D1), as the alignment, number of lanes as well as the speed limit of the road will remain unchanged after widening, and the proposed widening works will only be bringing the existing road to meet current road standards, the widened Tin Ha Road is not considered as a new road for the purpose of noise assessment in this report.

On the same ground, Road L4 upgraded from the existing Tan Kwai Tsuen Road is not considered as a new road as the number of lanes and speed limit on the road will remain unchanged after the project.

The existing traffic flows and percentage of heavy vehicles on Tin Ha Road and Tan Kwai Tsuen Road for the year 1996 have been surveyed by the Project Traffic Consultant. These are set out below in Table 5-12.

Tin Ha Road	AM Peak (Year 1996)	PM Peak (Year 1996)
Total Vehicles / Hour	300	387
% of Heavy Vehicles	37	37
Tan Kwai Tsuen Road	AM Peak	PM Peak
Total Vehicles / Hour	142	106
% of Heavy Vehicles	8	21

Table 5-12 Existing Traffic Flows and % of Heavy Vehicles on the Existing Roads in the Project

### 5.3.5 Noise Sensitive Receivers

Both existing and future noise sensitive receivers (NSRs) and planned noise sensitive land uses within the study area have been represented in the road traffic noise impact assessment. These NSRs and planned noise sensitive land uses are described below in the following subsections.

#### Existing Noise Sensitive Receivers

Existing NSRs situated along the proposed road alignments within the study area have been identified through site visits. Lands for the proposed road alignments and associated footpaths, cycle tracks and planting strips will be resumed and hence existing NSRs lying within these areas have not been selected for the noise impact assessment. Affected NSRs chosen for the assessment include recently built private developments such as Parkview Garden and Meadowlands as well as village houses that are not expected to be redeveloped before the commissioning of the proposed roadworks.

Locations of the selected representative NSRs (E1 to E19) are shown in Figure 5-2. The assessment points have all been taken to be located at 1 m away from the building facade. Noise shielding effects of existing solid fence walls have been taken into account in the assessment for NSRs E4 and E11 to E13. Location and approximate height of these fence walls are also indicated in Figure 5-2.

Identity of the NSRs, with ground level heights, floor numbers and assessment heights, as well as the shortest distance of the assessment points from the kerbside of the concerned roads are given below in Table 5-13. The approximate numbers of existing dwellings, classrooms (for schools) or church that can be represented by each of the selected NSRs are also listed in the Table.

Site investigations have revealed that existing sensitive receivers facing the widened Road D1 are mainly located north of Tin Sum Road. i.e. village houses in Tin Sum Tsuen and San Lei Uk Tsuen. The road section between Tin Sum Road and Castle Peak Road are generally occupied by non-sensitive uses such as industrial buildings and storage facilities, through a few existing village houses (represented by NSRs E16 to E19) have also been identified in the area.

#### Yuen Long - Tuen Mun Corridor - Engineering Works for Hung Shui Kiu; Agreement No. CE34/93

At present, only a few village houses are situated along the northern boundary of Road D2 with the rest of the area occupied by agricultural lands. Located to the southern side of Road D2 is Area 13 which has been designated for development of the proposed rural public housing estate. Construction activities for the proposed rural public housing estate in Area 13 would start before the commissioning of the proposed road scheme (see Appendix 8). As existing NSRs in the area will have been demolished during the operation phase of the Project, future traffic noise impacts on these existing NSRs will not be a concerned. No existing NSRs have therefore been selected within Area 13.

Existing NSRs	NSR	Ground Elevation (mPD)	Floors	Assessment Heights (mPD)	Shortest Distance of Assessment Point from Kerbside of Road	Approximate no. of dwellings (d)/ classrooms (c)/ other NSRs represented
El	Village House	7.3	gf / 1st/ 2nd	8.5/ 11/ 13.5	23.9 m from Road D1	9d
E2	Church	8.5	gf/ 1st	9.7/ 12.7	10.5 m from Road D1	6d + 1 church
E3	Village House	8.5	gf/ 1st/ 2nd	9.7/ 12.2/ 14.7	21.2 m from Road D1	13d
E4	Kindergarten	9.3	gf/lst	10.5/ 12.5	10.7 m from Road D1	2c
E5	Village House	12.0	gf/ 1st/ 2nd	13.2/ 15.7/ 18.2	75.0 m from Road D1	6d
E6	Parkview Garden	11.2	gf/ 1st/ 2nd/ 3rd/ 4th	12.4/ 15.4/ 18.4/ 21.4	6.1 m from Road L12	12d
E7	Village House	6.7	gf/ 1st/ 2nd	7.9/ 10.4/ 12.9	10.8 m from Road D2	12d
E8	Village House	8.5	gf	9.7	30.2 m from L2	2d
E9	Kindergarten	9.8	gf	11.0	13.3 m from Road L1/ L2	2c
E10	Village House	9.8	gf	11.0	6.4 m from Road L1	2d
E11	Bauhinia Garden	13.2	Ist/ 2nd/ 3rd	17.4/ 20.4/ 23.4	10.1 m from Road L15	30đ
E12	Bauhinia Garden	12.7	1st/ 2nd/ 3rd	16.9/ 19.9/ 22.9	10.2 from Road L3	24d
E13	Bauhinia Garden	13.0	lst/ 2nd/ 3rd	17.2/ 20.2/ 23.2	8.9 from Road L15	24d
EI4	Primary School	16.0	gf/ 1st	17.2/ 20.2	3.8 m from Road L4	4c
E15	Meadowlands	19.5	Ist/ 2nd/ 3rd	23.7/ 26.7/ 29.7	41.9 m from Road L4	18d
E16	Village House	11.0	gf/ 1st	12.2/ 14.7	5.7 m from Road D1	4d
E17	Village House	11.4	gf	12.6	3.0 m from Road D1	. ld
E18	Village House	11.2	gf	12.4	12.4 m from Road D1	2d
E19	Village House	11.2	gf	12.4	11.1 m from Road D1	1d

Table 5-13 Identity of the	Selected Existing Representative	NSRs
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N.B. gf = ground floor

#### Future Noise Sensitive Receivers

As described in section 3.2.2, Hung Shui Kiu area will gradually be replaced by new designated land uses. However, as future developments will depend on private initiatives and should take some time even after the commissioning of the proposed road scheme, master layout plans for future developments were not available for the assessment.

The proposed rural public housing estate in Area 13 is still under preliminary planning and no detailed building design has yet been formulated (see Appendix 8 for the letter from the HKHS). Although a very preliminary layout plan of the rural public housing estate has been obtained from the HKHS (also provided in Appendix 8), further discussions with the HKHS have confirmed that major changes would likely be made to the preliminary design layout. As a result, assessment of potential noise impact on the rural public housing estate has only been conducted by modelling noise levels at representative worst-impacted locations.

The assessment of potential traffic noise disturbances on future NSRs has been made possible through a conservative approach. Depending upon the future NSRs involved, noise levels have

been predicted at selected assessment points taken to be situated at 5m or 10m away from the edge of zone boundary along the road carriageways. The 5m or 10m distance separation has been assumed after taking into consideration the planned land uses involved, available site area, typical layout plans for similar developments (e.g. schools), and by making reference to distance separation of existing NSRs from edge of zone boundary (e.g. for village houses).

Based on the designated future land uses, planned NSRs or potentially affected noise sensitive land use zonings have been identified. Representative future NSRs have been selected for the traffic noise impact assessment. Identity and location of the selected future NSRs (F1 to F22) are shown in Table 5-14 and Figure 5-2, respectively. The designated land uses, the assumed maximum building heights, together with the shortest distance of the selected NSRs from the edge of zone boundary along roads are also shown in Table 5-14.

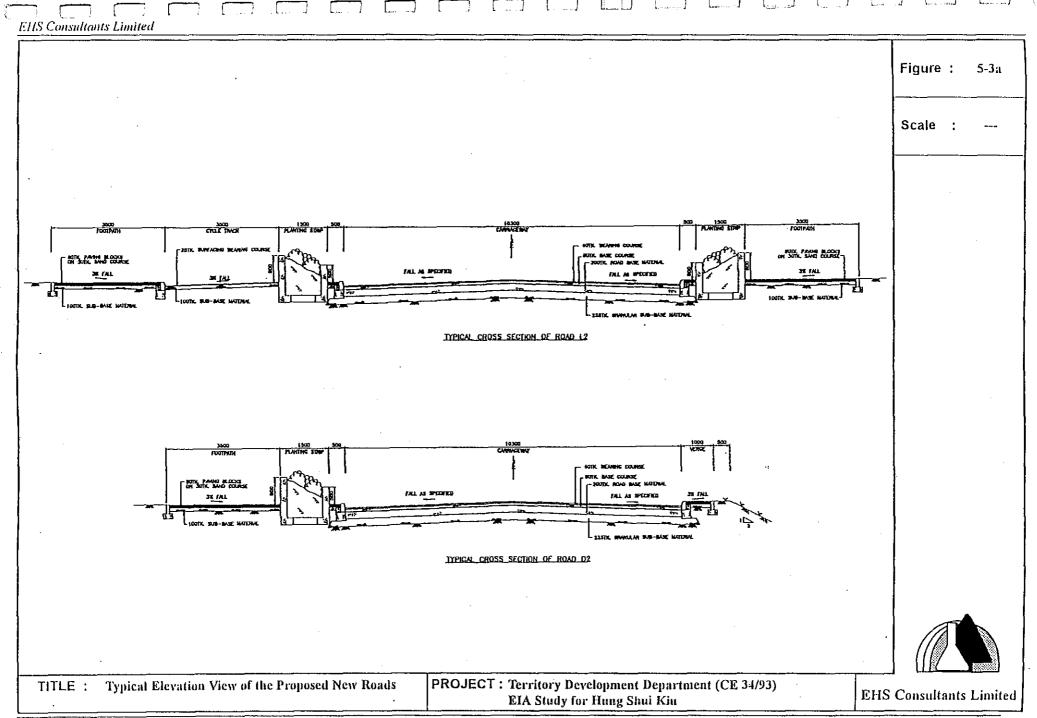
It has been assumed that the selected future NSRs will have a direct line-of-sight to the road of concern and hence the modelled noise levels shall represent the worst case situations. Maximum building heights for residential premises have been assumed based on design parameters/ restrictions given in the relevant outline zoning plans gazetted in June 1996. For the proposed area community centre (which comprises a post office, a children and youth centre, and a nursery), school, and clinic situated in Planning Areas 6, 7 and 8 respectively, the building heights have been assumed based on typical heights of similar facilities.

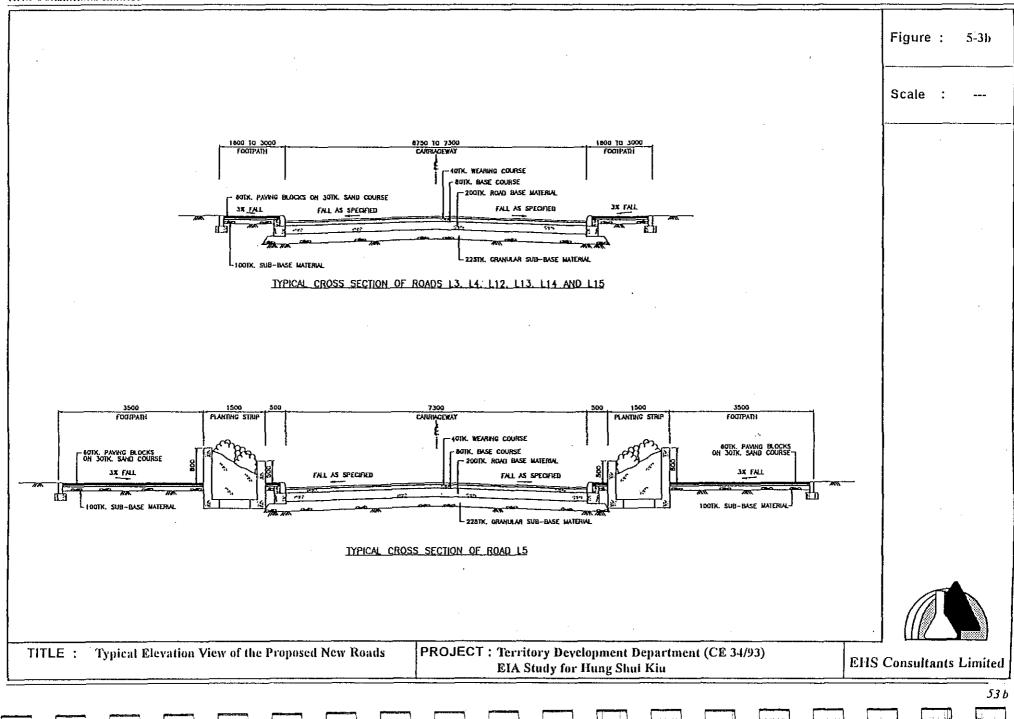
Future NSRs	Future Land Use, Zoning *	Maximum Building Height	Assumed Ground Elevation (mPD)	Assumed Shortest Distance of NSRs from Site Boundary
Fl	Residential (Group B) 2 [R(B)2]	6 storeys over single-storey carport	11.4	бm
F2	Residential (Group B) 2 [R(B)2]	6 storeys over single-storey carport	10.1	5m
F3	Residential (Group B) 2 [R(B)2]	6 storeys over single-storey carport	9.5	5m
F4	Residential (Group B) 2 [R(B)2]	6 storeys over single-storey carport	9.5	5m
F5	Comprehensive Development Area, [CDA]	20 storeys above podium	- 10.1	5m
F6	Residential (Group A) 2 [R(A)2]	12 storeys	10.0	5m,
F7	Residential (Group B) 1 [R(B)1]	4 storeys over single-storey carport	11.9	5m
F8	Residential (Group B) 1 [R(B)1]	4 storeys over single-storey carport	7.2	5m
F9	Rural public housing estate, [R(A)3]	19 storeys above podium	8.0	10m
F10	Rural public housing estate, [R(A)3]	19 storeys above podium	8.0	10m
F11	Rural public housing estate, [R(A)3]	19 storeys above podium	8.0	10m _
F12	Rural public housing estate, [R(A)3]	19 storeys above podium	8.0	10m
F13	Village Type Development, [V]	3 storeys	6.5	10m
F14	Residential (Group B) 2 [R(B)2]	б storeys over single-storey carport	7.4	Śm
F15	Residential (Group B) 2 [R(B)2]	6 storeys over single-storey carport	8.2	5m
F16	Residential (Group B) 2 [R(B)2]	6 storeys over single-storey carport	11.6	5m
F17	Residential (Group C) [R(C)]	3 storeys including carport	11.2	5m
F18	Education, [E] [in Area 7]	7 storeys	8.8	10m
F19	Area Community Centre - with a day nursery [in Area 6]	6 storeys	9.3	10m
F20	Clinic [in Area 8]	3 storeys	9.7	10m
F21	Residential (Group A) 2 [R(A)2]	12 storeys	10.4	5m
F22	Comprehensive Development Area, [CDA]	20 storeys above podium	10.6	5m

Table 5-14 Information on Selected Future NSRs

\* Based on the Ping Shan OZP No. S/YL-PS/1, Tong Yan San Tsuen OZP No. S/YL-TYST/1 and Lam Tei Yick Yuen OZP No. S/TM-LTYY/1 gazetted in June 1996, as well as information provided by the Planning Department.

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## 5.3.6 Predicted Traffic Noise Levels

The predicted noise levels at the selected existing and future NSRs are presented below in Table 5-15 and Tables 5-16, respectively. Noise levels that are exceeding the relevant HKPSG Noise Standards are shown in bold.

Table 5-15 Unmitigated Traffic Noise Level at the selected Existing NSRs in dB(A),  $L_{10}(1-hr)$ 

Existing NSRs	Floors	Assessment Heights Considered (mPD)	Prevailing Traffic Noise Levels	2011 Traffic Noise Levels (No mitigation)	HKPSG Noise Criteria L <sub>10</sub> (1-hr) dB(A)
E1	gf/ 1st/ 2nd	8.5/ 11/ 13.5	69/ 69/ 69	76/ 76/ 76	70
E2	gf/ 1st	9.7/ 12.7	63/ 67	70/ 74	65
E3	gf/ 1st/ 2nd	9.7/ 12.2/ 14.7	68/ 68/ 68 .	75/ 75/ 75	70
E4	gf/ 1st	10.5/ 12.5	60/ 63	69/ 71	65
E5	gf/ 1st/ 2nd	13.2/ 15.7/ 18.2	58/ 58	66/ 66/ 66	70
E6	gf/ 1st/ 2nd/ 3rd/ 4th	12.4/ 15.4/ 18.4/ 21.4/ 24.4	N/A	52/ 52/ 52/ 52/ 52	70
E7	gf/ 1st/ 2nd	7.9/ 10.4/ 12.9	N/A	76/ 76/ 76	70
E8	gf	9.7	N/A	66	70
E9	gf	11.0	N/A	70	65
E10	gf	11.0	N/A	65	70
EII	1 st/ 2nd/ 3rd	17.4/ 20.4/ 23.4	N/A	68/ 69/ 69	70
E12	1 st/ 2nd/ 3rd	16.9/ 19.9/ 22.9	N/A	69/ 70/ 70	70
E13	1st/ 2nd/ 3rd	17.2/ 20.2/ 23.2	N/A	67/ 70/ 69	70
E14	gf/ 1st	17.2/ 20.2	60/ 60	60/ 60	65
E15	1st/ 2nd/ 3rd	23.7/ 26.7/ 29.7	46/ 46/ 46	46/ 46/ 46	70
E16	gf/lst	12.2/ 14.7	70/ 70	78/ 78	70
E17	gf	12.6	74	81	70
E18	gf	12.4	70	76	70
E19		12.4	70	78	70

It can be observed from the modelling results that, except for the existing NSRs (E1-E4, E7, E16) ×to E19) that are lying along Roads D1 and D2 as well as the existing kindergarten (E9) situated along Road L1, the HKPSG noise standards can be met at all other existing NSRs.

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	Future NSRs	Representative Floors	Assessment Height (mPD)	2011 Noise Levels, L <sub>10</sub> (1-hr) dB(A) (No mitigation)	HKPSG Noise Criteria L <sub>10</sub> (1-hr) dB(A)
	F1	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	15.6/ 18.6/ 21.6/ 24.6/ 27.6/ 30.6	80/ 80/ 79/ 79/ 78/ 77	70
1	F2	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	14.3/ 17.3/ 20.3/ 23.3/ 26.3/ 29.3	80/ 80/ 79/ 78/ 78/ 77	70
	F3	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	13.7/ 16.7/ 19.7/ 22.7/ 25.7/ 28.7	66/ 66/ 66/ 65/ 65/ 65	70
/ [	F4	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	13.7/ 16.7/ 19.7/ 22.7/ 25.7/ 28.7	65/ 65/ 65/ 65/ 65/ 65	70
	F5	1st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 20th	14.3/ 20.3/ 26.3/ 32.3/ 41.3/ 56.3/ 71.3	67/ 66/ 65/ 64/ 63/ 62/ 60	70
	F6	1st/ 3rd/ 5th/ 7th/ 9th/ 11th	14.2/ 20.2/ 26.2/ 32.2/ 38.2/ 44.2	69/ 69/ 68/ 68/ 67/ 66	70
	F7	lst/ 2nd/ 3rd/ 4th	16.1/ 19.1/ 22.1/ 25.1	65/ 65/ 65/ 65	70
	F8	Ist/ 2nd/ 3rd/ 4th	11.4/ 14.4/ 17.4/ 20.4	58/ 58/ 58/ 58	70
	F9	1st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19th	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	75/ 75/ 74/ 73/ 73/ 71/ 71/ 71/ 70/ 70	70
	F10	l st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19th	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	76/ 75/ 74/ 74/ 73/ 71/ 71/ 71/ 71/ 70	70
	F11	1 st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19th	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	67/ 67/ 67/ 66/ 65/ 64/ 63/ 63/ 63/ 63	70
	F12	1st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19th	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	70/ 69/ 69/ 68/ 67/ 66/ 66/ 66/ 65/ 65	70
	F13	gf/ 1st/ 2nd	7.7/ 10.2/12.7	77/77/77	70
	F14	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	11.6/ 14.6/ 17.6/ 20.6/ 23.6/ 26.6	75/ 75/ 75/ 74/ 74/ 73	70
	F15	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	12.4/ 15.4/ 18.4/ 21.4/ 24.4/ 27.4	70/ 69/ 69/ 69/ 68/ 68	70
	F16	1 st/ 2nd/ 3rd/ 4th/ 5th/ 6th	15.8/ 18.8/ 21.8/ 24.8/ 27.8/ 30.8	78/ 78/ 77/ 77/ 77/ 76/ 76	70
v	F17	1 st/ 2nd	15.4/ 18.4	79/ 79/ 78	70
	F18	gf/ 1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	10.0/ 13.0/ 16.0/ 19.0/ 22.0/ 25.0/ 28.0	69/ 69/ 69/ 69/ 68/ 68/ 68	65
7	F19	gf/ 1st/ 2nd/ 3rd/ 4th/ 5th	10.5/ 13.5/ 16.5/ 19.5/ 22.5/ 25.5	69/ 69/ 69/ 69/ 69/ 69	65
	F20	gf/ 1st/ 2nd/ 3rd	10.9/ 13.9/ 16.9/ 19.9	69/ 69/ 69/ 69	55
	F21	1 st/ 3rd/ 5th/ 7th/ 9th/ 11th	14.6/ 20.6/ 26.6/ 32.6/ 38.6/ 44.6	64/ 64/ 63/ 63/ 62/ 61	70
	F22	1st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 20th	14.8/ 20.8/ 26.8/ 32.8/ 41.8/ 56.8/ 71.8	70/ 70/ 70/ 69/ 68/ 66/ 65	70

Table 5-16 Unmitigated Traffic Noise Level at Future NSRs in dB(A),  $L_{10}(1-hr)$ 

Without any available master layout plans for future developments in Hung Shui Kiu, assessment on traffic noise impact on future NSRs have been conducted with a conservative approach. All future NSRs have been assumed to have an unobstructed angle of view to the road of concern, and without any noise mitigation measures. Therefore, the predicted noise levels would represent the worst case situations. It is envisaged that the actual noise impacts are much smaller when factors such as building design and orientation and solid fence walls at site boundary could be taken into account in the assessment.

Nevertheless, the results indicated that without any noise mitigation measures, future noise sensitive developments situated along the proposed Roads D1 and D2 will likely be impacted by traffic noise. Noise levels at the nursery (one element of the proposed community centre), school and clinic situated in Area 7, 8 and 9 along Road L1 have also been predicted to exceed the relevant traffic noise standards. Practicable direct mitigation measures are required to minimise potential environmental constraints on future noise sensitive land uses along the road carriageways.

## 5.3.7 Noise Mitigation Measures

The assessment results presented in the above section indicated that the affected NSRs include the followings :

- (i) existing and future NSRs situated along Roads D1 and D2;
- (ii) existing kindergarten located near the junction of L1 and L2;
- (iii) proposed nursery (as one element of the proposed area community centre), school and clinic lying along Road L1.

Effective direct noise mitigation measures shall be incorporated into the proposed projects as far as practicable to protect both existing and future NSRs from future traffic noise impact.

## Noise Mitigation Measures Considered to be Impracticable

Judging from the constraints of the study area, the following direct technical remedies have been carefully considered for Roads D1, D2 and L1 but have been found to be impracticable :

(i) Alternative alignment of the Roads -

Alternative alignment of Roads D1, D2 and L1 is considered impossible owing to the site constraints involved. For example, the alternative alignment of the concerned roads will only shift the traffic noise impact to other existing/ future NSRs located in the area.

(ii) Paving road surface with open texture -

The use of open texture along Roads D1, D2 and L1 is not considered practicable since the speed limit on these roads is only 50 kph. The presence of numerous bus stops along Road D1, together with frequent junctions along all three concerned roads would also result in stop-start traffic, leading to accelerated wear and tear on the friction course and the need of impracticably frequent maintenance.

(iii) Partial or Full Enclosure of Roads -

This option is considered impracticable from the safety viewpoint as "canopy" formed by partial/ full enclosures of the concerned sections of Roads D1, D2 or L1 will inevitably obstruct access by fire engines via turntable ladder/ hydraulic platform to existing or future NSRs situated along the road carriageways in cases of fire. It will also be a source of visual intrusion. In addition, similar to the erection of roadside noise barriers, it may restrict pedestrian access to nearby developments which would require careful design of the road carriageways.

### **Proposed Noise Mitigation Measures**

The erection of roadside noise barriers has been identified to be the only possible option of practicable direct noise mitigation measure along the concerned road carriageways, subject to various identified site constraints. After taking into consideration of these constraints, a noise mitigation proposal in terms of roadside noise barriers has been determined. Location of the proposed noise barriers is shown in Figure 5-2, with further details of these barriers given in Table 5-17. The site constraints which have been considered are described in the following section.

Noise Barrier	Location	Barrier Height	Length	Major NSRs Protected
D2EB-1	Eastbound of Road D2; at 0.6m from kerbside	2m	120m	Existing and future NSRs in designated "V" site
D2EB-2	Eastbound of Road D2; at 0.6m from kerbside	2m	163m	Existing and future NSRs in designated "V" site
D2WB-1	Westbound of Road D2; at interface of planting strip and footpath	5m	70m	Future developments in designated "R(B)2" site
D2WB-2	Westbound of Road D2; at interface of planting strip and footpath	5m	154m	Proposed rural public housing estate in designated "R(A)3" site
L1EB-1	L1EB-1 Eastbound of Road L1; at interface of planting strip and cycle track		106m	Proposed nursery (within area community centre) and school in Areas 6 and 7 respectively
L1EB-2	1EB-2 Eastbound of Road L1; at interface of planting strip and cycle track		63m	Proposed nursery (within area community centre) and school in Areas 6 and 7 respectively

Table 5-17 Details on	Proposed [	Noise Barriers	
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## Various Site Constraints considered in the Development of Noise Mitigation Proposal

(i) Existing run-ins or accesses along Road D1 (widened Tin Ha Road)

Based on the drawing numbered N1078/WD/052 provided by the Highways Department, there are numerous existing run-ins/ accesses along Tin Ha Road that will still have to be maintained even after the proposed road widening works, as advised by District Land Office/ Yuen Long. The locations of these existing run-ins/ accesses (numbered as 1 to 40) are reproduced in Figure 5-2.

With the preservation of these run-ins/ accesses as a pre-condition, and taking into consideration safety factors such as sight-line/ visibility requirements that will have to be met near all possible vehicular ingress/ egress points (1 to 40), as well as the ineffectiveness of the noise reduction effect by erecting solely few and short noise barriers along the road carriageway, as pointed out by the Highways Department, the erection of noise barriers along the widened Tin Ha Road is not considered to be a feasible or an effective noise mitigation option.

(ii) Bus Stops along Road D1

In addition to the existing run-ins/ accesses, there will be four planned bus bays along the widened Tin Ha Road (marked as BB1 to BB4 in Figure 5-2). The erection of noise barriers along their length at kerbside is impossible as this will block passengers from getting on or alighting buses. Although it is possible to overcome this constraint by placing noise barriers behind footpaths, given the impracticability of erecting noise barriers near all existing run-ins/ accesses along Road D1 as detailed above, the provision of noise barriers with short length near bus bays is not considered as an effective noise mitigation measure.

(iii) Existing kindergarten along Road D1

Near the existing kindergarten situated along Road D1 near Tin Sum Road, there will not be sufficient space to allow the provision of the bicycle track section directly in front of the kindergarten. This space limitation excluded the possibility of erecting roadside barrier along the length of the school, should the existing kindergarten is to be preserved.

(iv) Existing vehicular access to villages

Along Road D1, there are the existing Tin Sum Road leading to Tin Sum Tsuen and the side road leading to San Lee Uk Tsuen. These vehicular accesses to villages will have to be maintained. On the other hand, on the northern boundary of the proposed Road D2, there is also an existing vehicular access leading to Shek Po Tsuen from Road D2 which will need to be retained for villagers.

(v) Planting strips along Road D2 and Road L1

There will be areas reserved for "planting strips" along the proposed Roads D2 and L1. In order to allow for the regular irrigation of the plants, the proposed noise barriers, namely L1EB1, L1EB2, D2WB1 and D2WB2 have to be placed at the interface of planting strip and cycle track (for barriers L1EB1 and L1EB2)/ footpath (for barriers D2WB1 and D2WB2) rather than at kerbside.

(vi) Fire

Potential adverse impacts on fire fighting operation in terms of access to existing or future developments along the new or improved roads, access to fire hydrants and radio communication, etc. have been preliminary examined during the development of the direct noise mitigation proposal.

Since vehicular ingress/ egress for the proposed rural public housing estate in Area 13 is planned to be situated along Roads L1 and L2 but not at Road D2, the erection of the proposed noise barrier D2WB2 along the northern boundary of the site would unlikely create an adverse effect on fire fighting. Similarly, for the "R(B)2" site along Road D2, the provision of the roadside barrier D2WB1 would unlikely create any adverse effect on fire fighting operation in the future as vehicular access to the site is reserved along Road L2. An access road to existing and future village houses along the northern boundary of Road D2 is also reserved near the junction of Roads D2 and L2.

Nevertheless, requirements of the Fire Services should be sought prior to the detailed design of the proposed noise barriers as well as any supporting structures that need to be erected adjacent to the noise barriers.

The structural integrity of the barriers shall also be designed such that they will not collapse in case of fire.

### (vii) Traffic/ Engineering

The noise mitigation proposal in form of noise barriers has been devised with consideration of their proximity to the shoulder of the carriageway and effects on line of sight. Thus, kerbside noise barriers are recommended to be situated at 0.6m away from road kerb to satisfy the horizontal clearance requirement specified in Table 3.5.2.1 of the Transport Planning and Design Manual Vol. 2. For the proposed noise barriers to be situated at the interface of planting strips and footpaths/ cycle tracks, the minimum horizontal clearance requirement can also be met.

Near road junctions, relevant sight-line requirements as specified in clause 4.3.8 and diagram 4.3.8.1 of the Traffic Planning Design Manual Volume 2.4 have been considered. Adequate visibility are maintained by eliminating sections of noise barriers that would obstruct the sight-line of drivers. For example, near the existing kindergarten (NSR E9), whereas noise modelling has indicated that a relatively short noise barrier can be erected along the kerbside near the road junction, consideration of the relevant sight-line/ visibility requirement has excluded this option.

## (viii)Visual Impact

The potential impact of the proposed barriers on the existing visual context is generally proportional to the dimension of the structures. As such, it is considered that the potential visual impacts caused by the proposed 5m high roadside noise barriers (along the westbound of a Road D2 section) will be higher than that of the 3m high roadside barriers (along the eastbound of a Road L1 section) which will in turn be slightly higher than that caused by the 2m high noise barriers (along the eastbound of a Road D2 section). With proper design techniques and landscape treatment, it is considered that the visual impact arising from the proposed noise barriers can be softened to acceptable levels. Possible techniques which can be employed are described below :

#### **Functional**

- Durable material with minimum maintenance requirements and costs should be used;
- Construction of supporting structures for the noise barriers should be minimised to avoid disturbance to surrounding open space, pedestrian ways and facilities. This can be achieved by the adoption of high-strength structures and/ or construction of a deeper foundation.

#### <u>Aesthetic</u>

- The proposed colour of the roadside barriers should take into consideration the chromatic "mood" of the local environment. As the proposed barriers are all situated in rural setting, a predominantly green colour scheme for the proposed barriers would be suitable.
- Transparent acrylic sheets (e.g. Plexiglass) can be used in the noise barriers to minimise the visual impact. The proposed barriers would also be screened or decorated with existing plants or additional plantation including trees.

#### (ix) Installation Works

For installation work during restricted hours (1900-0700 hours on Weekdays and all hours on Sundays and Public Holidays), the contractor will need to apply for and obtain a Construction Noise Permit with respect to the Noise Control Ordinance. However, it is unlikely that night time (2300-0700 hours) installation will be acceptable even with mitigation. Transport Department may also require the contractor to carry out a traffic impact assessment which should follow Highways Department Guidance Note RD/GN/021, in order to demonstrate that all proposed traffic management measures during construction will be effective.

### (x) Pedestrian Access

Potential constraints posed by noise barriers on pedestrian crossing along road sections have been evaluated during the development of the noise mitigation proposal. Sufficient space have been retained for pedestrian crossings and the proposed location of the noise barriers is considered feasible.

There will be planned planting strips along the southern boundary of Road D2. As the proposed noise barriers will only be situated behind the planting strips along their lengths, it

is not envisaged that the barriers will create any adverse effect on pedestrian crossings along Road D2. On the same ground, the two noise barriers (L1EB1 and L1EB2) are considered feasible.

#### (xi) Maximum barrier height

For the concerned section of the Local Road L1 with nearby medium rise buildings, it is considered that the erection of tall noise barriers is not practicable. Likely adverse effect of tall noise barriers include visual impact requiring unjustifiable landscape treatment and bad illumination at night. Taking these constraints into consideration, it is considered that the maximum practicable noise barrier height along the local road would be around 3 m.

Regarding the District Distributor Roads D1 and D2, taking into consideration the relatively high future traffic flows on the roads, locations and heights of nearby developments, together with other constraints similar those described above for Road L1, it is considered that the maximum practicable noise barrier height for Roads D1 and D2 would be about 5m.

The provision of noise barriers along Roads L1 and L2 is not effective in protecting the planned clinic site because of its location near the road junctions between Roads L1 and L2 and between Roads L2 and L5, where erection of noise barriers is not feasible because of sightline constraint. The noise barrier along Road L1 has therefore been designed primarily to protect the school site (in Area 7) and the proposed nursery (one element of the area community centre site in Area 6). With the proposed noise barrier along Road L1, the residual noise impact on the clinic site would be approximately 10dB(A) above the HKPSG noise standard of 55dB(A) L10(1-hour). This level of exceedance could not be mitigated by implementation of set back distance. As a last resort, the provision of acoustic insulation and air conditioning for the future clinic in this site is therefore recommended.

With the implementation of the identified direct noise mitigation measures, the mitigated noise levels at the selected existing and future NSRs have been calculated. Except for the four proposed noise barriers to be situated at the interface of planting strips and footpaths/ cycle tracks, the other two noise barriers (i.e. D2EB1 and D2EB2) have been modelled at 0.6m from kerb of road carriageways. The surfaces of all proposed noise barriers (D2EB-1, D2EB-2, D2WB-1, D2WB-2, L1EB-1 and L1EB-2) facing the carriageway should be sound absorptive having an average sound absorption coefficient of 0.55 or above. Table 5-18 set outs the predicted noise levels at all existing and future NSRs after the incorporation of the identified direct mitigation measures into the proposed projects.

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NSR	Floors	Floors Assessment Height (m)		HKPSG Noise Criteria L <sub>10</sub> (1-hr) dB(A)
Et	gf/ 1st/ 2nd	8.5/11/13.5	L <sub>10</sub> (1-hr) dB(A) 76/ 76/ 76	70
-	gf/ lst	9.7/ 12.7	70/ 74	65
E3	gt/ 1st/ 2nd	9.7/ 12.2/ 14.7	75/ 75/ 75	70
E4	gf/lst	10.5/ 12.5	69/ 71	65
<u></u> -	gf/ 1st/ 2nd	13.2/ 15.7/ 18.2	66/ 66/ 66	70
E6	gf/ 1st/ 2nd/ 3rd/ 4th	12.4/ 15.4/ 18.4/ 21.4	52/ 52/ 52/ 52/ 52	70
<b>Ξ</b> 7	gf/ 1st/ 2nd	7.9/ 10.4/ 12.9	69/ 70/ 70	70
	gf	9.7	66	70
<u>5</u> 9	gf	11.0	70	65
E10	gf	11.0	65	70
311	lst/ 2nd/ 3rd	17.4/ 20.4/ 23.4	68/ 69/ 69	70
312	lst/ 2nd/ 3rd	16.9/ 19.9/ 22.9	69/ 70/ 70	70
513	1st/ 2nd/ 3rd	17.2/ 20.2/ 23.2	67/ 70/ 69	70
E14	gf/ 1st	17.2/ 20.2	60/ 60	65
E15	1st/ 2nd/ 3rd	23.7/ 26.7/ 29.7	46/ 46/ 46	70
E16	gf/ 1st	12.2/ 14.7	78/ 78	70
E17	gf	12.6	81	70
518	gf	12.4	76	70
E19	gf	12.4	78	70
Fl	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	15.6/ 18.6/ 21.6/ 24.6/ 27.6/ 30.6	80/ 80/ 79/ 79/ 78/ 77	70
2	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	14.3/ 17.3/ 20.3/ 23.3/ 26.3/ 29.3	80/ 80/ 79/ 78/ 78/ 77	70
F3	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	13.7/ 16.7/ 19.7/ 22.7/ 25.7/ 28.7	66/ 66/ 66/ 65/ 65/ 65	70
F4	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	13.7/ 16.7/ 19.7/ 22.7/ 25.7/ 28.7	65/ 65/ 65/ 65/ 65/ 65	70
F5	lst/ 3rd/ 5th/ 7th/	14.3/ 20.3/ 26.3/ 32.3/ 41.3/ 56.3/ 71.3	67/ 66/ 65/ 64/ 63/ 62/ 60	70
	10th/ 15th/ 20th			
F6	1st/ 3rd/ 5th/ 7th/	14.2/ 20.2/ 26.2/ 32.2/ 38.2/ 44.2	69/ 69/ 68/ 68/ 67/ 66	70
	9th/ 11th			
F7	1st/ 2nd/ 3rd/ 4th	16.1/ 19.1/ 22.1/ 25.1	65/ 65/ 65/ 65	70
F8	1st/ 2nd/ 3rd/ 4th	11.4/ 14.4/ 17.4/ 20.4	58/ 58/ 58/ 58	70
F9	lst/2nd/3rd/4th/5th/7th/10th/ 15th/16th/17th/18th/19th	12.2/ 15.2/ 18.2/ 21.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	60/ 63/ 65/ 69/ 72/ 73/ 72/ 71/ 71/ 71/ 70/ 70	70
F10	lst/ 2nd/ 3rd/ 4th/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19th	12.2/ 15.2/ 18.2/ 21.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	65/ 66/ 67/ 69/ 70/ 73/ 73/ 71/ 71/ 71/ 71/ 70	70
F11	1st/ 3rd/ 5th/ 7th/	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/	67/ 67/ 67/ 66/ 65/ 64/ 63/ 63/	70
	10th/ 15th/ 16th/ 17th/ 18th/ 19th	60.2/ 63.2/ 66.2	63/ 63	
F12	1st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19th	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	70/ 69/ 69/ 68/ 67/ 66/ 66/ 66/ 65/ 65	70
F13	gf/ 1st/ 2nd	7.7/ 10.2/12.7	- 63/ 65/ 69	70
F14	l st/ 2nd/ 3rd/ 4th/ 5th/ 6th	11.6/ 14.6/ 17.6/ 20.6/ 23.6/ 26.6	64/ 66/ 69/ 73/ 73/ 73	70
F15	1 st/ 2nd/ 3rd/ 4th/ 5th/ 6th	12.4/ 15.4/ 18.4/ 21.4/ 24.4/ 27.4	70/ 69/ 69/ 69/ 68/ 68	70
F16	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	15.8/ 18.8/ 21.8/ 24.8/ 27.8/ 30.8	78/ 78/ 77/ 77/ 77/ 76/ 76	70
F17	l st/ 2nd	15.4/ 18.4	79/ 79/ 78	70
F18	gf/ 1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	10.0/ 13.0/ 16.0/ 19.0/ 22.0/ 25.0/ 28.0	60/ 61/ 62/ 64/ 66/ 67/ 68	65
F19	gf/ 1st/ 2nd/ 3rd/ 4th/ 5th	10.5/ 13.5/ 16.5/ 19.5/ 22.5/ 25.5	62/ 63/ 64/ 65/ 67/ 68	65
F20	gf/ 1st/ 2nd/ 3rd	10.9/ 13.9/ 16.9/ 19.9	67/ 67/ 67/ 68	55
F21	1st/ 3rd/ 5th/ 7th/	14.6/ 20.6/ 26.6/ 32.6/ 38.6/ 44.6	64/ 64/ 63/ 63/ 62/ 61	70
:	9th/ 11th			
F22	1st/ 3rd/ 5th/ 7th/	14.8/ 20.8/ 26.8/ 32.8/ 41.8/ 56.8/ 71.8	70/ 70/ 70/ 69/ 68/ 66/ 65	70
	10th/ 15th/ 20th			

Table 5-18 Mitigated Noise Levels at the Selected Existing and Future NSRs.

It can be seem that after the implementation of all identified practicable direct noise mitigation measures, there will still be residual noise impacts at some existing and future NSRs exceeding the HKPSG noise standards. Since all identified practicable direct technical remedies have been exhausted, the residual noise impacts at the affected existing NSRs have to be tested for eligibility for indirect measures in form of acoustic insulation as a "last-resort". For the future NSRs or potentially affected sensitive land uses at which the predicted noise levels will still be exceeding the HKPSG noise criteria after the implementation of all identified direct measures, the "constraints" in terms of the need to provide receiver mitigation measures have been identified.

## 5.3.8 Eligibility for Noise Insulation

It can be seem in Table 5-18 that even after the incorporation of all practicable direct noise mitigation measures, there will still be residual noise impact predicted at most of the selected representative existing NSRs.

Indirect technical remedies in the form of noise insulation and provision of air conditioners for existing residential premises affected by "new" roads should be considered on the merits of the case and presented to the ExCo for consideration. In order to assess the number of dwelling that could be qualified for consideration of noise insulation and provision of air conditioners, the mitigated noise levels at the affected NSRs have been compared with the three noise insulation criteria set out in Section 5.3.2. These are presented overleaf in Table 5-19. It is found that no dwellings will meet the eligibility criteria for insulation after the implementation of the identified direct noise mitigation measures.

Existing educational premises that will still be affected by the proposed projects after the implementation of the identified practicable mitigation measures should be provided with indirect technical remedies in the form of noise insulation and provision of air conditioners to redress the residual impacts. From the assessment results given in Table 5-19, it is found that the existing kindergarten (NSR E9) situated near the junction of Roads L1 and L2 will be the only existing NSR qualified for noise insulation and provision of air conditioners.

## 5.3.9 Constraints on Future Sensitive Land Uses

The mitigated noise levels predicted at the selected future NSRs given in Table 5-18 indicated that after the implementation of all identified practicable direct noise mitigation measures, there will still be residual noise impacts at some future NSRs. These affected future NSRs are located along Roads D1, D2 and L1. In order to satisfy the HKPSG traffic noise standards, there will be constraints on these planned noise sensitive developments or potentially affected noise sensitive land use zoning. These are specified below in Table 5-20.

As discussed in Section 5.3.7, the provision of practicable direct and receiver mitigation measures would unlikely be sufficient to alleviate the noise impact at the proposed clinic in Area 8 to acceptable level. As a "last resort", it is recommended that noise insulation shall be provided at the affected clinic.

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NSR <sup>a</sup>	Floor		Predicted Nois	e Level dB(A)			Indirect technical remedi	es eligibility test	
		Prevailing		Future (2011)		(1)	(2)	(3)	(4)
		Total	Existing Roads	New Roads	Total	[predicted overall noise level > specified noise level] ?	[predicted overall noise level - prevailing traffic noise level >1.0 dB(A)] ?	[noise contribution from new roads > 1 dB(A)] ?	Eligible ? Yes/ No
EI	gf	69	76	negligible °	76	yes [76>70]	yes [76-69>1.0]	no. [0.0<1.0]	No
	lst	69	76	negligible °	76	yes [76>70]	yes [76-69>1.0]	no. [0.0<1.0]	No
	2 nd	69	76	negligible °	76	yes [76>70]	yes [76-69>1.0]	no. [0.0<1.0]	No
E2	gf	63	70	negligible <sup>c</sup>	70	yes [70>65]	yes [70-63>1.0]	no [0.0 <1.0]	No
	1 st	67	74	negligible °	74	yes [74>65]	yes [74-67>1.0]	no [0.0 <1.0]	No
E3	gf	68	75	negligible °	75	yes [75>70]	yes [75-68>1.0]	no [0.0<1.0]	No
	1 st	68	75	negligible °	75	yes [75>70]	yes [75-68>1.0]	no [0.0 <1.0]	No
	2 nd	68	75	negligible °	75	yes [75>70]	yes [75-68>1.0]	no [0.0 <1.0]	No
E4	gf	60	69	negligible °	69	yes [69>65]	yes [69-60>1.0]	no [0.0 <1.0]	No
	lst	63	71	negligible <sup>°</sup>	71	yes [71>65]	yes [71-63>1.0]	no [0.0 <1.0]	No
E9	gf	N.A.	negligible <sup>b</sup>	70	70	yes [70>65]	yes [70-0.0>1.0]	yes [70 >1.0]	Yes
E16	gf	70	78	negligible°	78	yes [78>70]	yes [78-70>1.0]	no [0.0 <1.0]	No
	lst	70	78	negligible <sup> c</sup>	78	yes [78>70]	yes [78-70>1.0]	no [0.0 <1.0]	No
E17	gf	74	81	negligible °	81	yes [81>70]	yes [81-74>1.0]	no [0.0 <1.0]	No
E18	gf	70	76	negligible°	76	yes [76>70]	yes [76-70>1.0]	no [0.0 <1.0]	No
E19	gf	70	78	negligible°	78	yes [78>70]	yes [78-70>1.0]	no [0.0 <1.0]	No

Table 5-19 Eligibility for Noise Insulation at existing NSRs

N.A. - Not applicable.

<sup>a</sup> Existing NSR with mitigated noise level exceeding HKPSG noise standards.

<sup>b</sup>All existing roads are situated at significant distance away from the NSR E9.

<sup>c</sup> As the number of lanes, road alignment as well as the speed limit will remained unchanged on the widened Tin Ha Road, and the proposed widening works simply involve bringing the existing road to meet current road standards, the widened Tin Ha Road (Road D1) is <u>not</u> considered as a new road. Thus, for NSRs E1 to E4 and E16 to E19, as the dominant noise source will originate from the widened Tin Ha Road and all proposed new roads will be situated at significant distances from the NSRs, noise impacts from the new roads are predicted to be negligible.

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Selected Representative Future NSRs	Designated Land Use	Representative Floors	Assessment Height (mPD)	Constraints on Future Noise Sensitive Land Uses	Mitigated Noise Levels L <sub>10</sub> (1-hr) dB(A)
Future Noise Sen	sitive Land Uses	situated along Road D	1		
F1	Residential developments "R(B)2"	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	15.6/ 18.6/ 21.6/ 24.6/ 27.6/ 30.6	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in note 1 to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) the erection of a 4m high solid fence wall at the lot boundary facing Road D1 and (ii) a setback distance of 19m from the lot boundary facing the same road.	64/ 65/ 66/ 67/ 69/ 70 [after incorporation of noise mitigation measures (i) and (ii)]
F2	Residential developments "R(B)2"	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	14.3/ 17.3/ 20.3/ 23.3/ 26.3/ 29.3	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in note 1 to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) the erection of a 4m high solid fence wall at the lot boundary facing Road D1 and (ii) a setback distance of 15m from the lot boundary facing the same road.	68/69/69/69/69/70 [after incorporation of noise mitigation measures (i) and (ii)]
F16	Residential developments "R(B)2"	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	15.8/ 18.8/ 21.8/ 24.8/ 27.8/ 30.8	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in note 1 to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) the erection of a 4m high solid fence wall at the lot boundary facing Road D1 and (ii) a setback distance of 30m from the lot boundary facing the same road.	68/ 68/ 68/ 68/ 69/ 70 [after incorporation of noise mitigation measures (i) and (ii)]
F17	Residential developments "R(C)"	1st/ 2nd	15.4/ 18.4	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in note 1 to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) the erection of a 4m high solid fence wall at the lot boundary facing Road D1 and (ii) a setback distance of 18m from the lot boundary facing the same road.	68/70 [after incorporation of noise mitigation measures (i) and (ii)]

Table 5-20 Constraints on Future Noise Sensitive Land Uses\*

\* Constraints on Future Noise Sensitive Land Uses are restricted to those stated under Column 5 of the Table.

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Note 1 : Examples of noise mitigation measures that can be used at NSRs include, where appropriate, building design and orientation, use of extended podium, setback of buildings, and erection of solid fence wall at site boundary, etc.

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			Table 3-20 (Co	ntinued) Constraints on Future Noise Sensitive Land Uses*	
Future Noise	Sensitive Land Uses.	situated along Road D	2		
F9	HKHS Housing Estate "R(A)3"	1st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19 <sup>th</sup>	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in note 1 to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) a setback distance of 23m from the lot boundary facing Road D2.	59/ 60/ 62/ 66/ 70/ 70/ 70/ 70/ 69/ 69 [after incorporation of noise mitigation measures (i)]
F10	HKHS Housing Estate "R(A)3"	1st/ 3rd/ 5th/ 7th/ 10th/ 15th/ 16th/ 17th/ 18th/ 19 <sup>th</sup>	12.2/ 18.2/ 24.2/ 30.2/ 39.2/ 54.2/ 57.2/ 60.2/ 63.2/ 66.2	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in note 1 to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) a setback distance of 23m from the lot boundary facing Road D2.	
F14	Residential developments "R(B)2"	1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	11.6/ 14.6/ 17.6/ 20.6/ 23.6/ 26.6	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in <b>note 1</b> to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) a setback distance of 16m from the lot boundary facing Road D2.	67/ 67/ 67/ 67/ 68/ 69 [after incorporation of noise mitigation measures (i)]
		situated along Road L			
F18	School "E"	gf/ 1st/ 2nd/ 3rd/ 4th/ 5th/ 6th	10.0/ 13.0/ 16.0/ 19.0/ 22.0/ 25.0/ 28.0	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in <b>note 1</b> to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) a setback distance of 22m from the lot boundary facing Road L1.	60/ 60/ 61/ 62/ 63/ 64/ 65 [after incorporation of noise mitigation measures (i)]
F19	Nursery (within area community centre) "G/IC"	gf/ 1st/ 2nd/ 3rd/ 4th/ 5th	10.5/ 13.5/ 16.5/ 19.5/ 22.5/ 25.5	Implementation of traffic noise mitigation measures at receivers such as a combined use of those measures listed in note 1 to bring about a reduction in noise levels to meet the HKPSG traffic noise standards. As an indicator, the noise standards can be satisfied by (i) a setback distance of 23m from the lot boundary facing Road L1.	62/ 62/ 63/ 63/ 64/ 65 [after incorporation of noise mitigation measures (i)]
F20	Clinic "G"	gf/ 1st/ 2nd/ 3rd	10.9/ 13.9/ 16.9/ 19.9	(i) Provision of noise insulation and air conditioners as a "last resort".	N.A.

Table 5-20 (Continued) Constraints on Future Noise Sensitive Land Uses\*

\* Constraints on Future Noise Sensitive Land Uses are restricted to those stated under Column 5 of the table.

Note 1 : Examples of noise mitigation measures that can be used at NSRs include, where appropriate, building design and orientation, use of extended podium, architectural fins/ balcony, setback of buildings, and erection of solid fence wall at site boundary, etc.

## 5.3.10 Estimated Numbers of NSRs Exceeding Noise Standards

From the predicted 2011 traffic noise levels at the selected representative existing and future NSRs, the total number of dwellings and classrooms (for schools) that will be subject to exceedance of the HKPSG noise criteria before and after the provision of the identified direct noise mitigation measures can be estimated. These are set out below in Table 5-21 for both existing and future classrooms and dwellings. As master layout plans for future developments are not available, please note that the stated numbers for future dwellings and classrooms are only an approximate estimation.

	Approximate No. of Dwellings		Approximate No. of Classrooms in School		
	Existing	Planned	Existing	Planned*	
Without direct mitigation measures	45	420	4	48	
With proposed direct mitigation measures	33	320	4	24	
With proposed direct mitigation measures plus additional noise mitigation measures at future NSRs	N.A.	Nil	N.A.	N.A.	

	Table 5-21 N	umber of NSRs	r exceeding the	noise standards
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N.A. - Not applicable.

\* Although the preliminary layout plan provided by the HKHS include a school near the north-eastern boundary in Area 13, the consultants have been advised by the HKHS that the proposed layout plan is still under preliminary planning and the school could be removed from the plan. The northern boundary of Area 13 has therefore been considered to be occupied by residential units only in the calculation.

Apart from schools and dwellings, after the implementation of all practicable direct noise mitigation measures, it has been predicted that an existing church (NSR E2) along Road D1 would still be impacted by traffic noise. There will also be constraints on the proposed nursery (one element of the area community centre) and clinic in Area 6 and 8 respectively along Road L1.

### 5.3.11 Financial Implications

The costs for erecting noise barriers and the provision of noise insulation for the affected existing kindergarten are estimated as follows. Details of the breakdown are given in Appendix 10.

Tabl	e 5-22	? Costs	for	Noise	Mitigation	М	easures

Mitigation Measure	Costs (HK\$)		
Noise Barriers	10.7 M		
Noise Insulation	0.04 M		

## 5.3.12 Conclusion

Traffic noise impacts from the proposed road scheme on existing and future NSRs have been quantitatively assessed. Predicted results showed that the noise criteria as stated in the HKPSG will be met at most of the selected existing and future NSRs, except for the existing and future ones located along Roads D1 and D2, as well as the existing kindergarten, proposed school, nursery and clinic lying along Road L1.

Practicable direct noise mitigation measures have been identified and recommended for implementation to reduce the potential traffic noise problem on both existing and future NSRs. Where an exceedance is predicted at an existing NSR, the residual noise impacts at the NSR has been tested for eligibility of indirect measures. For future NSRs that will still be subject to noise level exceeding the HKPSG noise standards after the implementation of all identified direct mitigation measures at source, constraints in terms of the need to implement additional noise mitigation measures at receivers have been identified. Possible noise mitigation measures at receivers and orientation, use of extended podium, setback of buildings, and erection of solid fence wall at site boundary, etc.

## 6. COMMENTS ON POLLUTION CONTROL CLAUSES

## 6.1 Introduction

Standard pollution control clauses giving details on noise pollution control, dust suppression, etc. are provided in Appendix B of the study brief. These clauses have been reviewed and modified as shown below to suit specific site situation and constraints. The "revised" Site-specific Pollution Control Clauses is given in Appendix 9 for information.

## 6.2 Comments on Pollution Control Clauses

- (i) The original Section 1 "Avoidance of Nuisance" becomes new Section 1 "General Specification for Environmental Protection" including regulatory requirements and general environmental control clauses.
- (ii) Add after new Section 1, "Environmental Monitoring and Target Levels". This will be the new Section 2.
- (iii) The old Section 2 will become Section 3 with the same title of "Noise Pollution Control". Old clauses are re-arranged and additional ones added under sub-headings of "General Specification", "Non-Statutory Control", "To Provide Sound Level Meter", "Environmental Monitoring and Auditing", "Baseline Monitoring", and "Regular Monitoring".
- (iv) Sub-heading of "General Specification" shall be added before the first clause under Section
   4. "Dust Suppression Measures". Additional clauses "(d)", "(j)", and "(l) to (p)" (new numbering) shall be added.
- (v) Additional clauses shall be added under sub-headings of "To Provide Dust Monitoring Equipment", "Baseline Monitoring", "Regular Monitoring", and "Non-compliance Impact Monitoring".
- (vi) Clauses regarding on-site cement batching facilities shall be arranged under sub-heading of "If on-site cement batching facilities exist, the following clauses shall be deemed applicable:-".
- (vii) Add after the original clause 3(c) a clause regarding measures for unacceptability of plant, equipment or methods of working.
- (viii) Add after the original 3(h) a clause regarding the road surface requirement within the construction site.

- (ix) Add after the original clause 3(I) 2 clauses regarding furnace, boiler or other plant or equipment that might result in air pollution. Add after this 3 clauses regarding blasting, earthworks and soilworks that could result in dust generation.
- (x) Add after the original clause 3(1) a clause regarding the cleaning of concrete batching plant.
- (xi) While the Original Section 5. & 6. are applicable to the Hung Shiu Kiu project, the Original Section 7. & 8. shall be omitted as there will be no dredging work.

## 7. ASSESSMENT SUMMARY AND CONCLUSION

This EIA has assessed the potential environmental impacts associated with the construction and operation of the proposed roadworks to be carried out under two separate projects. Areas assessed include dust emission and noise impacts during the construction phase, vehicular emission and traffic noise impacts during the operation of the proposed roadworks.

## 7.1 Air Quality Impacts

In the absence of effective dust control measures, the construction works is expected to introduce an unacceptable dust emission impact upon the existing sensitive receivers which are scattered around the project area. With the implementation of effective control measures, the impact will be reduced to within acceptable levels. Environmental pollution control clauses are recommended which should be implemented through contract clauses. An Environmental Monitoring and Audit (EM&A) report (R718/0696) has been prepared to oversee the effectiveness of the proposed dust control measures.

The potential air quality impacts resulted from the operation of the proposed road network has been quantitatively assessed. Calculations show that with the provided buffer distances along the kerbsides of the carriageways, which range from a minimum of 1.6m for L14 to a maximum of 10m for a section of road L1, vehicular emission will not pose an unacceptable impact upon the existing and future sensitive receivers located in the area.

## 7.2 Noise Impacts

Noise from construction works other than percussive piling is expected to result in exceedance of the noise criteria at most of the sensitive receivers. With the use of silenced powered mechanical equipment and mobile barriers/ enclosure as mitigation measures, it is found that noise levels would still exceed the established guidelines at a number of NSRs. The period during which the noise guidelines will be exceeded has been predicted at each affected NSRs and additional noise mitigation have been proposed to further reduce the noise impacts. For the two affected educational premises, according to ProPECC PN 2/93, as a last resort, consideration should be given to provide acoustic insulation and air conditioning to these educational premises during the duration of the construction activities. Implementation of the recommended noise mitigation should be checked by EM&A procedures as detailed in the prepared EM&A report (ref.: R718/0696). Construction noise arising from percussive piling has also been assessed with the appropriate permitted hours of operation determined. A construction noise permit shall be applied from the Authority before the operation of percussive piling activities.

The Traffic Noise Impact Assessment indicated that traffic noise will not be a main concern for most of the proposed road alignments except for Roads D1 and D2 where the predicted traffic volume will be relatively high. Relatively sensitive land uses, which include an existing kindergarten, a proposed school, a nusery (one element of an area community centre) and a clinic lying along Road L1, have also been predicted to have noise levels exceeding the relevant noise standards.

Direct noise mitigation measures in the form of roadside barriers have been recommended as far as practicable for alleviating the potential noise impact on affected existing and future NSRs identified along the road carriageways. After the implementation of all practicable direct mitigation measures at source, there would still be residual traffic noise impacts on NSRs. Residual impacts at existing NSRs have been tested against the noise insulation criterion. Constraints on future NSRs have been specified.

## Appendix 1

## Existing Industrial Emission Impact ISCST Result File

ISCST - (DATED 90346)

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IBM-PC VERSION (2.05) (C) COPYRIGHT 1990, TRINITY CONSULTANTS, INC. SERIAL NUMBER 7303 SOLD TO EHS CONSULTANTS RUN BEGAN ON 04-01-96 AT 18:30:46

*** HUNG SHUI KIU (CHIMNEYS' EMISSION)		***
		_
CALCOLATE (CONCENTRATION=1, DEPOSITION=2) RECEDIOR CDID SYSTEM (RECTANCULAD=1 or 7 rolad=2 or ()	1SW(1) =	1
DISCRETE RECEDENCE SYSTEM (RECTANGULARE) OR 5, PULAREZ OR 4)	15W(2) = 1	5
TERRAIN FIEVATIONS ARE READ (YES=1 NO=0)	ISW(3) =	1
CALCULATIONS ARE UPITTEN TO TADE (YES-1 NO-0)	ISW(4) -	1
LIST ALL INPUT DATA (NO=0 YES=1 MET DATA ALSO=2)	ISW(J) =	1
CALCULATE (CONCENTRATION=1,DEPOSITION=2) RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4) DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2) TERRAIN ELEVATIONS ARE READ (YES=1,NO=0) CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0) LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2)	130(0) -	1
COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)		
WITH THE FOLLOWING TIME PERIODS:		
HOURLY (YES=1,NO=0)	ISW(7) =	1
2-HOUR (YES=1,NO=0)	ISW(8) =	0
3-HOUR (YES=1,NO=0)	ISW(9) =	0
4-HOUR (YES=1,NO=0)	ISW(10) =	0
6-HOUR (YES=1,NO=U)	ISW(11) =	0
8-HOUR (YES=1,NO=U)	ISW(12) =	0
12-HOUR (TES=1,NO=0)	ISW(13) =	0
24-HOUR (TES=),NU=U)	1SW(14) =	1
WITH THE FOLLOWING TIME PERIODS: HOURLY (YES=1,NO=0) 2-HOUR (YES=1,NO=0) 3-HOUR (YES=1,NO=0) 4-HOUR (YES=1,NO=0) 8-HOUR (YES=1,NO=0) 12-HOUR (YES=1,NO=0) 24-HOUR (YES=1,NO=0) PRINT 'N'-DAY TABLE(S) (YES=1,NO=0)	ISW(15) =	1
PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE		
SPECIFIED BY ISW(7) THROUGH ISW(14):		
DAILY TABLES (YES=1,NO=0)	ISW(16) =	0
DAILY TABLES (YES=1,NO=0) HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0)	ISW(17) =	1
MAXIMUM 50 TABLES (YES=1.NO=0)	ISW(18) =	0
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2) RURAL-URBAN OPTION (RU.=0,UR. MODE 1=1,UR. MODE 2=2,UR. MODE 3=3)	ISW(19) =	1
RURAL-URBAN OPTION (RU.=0,UR. MODE 1=1,UR. MODE 2=2,UR. MODE 3=3)	ISW(20) =	0
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3)	ISW(21) =	1
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3) VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3) SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0) PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2)	ISW(22) =	1
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0)	ISW(23) =	0
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1, NO=2)	ISW(24) =	2
PROGRAM ADJUSTS ALL STACK REIGHTS FUR DUWNWASH (TES=2,NU=T)	15W(25) =	2
CONCENTRATIONS DURING CALM REPLOCE OF = 0 (YES=1,NU=2)	15W(20) =	1
CONCENTRATIONS DURING CREM PERIODS SET = 0 ( $(cs=1, n0=2)$ ) PEC DEEALL OPTION CHOSEN (YES=1 NO=2)	ISW(27) =	ן . ס
TYPE OF DOLLUTANT TO BE MODELLED (1-SO2 2-OTHER)	150(20) -	1
DEBUG OPTION CHOSEN (YES=1 NO=2)	154(27) =	2
ABOVE GROUND (FLAGPOLE) RECEPTORS LISED (YES=1.NO=0)	15W(30) =	1
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2) PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1) PROGRAM USES BUOYANCY INDUCED DISPERSION (YES=1,NO=2) CONCENTRATIONS DURING CALM PERIODS SET = 0 (YES=1,NO=2) REG. DEFAULT OPTION CHOSEN (YES=1,NO=2) TYPE OF POLLUTANT TO BE MODELLED (1=S02,2=OTHER) DEBUG OPTION CHOSEN (YES=1,NO=2) ABOVE GROUND (FLAGPOLE) RECEPTORS USED (YES=1,NO=0)	100(21)	•
ABOVE GROUND (FLAGPOLE) RECEPTORS USED (YES=1,NO=0) NUMBER OF INPUT SOURCES NUMBER OF SOURCE GROUPS (=0,ALL SOURCES) TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS) NUMBER OF X (RANGE) GRID VALUES NUMBER OF Y (THETA) GRID VALUES NUMBER OF DISCRETE RECEPTORS SOURCE EMISSION RATE UNITS CONVERSION FACTOR HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION	NSOURC =	18
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES)	NGROUP =	0
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS)	IPERD =	0
NUMBER OF X (RANGE) GRID VALUES	NXPNTS =	31
NUMBER OF Y (THETA) GRID VALUES	NYPNTS =	31
NUMBER OF DISCRETE RECEPTORS	NXWYPT =	0
SOURCE EMISSION RATE UNITS CONVERSION FACTOR	TK =.	.10000E+07
REIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED	ZR =	10.00 METERS
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION		9
SURFACE STATION NO.		.000000E+00 92001
YEAR OF SURFACE DATA	155 = 15Y =	
UPPER AIR STATION NO.		94001
YEAR OF UPPER AIR DATA	103 = IUY =	
ALLOCATED DATA STORAGE		43500 WORDS
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN		19643 WORDS
*** HUNG SHUI KIU (CHIMNEYS' EMISSION)		***
*** METEOROLOGICAL DAYS TO BE PROCESSED	***	

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\*\*\* METEOROLOGICAL DAYS TO BE PROCESSED \*\*\* (IF=1)

1	1	1	1	1	1	1	1	1	1	1	1	1	1	t i	1 '	11	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	1	1	1	1	1	1	1	1	1	1	1	1	Ľ	1	1 1	11	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	1	1	1	1	1	1	1	1	1	1	1	1	11	Ľ	1 1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	Ľ	1 1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	î
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1 '	11	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	1	1	1	1	1	1	.1	1	1	1	1	1	1	1	1 1	11	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	1	1	1	1	1	1	1	1	1	1		1 1	1 '	1	1 '	1 1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	1	1	1	1	1	1	1	1	1	1		1 1	1'	1	1.	1																																	

\*\*\* UPPER BOUND OF FIRST THROUGH FIFTH WIND SPEED CATEGORIES \*\*\* (METERS/SEC)

1.54, 3.09, 5.14, 8.23, 10.80,

#### \*\*\* WIND PROFILE EXPONENTS \*\*\*

STABILITY		WING	SPEED CATEGOR	(		
CATEGORY	1	2	3	4	5	6
Α	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01
В	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01
C	.10000E+00	.10000E+00	.10000E+00	.10000E+00	_10000E+00	.10000E+00
D	.15000E+00	-15000E+00	.15000E+00	.15000E+00	.15000E+00	.15000E+00
E	.35000E+00	.35000E+00	.35000E+00	.35000E+00	.35000E+00	.35000E+00
F	.55000E+00	.55000E+00	.55000E+00	.55000E+00	.55000E+00	.55000E+00

## \*\*\* VERTICAL POTENTIAL TEMPERATURE GRADIENTS \*\*\* (DEGREES KELVIN PER METER)

:

STABILITY		WING	SPEED CATEGORY	ſ		
CATEGORY	1	2	3	4	5	-6
A	-00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
В	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
С	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
D	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
Ε	.20000E-01	.20000E-01	.20000E-01	.20000E-01	.20000E-01	.20000E-01
F	.35000E-01	.35000E-01	.35000E-01	.35000E-01	.35000E-01	.35000E-01
	*** HING SI	HUT KILL (CHIMNE)	ST ENISSION		***	

\*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

#### \*\*\* X-COORDINATES OF RECTANGULAR GRID SYSTEM \*\*\* (METERS)

817000.0,	817050.0,	817100.0,	817150.0,	817200.0,	817250.0,	817300.0,	817350.0,	817400.0,	817450.0,
817500.0,	817550.0,	817600.0,	817650.0	817700.0	817750.0,	817800.0,	817850.0	817900.0,	817950.0,
818000.0,	818050.0,	818100.0,	818150.0	818200.0,	818250.0,	818300.0,	818350.0	818400.0,	818450.0,
818500.0,									

#### \*\*\* Y-COORDINATES OF RECTANGULAR GRID SYSTEM \*\*\* (METERS)

832500.0	832550.0,	832600.0,	832150.0, 832650.0,	832700.0,	832750.0,	832800.0,	832850.0	832900.0,	832950.0,
833000.0,	833050.0,	833100.0,	833150.0,	833200.0,	833250.0,	833300.0,	833350.0	833400.0,	833450.0,
833500.0,									

\*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

## \* ELEVATION HEIGHTS IN METERS \* \* FOR THE RECEPTOR GRID \*

\*\*\*

Y-AXIS /				X-4	AXIS (METERS)				نيا
(METERS) /	817000.0	817050.0	817100.0	817150.0	817200.0	817250.0	817300.0	817350.0	817400
			• • • • • • • •						· []
833500.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50
833450.0 /	4.50000	4,50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
833400.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500_
833350.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50
833300.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50
833250.0 /	4,50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500-
833200.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
833150.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50f~
833100.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50
833050.0 /	4.50000	4,50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50
833000.0 /	4,50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
832950.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
832900.0 /	4.50000	4.50000	4.50000	4.50000	4,50000	4.50000	4.50000	4.50000	4.50
832850.0 /	4.50000	4.50000	4.50000	4,50000	4.50000	4.50000	4.50000	4.50000	4.50
832800.0 /	4.50000	4.50000	4.50000	4,50000	4.50000	4.50000	4,50000	4,50000	4.50
832750.0 /	4.50000	4,50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
832700.0 /	4.50000	4,50000	4,50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50p
832650.0 /	4.50000	4.50000	4.50000	4,50000	4,50000	4.50000	4.50000	4.50000	4.50
832600.0 /	4.50000	4,50000	4.50000	4,50000	4,50000	4.50000	4.50000	4.50000	4.50
832550.0 /	4.50000	4,50000	4,50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
832500.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
832450.0 /		4.50000	4.50000	4.50000	4,50000	4.50000	4.50000	4.50000	4.50
832400.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50
									L'

	832350.0 / 832300.0 / 832250.0 / 8322200.0 /	4.50000 4.50000 4.50000 4.50000	4.50000 4.50000 4.50000	4.500 4.500 4.500						
сэ гч	832150.0 / 832100.0 /	4.50000	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000 4.50000	4.500 4.500 4.500
	832050.0 / 832000.0 /	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000	4.50000 4.50000	4.50000	4.50000 4.50000	4.50000 4.50000	4.500 4.500
			*** HUNG S	SHUI KIU (CHIN	MNEYS' EMISSIO	N)		***		
					EVATION HEIGHT FOR THE RECEP					
	Y-AXIS / (METERS) /	817450.0	817500.0	817550.0	X-A 817600_0	XIS (METERS) 817650.0	817700.0	817750.0	817800.0	817850
L	833500.0 / 833450.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500 .000
	833400.0 / 833350.0 /	.00000 .00000	_00000 _00000	.00000 .00000	.00000	.00000 .00000	.00000	.00000	.00000	.000
نا	833300.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
	833250.0 / 833200.0 /	.00000 .00000	.00000 .00000	.00000.	.00000. .00000	.00000 .00000	.00000 .00000	.00000	.00000	.000 .000
1	833150.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
نـا	833100.0 / 833050.0 /	.00000 .00000	.00000 .00000	.00000.	.00000	.00000 .00000	.00000	.00000 .00000	.00000	.000 .000
	833000.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
	832950.0 / 832900.0 /	.00000	.00000	.00000.	.00000	.00000 .00000	.00000	.00000 .00000	.00000	.000 .000
نا	832850.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
-	832800.0 / 832750.0 /	.00000	.00000 .00000	.00000.	.00000 .00000	.00000 .00000	.00000	.00000 .00000	.00000 .00000	.000 .000
	832700.0 /	.00000	.00000	.00000	.00000	.00000	.00000	-00000	.00000	.000
	832650.0 / 832600.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
	832550.0 /	.00000	.00000 .00000	.00000.	.00000. .00000	.00000	.00000 .00000	.00000	.00000	.000 .000
Γ	832500.0 /	.00000	.00000	-00000	.00000	.00000	.00000	.00000	.00000	.000
Ľ	832450.0 / 832400.0 /	.00000	.00000 .00000	-00000	.00000	.00000 .00000	.00000 .00000	.00000	.00000	.000 .000
	832350.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
	832300.0 / 832250.0 /	.00000	.00000 .00000	.00000 .00000	.00000 .00000	.00000 .00000	.00000	.00000	.00000	-000
Ľ	832200.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000 .00000	.000 .000
	832150.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
	832100.0 / 832050.0 /	.00000 .00000	.00000 .00000	.00000. .00000	.00000. 00000.	.00000 .00000	.00000	.00000	.00000 .00000	.000 .000
	832000.0 /	5.00000	5.00000	5.00000	5.00000	.00000	6.00000	10.00000	70.00000	70.000
			*** HUNG S	HUI KIU (CHIM	NEYS' EMISSIO	N)		***		
					EVATION HEIGHT FOR THE RECEP				-	
[];-	Y-AXIS / (METERS) /	817900.0	817950.0	818000.0	X-A 818050.0	XIS (METERS) 818100.0	818150.0	818200.0	818250.0	818300
تــا	833500.0 /	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.50000	4.500
1 T	833450.0 / 833400.0 /	.00000 .00000	.00000 .00000	.00000 .00000	.00000 .00000	.00000	.00000 .00000	.00000	.00000 .00000	.000 .000
	833350.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
	833300.0 / 833250.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
rin	833200.0 /	.00000	.00000 .00000	.00000 .00000	.00000.	.00000 .00000	.00000	.00000 .00000	.00000 .00000	.000 .000
	833150.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.000
L	833100.0 / 833050.0 /	.00000 .00000	.00000 .00000	.00000.	.00000	.00000 .00000	.00000	.00000 .00000	.00000.	000. 000
	833000.0 /	.00000	.00000	-00000	.00000	.00000	.00000	.00000	_00000	_000
	832950.0 / 832900.0 /	.00000	.00000	.00000	.00000 .00000	.00000	.00000	.00000	.00000	.000 .000
L	832850.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	_000
	832800.0 / 832750.0 /	.00000 .00000	.00000 .00000	.00000 .00000	.00000	.00000 .00000	.00000 .00000	.00000.	.00000.	.000 .000
1. Sec. 1. Sec	832700.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	: .000
	832650.0 /	.00000	.00000	.00000	.00000	.00000	.00000	.00000	-00000	.000

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832600.0 / 832550.0 / 832500.0 / 832400.0 / 832350.0 / 832350.0 / 832250.0 / 832250.0 / 832150.0 / 832150.0 / 832100.0 / 832000.0 /	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	.000 .00 .00 .000 .000 .000 .000 .000
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\*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

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## \* ELEVATION HEIGHTS IN METERS \* \* FOR THE RECEPTOR GRID \*

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Y-AXIS	/			X	-AXIS (METERS)
(METERS)	/ 818350.0	818400.0	818450.0	818500.0	
					ter en la companya de
833500.0		4.50000	4.50000	4.50000	
833450.0		.00000	.00000	.00000	
833400.0		.00000	.00000	.00000	
833350.0		.00000	.00000	.00000	
833300.0		.00000	.00000	.00000	
833250.0	/ .00000	.00000	.00000	.00000	·
833200.0	/ .00000	_00000	.00000	.00000	
833150.0	/ .00000	.00000	.00000	.00000	
833100.0	/ .00000	.00000	.00000	.00000	
833050.0	/ .00000	.00000	.00000	.00000	
833000.0	/ .00000	.00000	.00000	.00000	
832950.0	/ .00000	.00000	.00000	.00000	
832900.0	/ .00000	.00000	.00000	.00000	
832850.0		.00000	.00000	.00000	
832800.0	/ .00000	.00000	.00000	.00000	
832750.0	-	.00000	.00000	.00000	
832700.0	-	.00000	.00000	.00000	
832650.0	•	.00000	.00000	.00000	·
832600.0		.00000	.00000	.00000	
832550.0	•	.00000	.00000	.00000	
832500.0	•	.00000	.00000	.00000	
832450.0		.00000	.00000	.00000	
832400.0	•	.00000	.00000	.00000	
832350.0		.00000	.00000	.00000	
832300.0		.00000	.00000	.00000	
832250.0		.00000	.00000	.00000	
832200.0		.00000	.00000	.00000	
832150.0		.00000	.00000	.00000	5
832100.0	•	.00000	.00000		
832050.0	,	.00000		.00000	Г
832000.0		133.70000	.00000	.00000	
032000.0	/ 20.00000	133.70000	133.70000	160.00000	Li

\*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

### \* ABOVE GROUND RECEPTOR HEIGHTS IN METERS \* \* FOR THE RECEPTOR GRID \*

Y-AXIS /				X-4	AXIS (METERS)				
(METERS) /	817000.0	817050.0	817100.0	817150.0	817200.0	817250.0	817300.0	817350.0	81740
									ن
833500.0 /	1,50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500
833450.0 /	1.50000	1.50000	1.50000	1,50000	1.50000	1.50000	1.50000	1.50000	1.500_
833400.0 /	1.50000	1.50000	1.50000	1.50000	1,50000	1.50000	1.50000	1.50000	1.50
833350.0 /	1.50000	1.50000	1,50000	1.50000	1.50000	1.50000	1,50000	1.50000	1.50
833300.0 /	1.50000	1.50000	1.50000	1.50000	1,50000	1.50000	1,50000	1.50000	1.500-
833250.0 /	1.50000	1.50000	1.50000	1.50000	1.50000	1,50000	1.50000	1,50000	1.500
833200.0 /	1.50000	1.50000	1,50000	1.50000	1.50000	1.50000	1.50000	1,50000	1.500 -
833150.0 /	1.50000	1.50000	1,50000	1,50000	1.50000	1.50000	1.50000	1.50000	1.50
833100.0 /	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1,50000	1.50000	1.50
833050.0 /	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500
833000.0 /	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500
832950.0 /	1.50000	1.50000	1.50000	1.50000	1,50000	1.50000	1.50000	1.50000	1.50
832900.0 /	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50
								,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	

832850.0 /       1.50000         832800.0 /       1.50000         832750.0 /       1.50000         832750.0 /       1.50000         832600.0 /       1.50000         832600.0 /       1.50000         832550.0 /       1.50000         832550.0 /       1.50000         832550.0 /       1.50000         832550.0 /       1.50000         832550.0 /       1.50000         832450.0 /       1.50000         832350.0 /       1.50000         832250.0 /       1.50000         832250.0 /       1.50000	1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000           000         1.50000	1.50000 1.50000 1.50000 1.50000 1.50000 1.50000 1.50000 1.50000 1.50000 1.50000 1.50000 1.50000	1.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.5001.500001.500
832200.0 /       1.50000         832150.0 /       1.50000         832100.0 /       1.50000         832050.0 /       1.50000         83200.0 /       1.50000         83200.0 /       1.50000	1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000           1.50000         1.50000	1.50000       1.500         1.50000       1.500         1.50000       1.500         1.50000       1.500         1.50000       1.500         1.50000       1.500         1.50000       1.500	1.50000           000         1.50000           000         1.50000           010         1.50000	1.50000 1.50000 1.50000 1.50000 1.50000	1.50000       1.500         1.50000       1.500         1.50000       1.500         1.50000       1.500         1.50000       1.500         1.50000       1.500
	*** HUNG SHUI KIU (CH	HIMNEYS' EMISSION)		***	
	* ABOVE (	GROUND RECEPTOR HEIGHTS * FOR THE RECEPTOR GRII			
Y-AXIS / (METERS) / 817450.0	817500.0 817550.0	X-AXIS (ME 817600.0 817650		817750.0	817800.0 817850
833500.0 /       1.50000         833450.0 /       1.50000         833400.0 /       1.50000         833350.0 /       1.50000         833220.0 /       1.50000         83320.0 /       1.50000         83320.0 /       1.50000         833200.0 /       1.50000         83320.0 /       1.50000         833150.0 /       1.50000         83300.0 /       1.50000         83300.0 /       1.50000         832950.0 /       1.50000         832950.0 /       1.50000         832800.0 /       1.50000         832850.0 /       1.50000         832850.0 /       1.50000         832650.0 /       1.50000         832550.0 /       1.50000         832550.0 /       1.50000         83250.0 /       1.50000         83250.0 /       1.50000         83250.0 /       1.50000         83250.0 /       1.50000         83250.0 /       1.50000         83250.0 /       1.50000         83250.0 /       1.50000         83250.0 /       1.50000         832250.0 /       1.50000         832250.0 /       1.50000 <tr< td=""><td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td><td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td><td>000         1.50000           000</td><td>1.50000 1.50000</td><td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td></tr<>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	000         1.50000           000	1.50000 1.50000	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	*** HUNG SHUI KIU (CH * ABOVE (	HIMNEYS' EMISSION) GROUND RECEPTOR HEIGHTS * FOR THE RECEPTOR GRII		***	

## \* ABOVE GROUND RECEPTOR HEIGHTS IN METERS \* \* FOR THE RECEPTOR GRID \*

	Y-AXIS	/				· X-	AXIS (METERS)				
- ſ`	(METERS)	1	817900.0	817950.0	818000.0	818050.0	818100.0	818150.0	818200.0	818250.0	818300
Ŀ										· <b></b> ·	
	833500.0	1	1.50000	1.50000	1.50000	1,50000	1.50000	1.50000	1.50000	1.50000	1.500
<b>F</b> `	833450.0	1	1.50000	1.50000	1.50000	1.50000	1,50000	1.50000	1.50000	1.50000	1.500
	833400.0	17	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1,500
L.	833350.0	17	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500
	833300.0	1	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500
	833250.0	1	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500
	833200.0	17	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500
L	833150.0	) /	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.50000	1.500

832200.0         /         1.50000         1.5	832150.0 / 832100.0 / 832050.0 /	1.50000 1.50000 1.50000	1.50000 1.50000 1.50000 1.50000	1.50						
	·									1.50

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\*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

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## \* ABOVE GROUND RECEPTOR HEIGHTS IN METERS \* \* FOR THE RECEPTOR GRID \*

Y-AXIS /				X-AX1	S (METERS)				-		
(METERS) /	818350.0	818400.0	818450.0	818500.0		-					
833500.0 /	1.50000	1.50000	1.50000	1.50000							
833450.0 /	1.50000	1.50000	1.50000	1.50000							
833400.0 /	1.50000	1.50000	1.50000	1,50000							
833350.0 /	1.50000	1.50000	1.50000	1.50000							
833300.0 /	1.50000	1.50000	1.50000	1.50000							
833250.0 /	1.50000	1.50000	1.50000	1.50000							
833200.0 /	1.50000	1.50000	1.50000	1.50000							
833150.0 /	1.50000	1.50000	1.50000	1.50000							
833100.0 /	1.50000	1.50000	1.50000	1.50000							
833050.0 /	1.50000	1.50000	1,50000	1.50000							
833000.0 /	1.50000	1.50000	1,50000	1.50000							
832950.0 /	1.50000	1.50000	1.50000	1.50000							
832900.0 /	1.50000	1,50000	1.50000	1.50000							
832850.0 /	1.50000	1.50000	1.50000	1.50000							
832800.0 /	1.50000	1.50000	1.50000	1.50000							
832750.0 /	1.50000	1.50000	1.50000	1.50000	•						
832700.0 /	1.50000	1.50000	1.50000	1.50000							
832650.0 /	1.50000	1.50000	1.50000	1.50000							
832600.0 /	1.50000	1.50000	1.50000	1,50000							
832550.0 /	1.50000	1.50000	1.50000	1.50000							
832500.0 /	1.50000	1.50000	1.50000	1.50000							
832450.0 /	1.50000	1.50000	1.50000	1.50000							
832400.0 /	1.50000	1.50000	1.50000	1.50000							
832350.0 /	1.50000	1.50000	1.50000	1.50000							
832300.0 /	1,50000	1.50000	1.50000	1.50000							
832250.0 /	1.50000	1.50000	1.50000	1.50000							
832200.0 /	1.50000	1.50000	1.50000	1,50000							
832150.0 /	1.50000	1.50000	1.50000	1.50000							
832100.0 /	1.50000	1.50000	1.50000	1.50000							
832050.0 /	1.50000	1.50000	1.50000	1.50000							
832000.0 /	1.50000	1.50000	1.50000	1.50000							
		*** HUNG \$	SHUI KIU (CHI	MNEYS' EMISSION)	•		,	***			

## \*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

#### \*\*\* SOURCE DATA \*\*\*

 URCE IMBER	Ρ	A K	NUMBER PART. CATS.	EMISSION RATE TYPE=0,1 (GRAMS/SEC) TYPE=2 (GRAMS/SEC) *PER METER**2	x	Y (METERS)	BASE ELEV (METERS)	HEIGHT (METERS)	TEMP. TYPE=0 (DEG.K); VERT.DIM TYPE=1 (METERS)	TYPE=1,2	DIAMETER TYPE=0	BLDG. HEIGHT TYPE=0 (METERS)	BLDG. LENGTH TYPE=0 (METERS)	BLDG. WIDTH TYPE=0 (METERS)	- <b>-</b>
ż	0 0 0 0	0 0	0 0 0 0	.99000E-01 .40000E-02 .11000E-01 .40000E-02	818138.0 818062.0 818078.0 818050.0	832412.0 832338.0 832338.0 832322.0	.0 .0 .0	19.80 11.10 9.40 11.10	273.15 273.15 273.15 273.15 273.15	9.00 9.00 9.00 9.00	.23 .24 .27 .20	.00 .00 .00 .00	.00 .00 .00	.00 .00 .00 .00	

	6 7 8 9 10 11 12 13 14 15 16 17	0 0 0 0 0 0	.40000E-0 .9000E-0 .21000E-0 .11000E-0 .11000E-0 .38300E+0 .97000E-0 .78000E-0 .10410E+0 .38400E+0 .37100E+0	22 818028.0 31 818026.0 31 818036.0 31 818034.0 31 818034.0 31 818034.0 31 818034.0 31 818034.0 31 818034.0 31 818034.0 31 818034.0 31 818034.0 31 81804.0 31 8170.0 31 817426.0 31 817426.0 31 817426.0 31 817426.0 31 81775.0 31 81 81775.0 31 81775.0		0 .0 0 .0		273.15 273.15 273.15 273.15 273.15 273.15 461.15 453.15 273.15 273.15 273.15 439.15 439.15 439.15 461.15	9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00	.31 .24 .34 .27 .27 .56 .69 .31 .38 .61 .35 .35 .71 *** THE DAY *	.00 .00 .00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00 .00 .00	00 00 00 00 00 00 00 00 00 00 00 00 00
	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	Hour	SCALAR	- <b></b>
	SOURCE NO 1 7 13 19	0. = 1 .00000E+00 .00000E+00 .10000E+01 .10000E+01	2 8 14 20	.00000E+00 .10000E+01 .10000E+01 .10000E+01	9 15	.00000E+00 .10000E+01 .10000E+01 .10000E+01	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .10000E+01	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+60	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
	SOURCE NO 1 7 13 19	0. = 2 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	9 15	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
	SOURCE NO 1 7 13 19	0. = 3 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	9 15	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
<b>؛</b> 	SOURCE NO 1 7 13 19	0. = 4 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	9 15	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
	SOURCE NO 1 7 13 19	0. = 5 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	9. 15.	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
	SOURCE NO 1 7 13 19	0. = 6 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	9 15	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
				*** HUNG SH	NI KIN (	CHIMNEYS' E	MISSION)			***			-
[]				* SOURCE EN	ISSION R	ATE SCALARS	WHICH V	ARY FOR EACH	HOUR OF	THE DAY *			
L	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	<b>-</b>
	SOURCE NO 1 7 13 19	0. = 7 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	9	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .1000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
	SOURCE NO 1 7	D. = 8 .00000E+00 .00000E+00		.00000E+00 .00000E+00		.00000E+00 .10000E+01	4 10	.00000E+00 .10000E+01	5 11	.00000E+00 .10000E+01	6 12	.00000E+00 .10000E+01	

13 19	.10000E+01 .00000E+00	14 20	.10000E+01 .00000E+00	15 21	.10000E+01 .00000E+00	_ 16 22	.10000E+01 .00000E+00	17 23	-10000E+01 -00000E+00	18 24	.10000E+01 .00000E+00	
SOURCE NO 1 7 13 19	= 9 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	3 9 15 21	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
SOURCE NO 1 7 13 19	= 10 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	3 9 15 21	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
SOURCE NO 1 7 13 19	. = 11 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	3 9 15 21	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
SOURCE NO. 1 7 13 19	= 12 .10000E+01 .10000E+01 .10000E+01 .10000E+01	2 8 14 20	.10000E+01 .10000E+01 .10000E+01 .10000E+01	3 9 15 21	.10000E+01 .10000E+01 .10000E+01 .10000E+01	4 10 16 22	.10000E+01 .10000E+01 .10000E+01 .10000E+01	5 11 17 23	.10000E+01 .10000E+01 .10000E+01 .10000E+01	6 12 18 24	.10000E+01 .10000E+01 .10000E+01 .10000E+01	
			*** HUNG SH	IUI KIU	(CHIMNEYS' E	(ISSION)			***			<b>L</b>
			* SOURCE EN	ISSION	RATE SCALARS	WHICH V	ARY FOR EACH	HOUR OF	THE DAY *.			
HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	[]
SOURCE NO 1 7 13 19	= 13 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	3 9 15 21	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .00000E+00 .00000E+00	5 11 17 23	.90000E+00 .10000E+01 .00000E+00 .90000E+00	6 12 18 24	.00000E+00 .10000E+01 .00000E+00 .00000E+00	
SOURCE NO 1 7 13 19	= 14 .00000E+00 .00000E+00 .10000E+01 .10000E+01	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .10000E+01	3 9 15 21	.00000E+00 .10000E+01 .10000E+01 .10000E+01	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .10000E+01	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .10000E+01	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .10000E+01	
SOURCE NO 1 7 13 19	. = 15 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	3 9 15 21	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
SOURCE NO 1 7 13 19	. = 16 .00000E+00 .00000E+00 .10000E+01 .00000E+00	2 8 14 20	.00000E+00 .00000E+00 .10000E+01 .00000E+00	3 9 15 21	.00000E+00 .10000E+01 .10000E+01 .00000E+00	4 10 16 22	.00000E+00 .10000E+01 .10000E+01 .00000E+00	5 11 17 23	.00000E+00 .10000E+01 .10000E+01 .00000E+00	6 12 18 24	.00000E+00 .10000E+01 .10000E+01 .00000E+00	
			.00000E+00	3	.00000E+00	4 10	.00000E+00 .10000E+01	5 11	.00000E+00 .10000E+01	6 12	.00000E+00 .10000E+01	
SOURCE NO 1 7 13 19	. = 17 .00000E+00 .00000E+00 .10000E+01 .10000E+01	2 8 14 20	.00000E+00 .10000E+01 .00000E+00	· 9 15 21	.10000E+01 .10000E+01 .00000E+00	16 22	.10000E+01 .00000E+00	17 23	.10000E+01 .00000E+00	18 24	.10000E+01 .00000E+00	ſ
1 7 13	.00000E+00 .00000E+00 .10000E+01 .10000E+01	8 14	.00000E+00 .10000E+01	15	.10000E+01	16						

		HOURS				17 · 20 ·		0 0	0	0 0	0	0 0	0 1	0 0	0 0	0	0 0	0	0 0	0 0	0 0	0 0	0	1 0	0	0	0	0	0 0	0
	CALM	HOURS	(=1)	FOR	DAY	21 × 22 ×	۲ O	0 0	0 1	0 0	0 0	0	0	0	0 0	0 0	0	0	1 0	0	1 0	0	0 0	0	0	0	0	0	0	0
<b>—</b> *	CALM	HOURS	(=1)	FOR	DAY	30 ° 32 °	r 1	0	0 0	0 0	0 0	0 0	.0 0	0 0	0 0	1 0	0 0													
1	CALM	HOURS	(=1)	FOR	DAY	38 * 47 *	۰ Ó	-	0	0	0	0	0	0	1	1	1	0	0	0 0	0	0	0	0	0	0	0 0	0	0 0	0
-	CALM	HOURS HOURS HOURS	(=1)	FOR	DAY	48 ° 63 ° 67 °	• 0	0 1 1	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	1 0 0	0 0 0	1 0 0	0 0 0	1 0 0
*	CALM	HOURS	(=1)	FOR	DAY	76 v 87 v	۰ O	1 0	0 0	0 0	0 0	0	0	0	0	0 0	0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0
*	CALM	HOURS HOURS	(=1)	FOR	DAY	89 9 92 9	۰ O	0	0	0	0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 1	0 0	0 0	0 0	0 0	0 0	o O	0 0	1 0
	CALM	HOURS HOURS	(=1)	FOR	DAY	96 * 97 *	r Ö	0	0 0	0 1	0 0	0 0	0 0	0 0	1 0	0 0	0 0	0 0	0 0											
	CALM	HOURS	(=1)	FOR	DAY	107 v	' 0	0	0	0	0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0 0	1	0	0	0
	CALM	HOURS HOURS HOURS	(=1)	FOR	DAY	118,	r 0	0 0 0	0 0 1	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 1 0	0 0 0	0 0 0	1 0 0
<b>`</b> *	CALM	HOURS	(=1)	FOR	DAY	י 127	• 0	0	0	0	0 1	1 0	0	0	0	1 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
_∏*	CALM	HOURS	(=1)	FOR	DAY	129 *	· 0	0	1	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
*	CALM	HOURS HOURS	(=1)	FOR	DAY	136 '	• 0	0	0	0 1	0	0	0	0	0 0	0	0 0	0	0	0	0	1 0	0	0	0	0 0	0	0	0 0	0 0
*	CALM	HOURS	(=1)	FOR	DAY	145 '	r 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.	0	0	0	0	1
*	CALM	HOURS HOURS HOURS	(=1)	FOR	DAY	147 *	' 1	0 0 0	1 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 1	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0
_ <b>∏</b> *	CALM	HOURS	(=1)	FOR	DAY	162 1	• 0	0 0	1	0 0	0	0 0	0	0 0	0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0 0
* ليا	CALM	HOURS HOURS	(=1)	FOR	DAY	165 '	1	0	0	0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0	0 0	0	0 0	0 1	0	0 0	0 0	0	0 0	0 0	0 0	0 0
*	CALM	HOURS	(=1)	FOR	DAY	180 '	r 0	0	1	0	0 0	1 0	0	0	0	0	0 0	0	0 1	0	0	0	0	0 0	0	0	0	0	0	0 0
*	CALM	HOURS HOURS HOURS	(=1)	FOR	DAY	194 *	f 0	0 0 0	0 0 0	1 0 0	0 0 0	0 0 1	0 0 0	0 0 0	0 0 0	1 0 0	0 0 0	0	0 0 0	0 0 0	0 0 0	0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0	0 1	0 0 0
· []*	CALM	HOURS	(=1)	FOR	DAY	197 *	• 0	0	0	0	0	0	1	0	0	0	0	0 0 0	0	0	0	0 0 0	0	0	0	0	0	0 0 0	0 0 0	0
L/*	CALM	HOURS HOURS	(=1)	FOR	DAY	200 *	0	0	0 0	0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0	0 0	0 0	0 0	0 0	0 0	0	0 0	0 1	1 0	0 0	1 0	0 0
*	CALM	HOURS HOURS	(=1)	FOR	DAY	215 *	' 0	0	0	0	0	0	0	0 0	0 0	0	0 0	0	0	0	0	0	0 0	0 0	0 1	0 0	0 1	1 0	0	0
*	CALM	HOURS	(=1)	FOR	DAY	220 *	۰ 1	0 0 0	0	0 0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0 0
[*	CALM	HOURS HOURS HOURS	(=1)	FOR	DAY	223 1	• 0	0	0 0 0	0 0 0	1 0 0	0 0 0	0 1 1	0 0 0	0 .0 0	0 0 0	0 0 0	0 0 0												
*لسا	CALM	HOURS	(=1)	FOR	DAY	234 *	r 0	0	0 0	0 0	0 0	0 0	0 0	0 1	0 0	1 0	0 0	0	0 0	1 0	0 0									
*	CALM	HOURS HOURS	(=1)	FOR	DAY	262 *	' 0	0	0 0	0 0	0	0	0 1	0 0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	1 0	0
*	CALM	HOURS	(=1)	FOR	DAY	268 '	۰ °	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
*	CALM	HOURS HOURS HOURS	(=1)	FOR	DAY	י 271	0 ۱	0 0 0	0 0 0	0 0 0	0 0 0	1 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 1	0 0 0	0 1 0	0 0 1
×ئــا	CALM	HOURS	(=1)	FOR	ÐAY	277 י	۰ ۱	0	0	0	0 0	0 0	0	0	0	0 0	0 0	0 0	0	0 0	0	0 0	0	0 0	0	0	1 0	0	0	o o
*	CALM CALM	HOURS	(=1) (=1)	FOR FOR	DAY DAY	304 ° 310 °	r 0 r 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	1 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	1 0	0 1
*	CALM	HOURS	(=1)	FOR	DAY	317 '	۰ ۱	0	1	0	0 0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0	0	0	0	0
*	CALM	HOURS HOURS HOURS	(=1)	FOR	DAY	327	۰ ۱	0	0 0 0	0 0 0	0 0 0	0 0 0	0 1. 0	0 0 0	1 0 0	1 0 0	0 0 0	0 0 1	0 0 0	0 0 0										
L*	CALM	HOURS	(=1)	FOR	DAY	332 3	* 0	0	0	1 0	0	0 0	0 0	1 0	0	1 0	0	0	0 1	0	0	0	0	0	0	0	0	0	0	0
	CALM	HOURS	(=1)	FOR	DAY	356	۰ ۱	0	0 0	0 0	ů O	0 0	1 0	1 1	0 0	0 0	0 0	0 0	0	0 0	0 0	0 0	0 0							
L																														

\*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

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\* 365-DAY AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER)

\* FROM ALL SOURCES \* \* FOR THE RECEPTOR GRID \* 'N'-DA 365 DA SGROUP

		* NAVILAIN VAL		D 00070 (VD					,
		" MAXIMUM VAL	DE EQUALS	2.82070 AND	OCCURRED AT (	818100.0,	832000.0) *		:
Y-AXIS / (METERS) /	817000.0	817050.0	817100.0		XIS (METERS) 817200.0	817250.0	817300.0	817350.0	817/00
									817400
833500.0 /	.82613	.85638	.88836	.92496	.96676	1.01840	1.08196	1.15360	1.23
833450.0 /	86830	.90157	.93502	.97139	1.01268	1.06195	1.12243	1.19186	1.272
833400.0 / 833350.0 /	.91848	.95618	-99573	1.03614	1.08090	1.13364	1.19687	1.26756	1.350
833300.0 /	.97169 1.00377	1.01436 1.04974	1.06219 1.10216	1.11080 1.15609	1.16164 1.21259	1.21846 1.27305	1.28589	1.35854	1.44
833250.0 /	1.02402	1.07304	1.13023	1.19051	1.25423	1.32361	1.34463 1.40201	1.42279 1.48418	1.50
833200.0 /	1.04371	1.09721	1.15843	1.22740	1.29677	1.36962	1.44971	1.52854	1.602
833150.0 / 833100.0 /	1.05902 1.06914	1.11665 1.12921	1.17648	1.24853	1.32114	1.39403	1.47198	1.54894	1.610_ 1.60
833050.0 /	1.07323	1.13538	1.18541 1.19480	1.25472	1.33029 1.32963	1.40610 1.40035	1.48230 1.46981	1.55344 1.53761	1.60
833000.0 /	1.07221	1.12891	1.19479	1.25032	1.31346	1.37285	1.43559	1.51239	1.590
832950.0 /	1.06743	1.11535	1.17389	1.22613	1.28377	1.34481	1.41141	1.50178	1.599
832900.0 / 832850.0 /	1.05996 1.06074	1.10199 1.09554	1.14230 1.12378	1.19531	1.24849 1.21765	1.32321	1.40480	1.50065	1.597
832800.0 /	1.07483	1.10118	1.13140	1.15657	1.19858	1.29271 1.25233	1.37580 1.32228	1.47201	1.55 1.47
832750.0 /	1.10498	1.12126	1.14877	1.16899	1.19725	1.22468	1.26899	1.31087	1.352
832700.0 / 832650.0 /	1.13520	1.14454	1.16688	1.19713	1.20635	1.21606	1.23029	1.23851	1.253
832600.0 /	1.17852 1.23198	1.18441 1.24808	1.18813 1.24346	1.20881 1.22946	1.21920 1.23501	1.21398 1.21081	1.20788	1.20853	1.21
832550,0 /	1.22229	1.29981	1.31037	1.28331	1.25232	1.24480	1.19105 1.21178	1.19754 1.21267	1.21 1.23
832500.0 /	1.17989	1.25193	1.34558	1.37122	1.32856	1.29636	1.26793	1.24737	. 1.258
832450.0 / 832400.0 /	1.10904 1.10413	1.18785 1.12888	1.27309	1.38566	1.46458	1.40727	1.37056	1.31144	1.30
832350.0 /	1.14261	1.18531	1.19069 1.22229	1.30491 1.24942	1.44987 1.31009	1.60172 1.46606	1.51359 1.66035	1.43485 1.51904	1.36
832300.0 /	1.17941	1.22979	1.28221	1.33563	1.38684	1.41756	1.40411	1.41623	1.238
832250.0 /	1.20711	1.26979	1.34093	1.41980	1.50203	1.57257	1.58181	1.41122	1_167
832200.0 / 832150.0 /	1.20500 1.20918	1.27302 1.27054	1.35730 1.35209	1.45173 1.44454	1.54523 1.52820	1.64158 1.61458	1.68729 1.53175	1.48708	1.23
832100.0 /	1.18274	1.24702	1.30240	1.38616	1.46115	1.42179	1.45847	1.47387 1.42799	1.47
832050.0 /	1.13170	1.18876	1.27693	1.29325	1.29016	1.33589	1.35421	1.38851	1.499
832000.0 /	1.11084	1.16128	1.15533	1.17385	1.21413	1.25940	1.27300	1.35002	1.428- 'N'-D
									365 D
		*** 9000		MNEYS' EMISSIO	MA		***		SGROUP
		nond .	SHOT KID (CHI	MNETS' EMISSIO	N )				
									<b>–</b>
		* 345-1		ONCENTRATION /		DIC NETEDS			
		* 365-0	DAY AVERAGE (	CONCENTRATION (	MICROGRAMS/CUE	BIC METER)	*		
		* 365-6		CONCENTRATION ( * FROM ALL S F FOR THE RECEP	OURCES *	BIC METER)	*		
		* 365-0 * MAXIMUM VALU	*	* FROM ALL S	OURCES * TOR GRID *		* 832000.0) *		
Y-AXIS /		* MAXIMUM VALU	* JE EQUALS	* FROM ALL S FOR THE RECEP 2.82070 AND X-A	OURCES * TOR GRID *	818100.0 <b>,</b>			
Y-AXIS / (METERS) /	817450.0		* JE EQUALS	* FROM ALL S FOR THE RECEP 2.82070 AND X-A	OURCES * TOR GRIÐ * OCCURREÐ AT (	818100.0 <b>,</b>	* 832000.0) * 817750.0	817800.0	81785
(METERS) /		* MAXIMUM VALU 817500.0	* JE EQUALS 817550.0	* FROM ALL S FOR THE RECEP 2.82070 AND X-A	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS)	818100.0 <b>,</b>		817800.0	81785
(METERS) / 833500.0 /	1.32567	* MAXIMUM VALU 817500.0 1.43084	JE EQUALS 817550.0 1.54862	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719	818100.0, 817700.0 1.95466	817750.0	2.21841	
(METERS) / 833500.0 / 833450.0 /	1.32567 1.21250	* MAXIMUM VALU 817500.0 1.43084 1.29651	JE EQUALS 817550.0 1.54862 1.38837	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241	818100.0, 817700.0 1.95466 1.70164	817750.0 2.09060 1.80350	2.21841 1.86622	2.330- 1.83
(METERS) / 833500.0 /	1.32567 1.21250 1.28465 1.36929	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719	818100.0, 817700.0 1.95466	817750.0	2.21841	2.330 1.83 1.83
(METERS) / 833500.0 / 833450.0 / 833400.0 / 833350.0 / 833300.0 /	1.32567 1.21250 1.28465 1.36929 1.43177	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402	2.21841 1.86622 1.87628 1.90591 1.95347	2.330 1.83 1.83 1.957 2.025
(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833300.0 / 833250.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119	2.330 1.83 1.83 1.957 2.025 2.03
(METERS) / 833500.0 / 833450.0 / 833400.0 / 833350.0 / 833300.0 /	1.32567 1.21250 1.28465 1.36929 1.43177	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347	2.330 1.83 1.83 1.957 2.025 2.03 2.03
(METERS) / 833500.0 / 833450.0 / 833450.0 / 83350.0 / 833250.0 / 8332250.0 / 833200.0 / 833150.0 / 833100.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.47435 1.48720 1.47931 1.47279	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.56922 1.57570	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604	2.330 1.83 1.957 2.025 2.03 2.07: 2.124 2.042
(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833250.0 / 833250.0 / 833150.0 / 833150.0 / 833100.0 / 833050.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.48720 1.47931 1.47279 1.47678	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.56922 1.57570 1.61709	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076	2.330 1.83 1.957 2.025 2.03 2.07: 2.124 2.042
(METERS) / 833500.0 / 833450.0 / 833450.0 / 83350.0 / 833250.0 / 8332250.0 / 833200.0 / 833150.0 / 833100.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.49823	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.69379 1.70773	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76704 1.73440	818100.0, 817700.0 1.95466 1.70164 1.70000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.75516	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69
(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 833150.0 / 833150.0 / 83300.0 / 83300.0 / 83300.0 / 832950.0 / 832900.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.49823 1.51581 1.49875	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.67990 1.48637 1.67970 1.48637 1.68074 1.67175 1.68074 1.65102 1.64171 1.65879 1.69379 1.70773 1.68613 1.62648	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76400 1.67221 1.60073	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.75516 1.64421 1.56941	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69 1.64 1.615
(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 83350.0 / 83320.0 / 83320.0 / 83320.0 / 833150.0 / 833150.0 / 83300.0 / 83300.0 / 832950.0 / 832950.0 / 832950.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.49823 1.51581 1.49875 1.44744	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.67990 1.48637 1.67970 1.48637 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.70773 1.68613 1.62648 1.54298	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76704 1.75440 1.67221 1.60073 1.55680	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.82716 1.75516 1.64421 1.56941 1.56941	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796	2.330 1.83 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.64 1.645 1.645 1.645
(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 833150.0 / 833150.0 / 83300.0 / 83300.0 / 83300.0 / 832950.0 / 832900.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.49823 1.51581 1.49875	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76704 1.76704 1.773400 1.67221 1.60073 1.55680 1.53164	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.64421 1.56941 1.56441 1.56441 1.56441	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.58905	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69 1.69 1.615 1.557 1.521
(METERS) / 833500.0 / 833450.0 / 833450.0 / 83350.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 833100.0 / 833100.0 / 83300.0 / 83200.0 / 832900.0 / 832850.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.47823 1.51581 1.49875 1.44744 1.35905 1.23963 1.13743	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.52504 1.61662 1.52504 1.61662 1.52504 1.61662 1.52504	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76704 1.75440 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.75516 1.64421 1.56941 1.56941 1.56941 1.56941 1.57024 1.51593	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.75836 1.62610 1.56383 1.56361 1.58905 1.60267 1.57133	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69 1.64 1.615 1.567 1.52[ 1.51] 1.58
(METERS) / 833500.0 / 833450.0 / 833450.0 / 83350.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 833100.0 / 833100.0 / 83300.0 / 832950.0 / 832850.0 / 832850.0 / 832850.0 / 832750.0 / 832750.0 / 832750.0 / 832750.0 / 832750.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.47823 1.51581 1.49823 1.51581 1.49875 1.44744 4.35905 1.23963 1.13743 1.09330	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104 1.13937	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 - 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76704 1.73440 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394	818100.0, 817700.0 1.95466 1.70164 1.7010 1.85676 1.82877 1.80042 1.81716 1.82716 1.82716 1.75516 1.64421 1.56941 1.56941 1.56941 1.56941 1.56941 1.57024 1.57024 1.51593 1.45258	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.58905 1.60267 1.57133 1.50742	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.58589	2.330 1.83 1.957 2.025 2.03 2.07 2.07 2.042 1.830 1.69 1.69 1.64 1.615 1.567 1.52[ 1.551 1.58 1.551
(METERS) / 833500.0 / 833450.0 / 833450.0 / 83350.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 833100.0 / 833100.0 / 83300.0 / 83200.0 / 832900.0 / 832850.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.47823 1.51581 1.49875 1.44744 1.35905 1.23963 1.13743	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104 1.13937 1.13633	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.52504 1.61662 1.52504 1.61662 1.52504 1.61662 1.52504	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 - 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76704 1.73440 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394 1.30931	818100.0, 817700.0 1.95466 1.70164 1.70000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.64421 1.56941 1.56958 1.37711	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.58905 1.60267 1.57133 1.50742 1.45287	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.57025 1.57025 1.59409 1.58589 1.54643	2.330 1.83 1.957 2.025 2.03 2.07 2.07 2.042 1.830 1.69 1.64 1.615 1.567 1.52 1.58 1.582 1.652 1.642
(METERS) / 833500.0 / 833400.0 / 833400.0 / 83350.0 / 83350.0 / 833200.0 / 833200.0 / 833200.0 / 83300.0 / 83300.0 / 83200.0 / 83290.0 / 83290.0 / 83280.0 / 832750.0 / 832750.0 / 832650.0 / 832650.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47678 1.49823 1.51581 1.49825 1.44744 1.35905 1.23963 1.13743 1.09330 1.09155 1.09873 1.11005	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104 1.13937 1.13633 1.14132 1.15269	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616 1.19434 1.20417 1.21065	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.67990 1.48637 1.67970 1.48637 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262 1.24959	OURCES * TOR GRID * OCCUURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76704 1.76704 1.73440 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394 1.30931 1.29133 1.30708	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.64421 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.57024 1.51593 1.45258 1.37711 1.35261 1.37870	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.58905 1.60267 1.57133 1.50742 1.45287 1.43616 1.46411	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.58589 1.54643 1.50809 1.56678	2.330 1.83 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.64 1.645 1.567 1.52 1.557 1.557 1.552 1.652 1.652 1.652 1.652 1.652 1.652 1.652 1.652
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(METERS) / 833500.0 / 833450.0 / 833450.0 / 83350.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 833100.0 / 83300.0 / 83300.0 / 832950.0 / 832950.0 / 832950.0 / 832750.0 / 832750.0 / 832650.0 / 83250.0 / 83260.0 / 83250.0 / 83260.0	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47678 1.49823 1.51581 1.49825 1.44744 1.35905 1.23963 1.13743 1.09330 1.09155 1.09873 1.11005	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.39727 1.28953 1.19104 1.13937 1.13633 1.14132 1.15269 1.17447 1.20168	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616 1.19434 1.20417 1.21065 1.22792 1.28204	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.69379 1.69379 1.69379 1.64171 1.658613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262 1.24964 1.24959 1.28467 1.38897	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.77340 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394 1.30708 1.35524 1.45810	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.82877 1.80042 1.81716 1.64421 1.56941 1.5593 1.45258 1.377701 1.57024 1.57024 1.57870 1.45258 1.37870 1.45258 1.37870 1.45258 1.37870 1.4215 1.50218	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.5751 1.56363 1.56361 1.56363 1.56361 1.58905 1.60267 1.57133 1.50742 1.45287 1.43616 1.46411 1.49485 1.54836	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.58589 1.54643 1.50809 1.56678 1.58032 1.60213	2.330 1.83 1.957 2.025 2.03 2.025 2.03 2.12 2.042 1.839 1.69 1.69 1.615 1.557 1.557 1.557 1.557 1.557 1.557 1.642 1.642 1.59 1.672 1.670
(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833250.0 / 833250.0 / 833150.0 / 833050.0 / 833050.0 / 832950.0 / 832950.0 / 832950.0 / 832750.0 / 832750.0 / 832750.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832450.0 / 832350.0 / 832350.0 / 832300.0 /	$\begin{array}{c} 1.32567\\ 1.21250\\ 1.28465\\ 1.36929\\ 1.43177\\ 1.47435\\ 1.48720\\ 1.47931\\ 1.47279\\ 1.47678\\ 1.49875\\ 1.49875\\ 1.51581\\ 1.49875\\ 1.44744\\ 1.35905\\ 1.23963\\ 1.13743\\ 1.09330\\ 1.09155\\ 1.09873\\ 1.11005\\ 1.13425\\ 1.13425\\ 1.13425\\ 1.1631\\ 1.08461 \end{array}$	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.392727 1.28953 1.19104 1.13937 1.13633 1.14132 1.15269 1.17447 1.20168 1.21572 1.23880	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616 1.19434 1.20417 1.21065 1.22792 1.28204 1.38236 1.37909	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262 1.24964 1.24959 1.28467 1.38897 1.45958 1.42720	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 - - 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76704 1.73440 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394 1.30931 1.29133 1.30708 1.35524 1.45810 1.49034 1.47337	818100.0, 817700.0 1.95466 1.70164 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.82716 1.82716 1.64421 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.57024 1.51593 1.45258 1.377711 1.35261 1.37870 1.42115 1.50218 1.50218 1.53579 1.53882	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.92661 1.75836 1.62610 1.56383 1.56361 1.58905 1.60267 1.57133 1.50742 1.45287 1.43616 1.49485 1.54836 1.60052 1.60253	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.58589 1.54643 1.50809 1.56678 1.56678 1.58032 1.60213 1.66639 1.71374	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69 1.64 1.615 1.567 1.52 1.652 1.652 1.652 1.652 1.672 1.670 1.670 1.69 1.78
(METERS) / 833500.0 / 833400.0 / 833400.0 / 83350.0 / 83350.0 / 833200.0 / 833200.0 / 833200.0 / 83300.0 / 83300.0 / 832900.0 / 832900.0 / 832900.0 / 832850.0 / 83260.0 / 83260.0 / 83260.0 / 83260.0 / 83250.0 / 83250.0 / 83260.0 /	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.49823 1.51581 1.49823 1.51581 1.49875 1.44744 1.35905 1.23963 1.13743 1.09330 1.09155 1.09873 1.11005 1.12352 1.13425 1.11631 1.08461 1.07326	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104 1.13937 1.13633 1.14132 1.15269 1.17447 1.20168 1.21572 1.23880 1.16124	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616 1.19434 1.20417 1.21065 1.22792 1.28204 1.38236 1.37909 1.28473	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262 1.24964 1.24959 1.28467 1.38897 1.45958 1.42720 1.37368	OURCES * TOR GRID * OCCURRED AT ( XIS (METERS) 817650.0 - 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76704 1.76704 1.76704 1.76704 1.76704 1.76704 1.76704 1.76704 1.75680 1.55164 1.60073 1.55680 1.53164 1.49691 1.49691 1.30931 1.29133 1.30708 1.35524 1.45810 1.49034 1.47337 1.45642	818100.0, 817700.0 1.95466 1.70164 1.7010 1.85676 1.82877 1.80042 1.81716 1.82716 1.84780 1.82716 1.75516 1.64421 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.55702 1.51593 1.45258 1.37711 1.35261 1.37870 1.42115 1.50218 1.53579 1.53882 1.54732	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.58905 1.60267 1.57133 1.50742 1.45287 1.43616 1.46411 1.49485 1.54836 1.60522 1.62253 1.64569	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.58589 1.54643 1.50809 1.56678 1.58032 1.60213 1.66639 1.71374 1.74356	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69 1.69 1.64 1.615 1.557 1.551 1.557 1.551 1.559 1.652 1.670 1.670 1.69 1.670 1.69 1.78 1.82
(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833250.0 / 833250.0 / 833150.0 / 833050.0 / 833050.0 / 832950.0 / 832950.0 / 832950.0 / 832750.0 / 832750.0 / 832750.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832450.0 / 832350.0 / 832350.0 / 832300.0 /	$\begin{array}{c} 1.32567\\ 1.21250\\ 1.28465\\ 1.36929\\ 1.43177\\ 1.47435\\ 1.48720\\ 1.47931\\ 1.47279\\ 1.47678\\ 1.49875\\ 1.49875\\ 1.51581\\ 1.49875\\ 1.44744\\ 1.35905\\ 1.23963\\ 1.13743\\ 1.09330\\ 1.09155\\ 1.09873\\ 1.11005\\ 1.13425\\ 1.13425\\ 1.13425\\ 1.1631\\ 1.08461 \end{array}$	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104 1.13937 1.13633 1.14132 1.15269 1.17447 1.20168 1.21572 1.23880 1.16124 1.18203	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616 1.19434 1.20417 1.21065 1.22792 1.28204 1.38236 1.37909	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.67990 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262 1.24964 1.29828 1.25262 1.24964 1.24959 1.28467 1.38897 1.45958 1.45958 1.42720 1.37368 1.42239	OURCES * TOR GRID * OCCUURRED AT ( XIS (METERS) 817650.0 - 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.74170 1.76704 1.73440 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394 1.30931 1.29133 1.30708 1.35524 1.45810 1.45810 1.45810 1.45642 1.52076	818100.0, 817700.0 1.95466 1.70164 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.75516 1.64421 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.5593 1.45258 1.37711 1.35261 1.37870 1.42115 1.50218 1.53579 1.53882 1.53879 1.53882 1.53772 1.53882	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.58905 1.60267 1.57133 1.50742 1.45287 1.43616 1.46411 1.49485 1.54836 1.60522 1.62253 1.64569 1.71322	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.58589 1.54643 1.50809 1.56678 1.58032 1.60213 1.66639 1.71374 1.74356 1.79749	2.330 1.83 1.957 2.025 2.037 2.12 2.042 1.839 1.64 1.645 1.567 1.527 1.51 1.58 1.642 1.642 1.567 1.527 1.527 1.642 1.59 1.642 1.642 1.59 1.642 1.642 1.59 1.672 1.672 1.670 1.672 1.670 1.672 1.6
(METERS) / 833500.0 / 833400.0 / 833400.0 / 83350.0 / 83350.0 / 83320.0 / 83320.0 / 83320.0 / 83300.0 / 83300.0 / 83300.0 / 83290.0 / 83290.0 / 83290.0 / 83290.0 / 83290.0 / 83290.0 / 832650.0 / 83250.0 / 83260.0 / 83250.0 / 83260.0	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47279 1.47678 1.49823 1.51581 1.49825 1.44744 1.35905 1.23963 1.13743 1.09330 1.09155 1.09873 1.11005 1.12352 1.13425 1.11631 1.08461 1.07326 1.07954 1.07954 1.15629 1.20414	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104 1.13937 1.13633 1.14132 1.15269 1.17447 1.20168 1.21572 1.23880 1.16124 1.18203 1.21877 1.22928	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616 1.19434 1.20417 1.21065 1.22792 1.28204 1.38236 1.37999 1.28473 1.31388 1.30990 1.29455	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.57175 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262 1.24964 1.24959 1.28467 1.38897 1.45958 1.42720 1.37368 1.42239 1.39579 1.37299	OURCES * TOR GRID * OCCUURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76704 1.76704 1.76704 1.73440 1.67221 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394 1.30708 1.35524 1.45810 1.49034 1.45810 1.49034 1.452076 1.49447 1.45088	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.64421 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.5593 1.45258 1.377711 1.35261 1.37870 1.42115 1.50218 1.53579 1.53882 1.54732 1.61677 1.59455 1.50481	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.56361 1.56383 1.56361 1.56361 1.56383 1.56361 1.56361 1.56383 1.56361 1.56361 1.56383 1.56361 1.56361 1.56383 1.56361 1.56361 1.56383 1.56361 1.56365 1.60267 1.57133 1.563661 1.66252 1.66253 1.66259 1.67330 1.51707	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.58589 1.54643 1.50809 1.54643 1.50809 1.54678 1.58032 1.60213 1.66639 1.71374 1.74356 1.79749 1.69396 1.50093	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69 1.645 1.567 1.557 1.557 1.557 1.557 1.557 1.557 1.557 1.557 1.645 1.645 1.652 1.645 1.652 1.645 1.652 1.672 1.670 1.672 1.670 1.672
(METERS) / 833500.0 / 833400.0 / 833400.0 / 83350.0 / 83320.0 / 83320.0 / 83320.0 / 83320.0 / 83300.0 / 83300.0 / 83300.0 / 83290.0 / 83290.0 / 83290.0 / 83290.0 / 83280.0 / 83260.0	1.32567 1.21250 1.28465 1.36929 1.43177 1.47435 1.48720 1.47931 1.47931 1.47678 1.49823 1.51581 1.49823 1.51581 1.49825 1.44744 1.35905 1.23963 1.13743 1.09330 1.09155 1.09873 1.11005 1.12352 1.13425 1.11631 1.08461 1.07326 1.07954 1.15629	* MAXIMUM VALU 817500.0 1.43084 1.29651 1.37230 1.46775 1.53012 1.55800 1.54384 1.51938 1.51623 1.54257 1.58745 1.60305 1.57341 1.49831 1.39727 1.28953 1.19104 1.13937 1.13633 1.14132 1.15269 1.17447 1.20168 1.21572 1.23880 1.16124 1.18203 1.21877	JE EQUALS 817550.0 1.54862 1.38837 1.46957 1.57570 1.63176 1.63867 1.59842 1.56922 1.57570 1.61709 1.66135 1.66296 1.61662 1.52504 1.42445 1.34623 1.26907 1.20616 1.19434 1.20417 1.21065 1.22792 1.28204 1.38236 1.37909 1.28473 1.31388 1.30090	* FROM ALL S FOR THE RECEP 2.82070 AND X-A 817600.0 1.48637 1.67990 1.48637 1.67970 1.68074 1.72016 1.69807 1.65102 1.64171 1.65879 1.69379 1.69379 1.70773 1.68613 1.62648 1.54298 1.46852 1.41562 1.36834 1.29828 1.25262 1.24964 1.29828 1.25262 1.24964 1.24959 1.28467 1.38897 1.45958 1.42720 1.37368 1.42239 1.39579	OURCES * TOR GRID * OCCUURRED AT ( XIS (METERS) 817650.0 1.81719 1.59241 1.68245 1.77783 1.78421 1.74333 1.72292 1.74170 1.76024 1.76704 1.76704 1.76704 1.76724 1.60073 1.55680 1.53164 1.49691 1.45319 1.38394 1.30931 1.29133 1.30708 1.35524 1.45810 1.49034 1.45810 1.49034 1.45642 1.52076 1.49447	818100.0, 817700.0 1.95466 1.70164 1.79000 1.85676 1.82877 1.80042 1.81716 1.83847 1.84780 1.82716 1.64421 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.56941 1.55793 1.45258 1.37770 1.45258 1.37770 1.45258 1.37870 1.42115 1.50218 1.53579 1.53882 1.54732 1.61677 1.59455	817750.0 2.09060 1.80350 1.86421 1.88937 1.87402 1.88924 1.91013 1.91698 1.92661 1.87951 1.75836 1.62610 1.56383 1.56361 1.56383 1.56361 1.56361 1.56383 1.56267 1.57133 1.50742 1.45287 1.43616 1.46411 1.49485 1.54836 1.6052 1.62253 1.64569 1.71322 1.67330	2.21841 1.86622 1.87628 1.90591 1.95347 1.97119 1.98347 2.01450 2.00604 1.89076 1.72493 1.62634 1.59079 1.56796 1.55493 1.57025 1.59409 1.56796 1.55493 1.57025 1.59409 1.58589 1.54643 1.50809 1.56678 1.58032 1.60213 1.66639 1.71374 1.74356 1.79749 1.69396	2.330 1.83 1.957 2.025 2.03 2.07 2.12 2.042 1.839 1.69 1.69 1.645 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.567 1.645 1

	832000.0 /	1.41764	1,41853	1.41641	1.43816	1.22466	1.50134	1.69024	2.41349	2.560 'N'-DA 365 DA
نـا	•		*** HUNG S	HUI KIU (CHI	MNEYS' EMISSIC	)N)		***		SGROUP
		·	* 365-0	AY AVERAGE C	ONCENTRATION (	MICROGRAMS/CUE	SIC METER)	*		
				*	* FROM ALL S					
L			* MAXIMUM VALU	IE EQUALS	2.82070 AND	OCCURRED AT (	818100.0,	832000.0) *		
[].	Y-AXIS / (METERS) /	817900.0	817950.0	818000.0	X-A 818050.0	XIS (METERS) 818100.0	818150.0	818200.0	818250.0	818300
	833500.0 / 833400.0 / 833400.0 / 833350.0 / 833200.0 / 833200.0 / 833200.0 / 833150.0 / 83300.0 / 83300.0 / 832950.0 / 832950.0 / 832850.0 / 832750.0 / 832750.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832550.0 / 832450.0 / 832450.0 / 832250.0 / 832200.0 / 832250.0 / 832250.0 / 832200.0	2.39548 1.67278 1.79022 1.97776 2.05962 2.11435 2.19913 2.19705 1.99361 1.78541 1.71489 1.66872 1.59784 1.54038 1.52273 1.53255 1.56650 1.64818 1.72474 1.60102 1.65851 1.72474 1.67763 1.78676 1.82208 1.69113 1.54654 1.57384	2.34145 1.50659 1.69780 1.93540 2.07362 2.19029 2.30173 2.17520 1.92664 1.82591 1.75056 1.64480 1.56832 1.55994 1.54115 1.55474 1.57401 1.60152 1.66271 1.65357 1.55107 1.58436 1.62491 1.61044 1.61044 1.61285 1.60046 1.44966 1.35802 1.31814	2.31269 1.38737 1.54403 1.85899 2.06527 2.26636 2.30668 2.04804 1.92267 1.83012 1.70599 1.63315 1.59891 1.57633 1.57729 1.54655 1.55688 1.576502 1.56258 1.49203 1.42275 1.30989 1.23811 1.20102 1.26695 1.34170 1.36670	2.39285 1.37440 1.42449 1.74034 1.96566 2.20121 2.03672 1.89775 1.82722 1.72287 1.67143 1.64968 1.62554 1.59411 1.56473 1.54791 1.54914 1.55180 1.52792 1.46259 1.36859 1.24488 1.13987 1.01605 .98467 1.05163 1.21507 1.29350 1.31355	2.05276 1.29161 1.16807 1.32048 1.54028 1.69513 1.61218 1.61219 1.63232 1.64605 1.65323 1.64640 1.62474 1.59780 1.57471 1.55822 1.52468 1.46382 1.37904 1.26272 1.16775 1.09699 1.10892 1.02762 1.15646 1.20225 1.26191 1.27656	1.66775 .89521 .77965 .79029 .92170 1.03805 1.18880 1.34630 1.52703 1.66592 1.73069 1.74571 1.71878 1.66724 1.61202 1.56606 1.52727 1.47441 1.40869 1.32728 1.22317 1.16524 1.26849 1.22555 1.16965 1.16957 1.17258 1.20866 1.19518	1.31359 .67608 .64188 .67981 .69251 .77014 1.08987 1.44621 1.68227 1.77649 1.80677 1.77141 1.71068 1.63757 1.57004 1.51825 1.47081 1.41130 1.33997 1.25617 1.18534 1.20740 1.27265 1.19546 1.13538 1.13401 1.08081 1.08729 1.06389	1.09302 .60841 .62823 .67827 .68197 .75454 1.06864 1.36518 1.53059 1.60457 1.60589 1.57615 1.53050 1.47396 1.42375 1.38734 1.35008 1.2458 1.21096 1.23294 1.23334 1.18065 1.11101 1.04255 1.03885 .98145 .96007 .92764	1.261 .721 .677 .661 .700 .824 1.036 1.171 1.259 1.321 1.348 1.350 1.242 1.216 1.209 1.232 1.265 1.242 1.216 1.209 1.232 1.267 1.219 1.110 1.042 .967 .945 .892 .867 .837
	832050.0 / 832000.0 /	1.26454 2.33999	1.28056 1.93592 *** HUNG S	1.34586 1.63005	1.28264 2.23552 MNEYS' EMISSIC	1.25758 2.82070	1.15897 2.55126	1.01979 2.06741	.89266 1.72270	.796 1.455 'N'-DA 365 DA SGROUP
						,				
			* 365-D		ONCENTRATION ( * FROM ALL S FOR THE RECEP		BIC METER)	*		
Π			* MAXIMUM VALL	IE EQUALS	2.82070 AND	OCCURRED AT (	818100.0,	832000.0) *		
	Y-AXIS / (METERS) /	818350.0	818400.0	818450.0	X-A 818500.0	XXIS (METERS)				
	833500.0 / 833450.0 / 833400.0 / 833350.0 / 833350.0 / 833250.0 / 833200.0 / 833150.0 / 833150.0 / 833050.0 / 833050.0 / 832950.0 / 832850.0 / 832850.0 / 8322700.0 / 832270.0 / 8322650.0 / 832650.0 /	1.58162 1.20171 1.14098 .85290 .93488 .98203 1.08627 1.16105 1.15331 1.14548 1.17237 1.20326 1.22390 1.21846 1.20728 1.20695 1.20183 1.20523 1.22508	2.18608 1.76082 1.49294 1.07908 1.17521 1.17295 1.14182 1.13423 1.10242 1.06193 1.04848 1.05527 1.07392 1.08460 1.10671 1.14089 1.17081 1.20429 1.25153	2.51684 1.90682 1.53971 1.17243 1.25612 1.27171 1.19528 1.12555 1.06184 .98857 .95880 .95147 .95385 .95147 .97720 1.02972 1.028677 1.14665 1.21910	2.45503 1.78922 1.45338 1.16938 1.25135 1.26848 1.18598 1.0086 1.01792 .93937 .87603 .86071 .85693 .84962 .88495 .94271 .99680 1.05732 1.12634			- - -		

832550.0 / 832450.0 / 832450.0 / 832350.0 / 832350.0 / 832250.0 / 832250.0 / 832200.0 / 832100.0 / 832100.0 / 832050.0 / 832000.0 /		449 1.24279 143 1.11554 379 .96837 937 .91575 646 .87899 218 .83769 312 .78988 886 .74693 762 .71849 982 .68525 429 1.12237	1.15474 1.09778 .98251 .87395 .84870 .84331 .81266 .77362 .73664 .70775 .68125 1.14907 S' EMISSION)	*** S/CURIC METER) *	HIGH 1-HR SGROUP
		* F	ROM ALL SOURCES * THE RECEPTOR GRID *	S COBIC METERY	
	MUMIXAM *	1 VALUE EQUALS 402.0	06100 AND OCCURRED AT (	818100.0, 832000.0)	* 1_i
Y-AXIS / (METERS) /	817000.0	817050.0	X-AXIS (METERS) 817100.0	817150.0	817200.0
833500.0 / 833450.0 / 833450.0 / 833450.0 / 83350.0 / 833250.0 / 833250.0 / 833250.0 / 833050.0 / 833050.0 / 832950.0 / 832950.0 / 832950.0 / 832850.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832550.0 / 832450.0 / 832450.0 / 832450.0 / 832250.0 / 832200.0 / 832250.0 / 832200.0 / 832200.0 / 832200.0 / 83200.0 / 832000.0 / 832000.0 / 832000.0 / 832000.0 / 832000.0 / 832000.0 / 8	38.17321 ( 15, 10) 37.48014 (275, 9) 45.85413 (315, 18) 104.14520 ( 9, 9) 66.38816 (358, 9) 54.47207 (358, 9) 85.10477 ( 11, 9) 88.65903 ( 11, 9) 50.18764 (364, 18) 55.62257 ( 34, 18) 62.56666 ( 34, 18) 62.56666 ( 34, 18) 62.42155 ( 2, 9) 50.10432 ( 2, 9) 55.78570 (359, 18) 77.94515 (314, 9) 83.13639 (314, 9) 83.13639 (314, 9) 54.53560 ( 8, 10) 53.75293 (310, 9) 54.32310 ( 11, 10) 51.78118 ( 11, 10) 42.27166 ( 11, 10) 32.48355 (332, 9) 43.72280 (358, 9) 43.72280 (358, 9) 43.72280 (358, 11, 9) 45.92642 (348, 18) 45.87812 (309, 9) 40.59303 (348, 18) 33.88072 (348, 18)	39.92944 ( 15,10) 39.20499 ( 66, 9) 46.84253 (315,18) 104.42090 ( 9, 9) 69.35278 (358, 9) 55.30251 (358, 9) 91.74480 ( 11, 9) 87.18233 ( 11, 9) 53.87582 (364,18) 62.89839 ( 34,18) 60.49852 ( 34,18) 60.49852 ( 34,18) 56.50925 ( 2, 9) 63.44907 ( 2, 9) 45.85842 (359,18) 65.25509 (314, 9) 88.30740 ( 314, 9) 75.31067 ( 314, 9) 59.87760 ( 8,10) 58.53273 ( 310, 9) 55.67320 ( 11,10) 55.94161 ( 11,10) 47.33411 ( 11,10) 34.19653 ( 11,10) 36.55985 ( 322, 9) 38.36111 ( 348,18) 45.22443 ( 358, 9) 55.65449 ( 11, 9) 48.02306 ( 309, 9) 42.33010 ( 348,18) 34.91178 ( 348,18) 27.93661 ( 170,22)	39.13059 ( 11,10) 38.02471 (332, 9) 38.37374 (348,18) 45.61249 (348,18) 49.92479 (348,18) 51.68365 ( 11, 9) 44.20591 (348,18) 36.01583 (348,18) 28.98724 ( 37,19) 25.02047 (317,10)	48.48525 (315,18) 103.91340 (9,9) 75.76212 (358,9) 61.71476 (11,9) 103.87870 (11,9) 78.38566 (11,9) 56.99470 (364,18) 71.90221 (34,18) 57.07896 (360,18) 70.43835 (2,9) 50.52476 (2,9) 67.51279 (359,18) 95.56908 (314,9) 78.73985 (314,9)	46.99054 (327, 18)         47.59167 (66, 9)         49.05101 (315, 18)         102.99390 (9, 9)         79.17938 (358, 9)         69.62712 (11, 9)         108.48490 (11, 9)         70.81476 (11, 9)         70.81476 (11, 9)         70.81476 (2, 9)         63.86174 (34, 18)         71.20822 (34, 18)         63.91756 (2, 9)         69.63434 (2, 9)         60.11477 (359, 18)         89.06412 (314, 9)         95.78909 (314, 9)         70.19868 (8, 10)         66.95891 (310, 9)         64.43862 (11, 10)         64.5120 (11, 10)         51.16786 (11, 10)         64.62011 (332, 9)         43.34604 (332, 9)         48.08266 (348, 18)         54.70150 (348, 18)         54.70150 (348, 18)         54.7679 (309, 9)         48.330951 (58, 15)         34.38582 (220, 9)         27.71144 (269, 9)         34.52600 (311, 9)         9         9         9         9         9         9         9         9         9         9 <t< td=""></t<>
		HEST 1-HOUR AVERAGE CO	DICENTRATION (MICROGRAMS	S/CUBIC METER) *	
		* FOR	ROM ALL SOURCES * THE RECEPTOR GRID *		<b>L</b>
Y-AXIS /	* MAXIMUM	1 VALUE EQUALS 402.0	06100 AND OCCURRED AT ( X-AXIS (METERS)	818100.0, 832000.0)	*
(METERS) /	817250.0	817300.0	817350.0	817400.0	817450.0
833500.0 / 833450.0 / 833400.0 / 833350.0 / 833250.0 / 833250.0 / 833250.0 / 833150.0 / 833100.0 / 833100.0 /	50.18977 (327,18) 50.58102 (66,9) 49.79362 (275,9) 101.36760 (9,9) 82.71930 (358,9) 78.38215 (11,9) 111.28450 (11,9) 62.07582 (364,18) 73.57751 (34,18) 65.78610 (34,18)	53.19372 (327,18) 53.66784 (66,9) 53.55835 (275,9) 98.66588 (9,9) 86.29924 (358,9) 87.70551 (11,9) 111.22480 (11,9) 111.22480 (11,9) 66.95301 (364,18) 80.62408 (34,18) 64.84069 (360,18)	55.49845 (327,18) 57.51927 (15,10) 57.59837 (275,9) 95.11531 (9,9) 89.75420 (358,9) 97.42465 (11,9) 107.67480 (11,9) 69.10391 (364,18) 82.67847 (34,18) 71.99213 (2,9)	66.06142 ( 7,18) 61.53514 ( 15,10) 61.88052 (275, 9) 90.61291 ( 9, 9) 92.93678 (358, 9) 107.03960 ( 11, 9) 99.96072 ( 11, 9) 71.41605 ( 34,18) 77.70499 ( 34,18) 84.02763 ( 2, 9)	78.48655 ( 7,18)         55.22882 ( 15,10)         56.66972 ( 71,18)         68.65823 (358, 9)         77.65128 (358, 9)         79.73957 ( 11, 9)         60.78629 ( 11, 9)         59.16525 ( 34,18)         65.57126 (269, 9)         61.89188 ( 2, 9)

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	833000.0 / 832950.0 / 832900.0 / 832800.0 / 832800.0 / 832750.0 / 832750.0 / 832600.0 / 832600.0 / 832550.0 / 832400.0 / 832400.0 / 832250.0 / 832250.0 / 832250.0 / 832250.0 / 832250.0 / 832150.0 / 832150.0 / 832100.0 / 832000.0 / 832000.0 /	74.46531 ( 2, 9) 61.74212 ( 2, 9) 72.43964 (359,18) 103.44910 (314, 9) 81.47459 (314, 9) 69.89466 ( 8,10) 64.27794 ( 11,10) 69.40623 ( 11,10) 58.27045 ( 11,10) 41.58381 (332, 9) 46.07326 (332, 9) 49.33033 (348,18) 57.43748 (348,18) 58.32293 (309, 9) 50.74623 (348,18) 88.32293 (309, 9) 50.74623 (348,18) 51.96284 (105, 9) 39.13264 (311, 9) 89.88213 (311, 9)	79.08243 ( 2, 9) 60.48185 (359,18) 94.67455 (314, 9) 102.36230 (314, 9) 77.56464 ( 8,10) 71.90088 (310, 9) 73.61005 ( 11,10) 65.94235 ( 11,10) 45.85560 ( 11,10) 45.85560 ( 11,10) 45.85560 ( 11,10) 45.85568 (348,18) 60.43415 (348,18) 60.43415 (348,18) 61.38181 (309, 9) 53.24646 (348,18) 40.51508 (348,18) 42.29115 (270, 9) 33.62326 (220, 9) 45.16674 (311, 9) 81.34126 (311, 9) 72.58019 (311, 9)	74.38127 ( 2, 9) 76.81174 (359,18) 111.73340 (314, 9) 82.87878 (314, 9) 76.12553 (310, 9) 75.89481 ( 11,10) 73.85114 ( 11,10) 53.73756 ( 11,10) 51.72212 (332, 9) 51.72324 (348,18) 63.70922 (348,18) 64.95789 (348,18) 64.95789 (348,18) 40.69310 ( 9, 9) 33.77779 (311, 9) 52.73243 (311, 9) 71.13728 (311, 9) 73.45013 (311, 9) 61.62191 (311, 9)	59.86277 ( 2, 9) 99.20205 (314, 9) 108.16450 (314, 9) 85.12324 ( 8,10) 75.18427 ( 11,10) 81.36638 ( 11,10) 62.86824 ( 11,10) 54.45129 (332, 9) 54.21042 (332, 9) 67.27330 (348,18) 69.09376 (348,18) 58.70613 (348,18) 58.70613 (348,18) 35.34456 (317,10) 41.86854 ( 9, 9) 61.80814 (311, 9) 77.60347 (311, 9) 81.25921 (311, 9) 72.68169 (311, 9) 56.76031 (311, 9) 42.60706 (314, 9)	57.59115 (359,18) 86.45935 (314, 9) 77.19467 ( 8,10) 65.08875 ( 8,10) 74.90197 ( 11,10) 63.13653 ( 11,10) 50.43227 (332, 9) 52.58912 (332, 9) 62.52901 (348,18) 65.08062 (348,18) 54.72200 (348,18) 38.42117 (348,18) 38.42117 (348,18) 35.16459 (317,10) 39.96346 (311, 9) 59.74081 (311, 9) 71.31126 (311, 9) 70.10336 (311, 9) 58.40187 (311, 9) 42.26165 (311, 9) 42.26165 (311, 9) 42.26165 (311, 9) 42.26165 (311, 9) 42.45761 (353, 9) HIGH 1-HR
		*** HU	NG SHUI KIU (CHIMNEYS'	EMISSION)	***	SGROUP
L		* HIGHE	ST 1-HOUR AVERAGE CON	CENTRATION (MICROGRAMS	/CUBIC METER) *	
1 of a Ball			* FR	ROM ALL SOURCES * THE RECEPTOR GRID *	· · ·	
		* MAXIMUM	VALUE EQUALS 402.06	5100 AND OCCURRED AT (	818100.0, 832000.0)	*
	Y-AXIS / (METERS) /	817500.0	817550.0	X-AXIS (METERS) 817600.0	817650.0	817700.0
	833500.0 / 833450.0 / 833400.0 / 833350.0 / 833250.0 / 833250.0 / 833250.0 / 833200.0 / 833100.0 / 833100.0 / 83300.0 / 832950.0 / 832950.0 / 832950.0 / 832850.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832250.0 / 832050.0 / 832050.0 /	91.34152 ( 7,18) 58.24523 ( 35,17) 61.98404 ( 71,18) 69.63164 (358, 9) 77.44769 (358, 9) 81.14822 ( 11, 9) 57.08556 (360,17) 62.02561 ( 34,18) 64.23365 (269, 9) 54.96278 (220, 9) 70.62807 (314, 9) 78.94964 (314, 9) 76.17154 ( 8,10) 75.80680 ( 11,10) 71.31501 ( 11,10) 51.49708 (332, 9) 56.68849 (332, 9) 56.68849 (332, 9) 56.68849 (332, 9) 56.681648 (348,18) 39.51825 (104,18) 37.93884 (317,10) 47.99458 (311, 9) 68.08134 (311, 9) 75.71748 (311, 9) 68.58147 (311, 9) 68.58147 (311, 9) 52.26603 (311, 9) 42.10582 (353, 9) 44.62589 (353, 9) 54.76083 (353, 9)	102.88610 (7,18) 61.31556 (327,18) 67.78880 (71,18) 69.86608 (358, 9) 76.00304 (358, 9) 79.32898 (11, 9) 61.07643 (360,17) 69.06527 (269, 9) 60.69955 (2, 9) 58.37798 (349,10) 83.76605 (314, 9) 82.28010 (8,10) 71.85188 (11,10) 78.45984 (11,10) 53.34936 (11,10) 60.84662 (32, 9) 68.02048 (348,18) 72.55465 (348,18) 58.7759 (348,18) 58.7759 (348,18) 58.7759 (348,18) 58.7759 (348,18) 58.7759 (348,18) 72.55465 (348,18) 58.7759 (348,18) 58.7759 (348,18) 75.93029 (311, 9) 77.49825 (311, 9) 63.71863 (311, 9) 43.78217 (311, 9) 51.74159 (353, 9) 51.74159 (353, 9) 52.55001 (353, 9)	110.27060 ( 7,18) 67.59715 ( 6,17) 73.98219 ( 71,18) 73.95171 (123,18) 72.95121 (358, 9) 73.26311 ( 11, 9) 67.99430 ( 58,15) 73.74049 (269, 9) 67.25606 (220, 9) 64.02869 (278, 9) 82.68014 (315, 9) 74.69387 ( 8,10) 82.72899 ( 11,10) 62.38605 ( 11,10) 64.69493 (332, 9) 70.15744 (348,18) 76.14425 (348,18) 76.14425 (348,18) 76.14425 (348,18) 76.14425 (348,18) 76.14425 (348,18) 76.14425 (348,18) 76.14425 (348,18) 76.14425 (348,18) 75.23638 (104,18) 43.64085 (317,10) 67.52291 (311, 9) 82.00008 (311, 9) 75.43754 (351, 9) 53.27417 (353, 9) 53.27417 (353, 9) 55.74165 (353, 9) 51.74818 (353, 9) 50.70461 ( 42, 9) 57.16648 ( 11,10)	109.68140 ( 7,18) 76.67667 ( 6,17) 80.32944 ( 71,18) 80.51913 (123,18) 78.99385 (214,18) 76.86343 ( 38,13) 77.25133 ( 58,15) 70.92673 ( 48,15) 70.16792 (220, 9) 75.27574 (314, 9) 83.08936 ( 8,10) 81.47154 ( 11,10) 71.38988 ( 11,10) 67.72025 (332, 9) 71.45918 (348,18) 61.07694 (348,18) 48.05845 (104,18) 48.91045 (311, 9) 77.44595 (311, 9) 84.53131 (311, 9) 68.56477 (311, 9) 84.53139 (353, 9) 59.86162 (353, 9) 59.86162 (353, 9) 52.79703 ( 42, 9) 52.40553 ( 42, 9) 51.25688 ( 42, 9) 49.45759 ( 42, 9)	101.32370 ( 3, 9) 85.61739 ( 6,17) 87.19508 ( 35,17) 87.31964 (123,18) 85.24006 (214,18) 80.56306 ( 38,13) 84.90576 ( 58,15) 80.51345 (220, 9) 76.97878 (278, 9) 81.86824 (315, 9) 74.55026 ( 59, 9) 74.55026 ( 59, 9) 74.55026 ( 32, 9) 71.40874 (348,18) 81.69976 (348,18) 81.69976 (348,18) 81.69976 (348,18) 52.50757 (317,10) 59.21013 (311, 9) 84.62320 (311, 9) 81.08055 (311, 9) 84.62320 (353, 9) 63.22182 (353, 9) 63.22182 (353, 9) 65.20012 (353, 9) 65.20012 (353, 9) 55.04340 ( 42, 9) 54.40980 (322, 9) 51.29826 ( 42, 9) 51.29826 ( 322, 9) HIGH 1-HR SGROUP
نہ ـــ		*** HL	JNG SHUI KIU (CHIMNEYS'	( EMISSION)	***	
		* HIGHE	* FR	NCENTRATION (MICROGRAMS ROM ALL SOURCES * THE RECEPTOR GRID *	S/CUBIC METER) *	
		* MAXIMUM	VALUE EQUALS 402.06	5100 AND OCCURRED AT (	818100.0, 832000.0)	*
L	Y-AXIS / (METERS) /	817750.0	817800.0	X-AXIS (METERS) 817850.0	817900.0	817950.0
	833500.0 /	109.05070 ( 3, 9)		99.34386 (208,18)	122.11800 ( 2,17)	139.32970 (161,18)
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833450.0 /	92.82912 ( 6,17)	98.15924 ( 9,16)	101.71670 (342,12)	99.34693 (342,12)	96.96996 (248,14)	
833400.0 /	93.47961 (35,17)	97.49561 (35,17)	96.83939 ( 35,17)	92.35488 ( 6,17)	95.66190 (259,12)	
833350.0 /	93.90553 (123,18)	99.40966 (123,18)	102.26250 (123,18)	99.84527 (123,18)	96.85567 (251,17)	
833300.0 /	90.67371 (214,18)	94.05123 (214,18)	99.52322 ( 38,13)	100.03060 ( 38,13)	96.41351 (194,14)	ني
833250.0 /	81.41224 ( 38,13)	90.24986 ( 58,15)	100.46600 ( 58,15)	101.19170 (48,15)	94-29044 (126,16)	
833200.0 /	90.91988 ( 48,15)	90.33936 (48,15)	100.34170 (220, 9)	94.99596 (220, 9)	96.65401 (278, 9)	
833150.0 /	86.97901 (220, 9)	89.98569 (278, 9)	97.98513 (278, 9)	101.52120 (105, 9)	90.15661 ( 52,10)	
833100.0 /	84.36998 (278, 9)	89.35098 (105, 9)	94.87326 (105, 9)	90.99799 (42,11)	101.75200 (236, 9)	
833050.0 /	83.01803 (105, 9)	78.40160 (105, 9)	90.16818 (42,11)	97.99239 ( 52,17)	100.58320 (277, 9)	L.
833000.0 /	80.52456 ( 11,10)	83.08245 ( 42,11)	89.95755 ( 52,17)	93.36450 (277, 9)	76.29153 (277, 9)	
832950.0 /	74.03675 ( 42,11)	80.38265 ( 52,17)	83.86906 (277, 9)	74.50397 (277, 9)	90.13869 ( 50,17)	
832900.0 /	71.08084 ( 52,17)	81.33624 (348,18)	69.55731 (277, 9)	75.84911 ( 50,17)	88.34648 ( 35,13)	1
832850.0 /	82.65910 (348,18)	63.54397 (277, 9)	62.80361 ( 50,17)	79.21883 ( 50,17)	80.69574 (271,18)	L
832800.0 /	59.25565 ( 10,10)	60.92876 (317,10)	76.60555 (311, 9)	71.85284 (35,13)	81.70888 (353, 9)	
832750.0 /	57.23512 (317,10)	76.47679 (311, 9)	65.82993 (35,13)	78.82657 (353, 9)	74.89165 (42,9)	
832700.0 /	69.27370 (311, 9)	79.99175 (311, 9)	64.65524 (353, 9)	82.44447 (353, 9)	76.10193 (42, 9)	Г
832650.0 /	86.54568 (311, 9)	54.14476 (35,13)	79.10106 (353, 9)	70.05048 (353, 9)	72.10114 ( 42, 9)	
832600.0 /	70.13648 (311, 9)	67.08491 (353, 9)	78.65118 (353, 9)	69.25877 (42, 9)	79.54152 (309.10)	L.
832550.0 /	53.38006 (353, 9)	75.63052 (353, 9)	66.96971 (353, 9)	66.60162 (42,9)	79.55470 (309,10)	
832500.0 /	66.06087 (353, 9)	73.02741 (353, 9)	64.22478 (42,9)	71.52798 (309,10)	77.15853 (22, 9)	
832450.0 /	70.57793 (353, 9)	62.52437 (353, 9)	62.20926 ( 42, 9)	74.28854 (309,10)	75.25510 (22, 9)	
832400.0 /	66.90519 (353, 9)	60.38446 (42,9)	63.47109 (309.10)	71.61034 (309,10)	69.43043 (22, 9)	
832350.0 /	57.67583 (353, 9)	58.70485 (42,9)	67 23009 (309,10)	69.90926 ( 22, 9)	66.68578 (274, 9)	
832300.0 /	57.30262 (42,9)	56.90002 (309,10)	66.97396 (309,10)	67.65060 (22, 9)	68.23920 (274, 9)	
832250.0 /	55.83645 (42,9)	60.75734 (309,10)	63.44075 (309,10)	62,92491 (22, 9)	67.66685 (274, 9)	
832200.0 /	53.34697 (42,9)	61.77227 (309,10)	63.15384 (22, 9)	60.22713 (274, 9)	65.39502 (274, 9)	
832150.0 /	55.49064 (309,10)	60.16820 (309,10)	60.94863 (22, 9)	61.49271 (274, 9)	61_93072 (274, 9)	
832100.0 /	56.97020 (309.10)	58.13680 (22, 9)	57.09286 ( 22, 9)	61,37286 (274, 9)	60.09825 (274, 9)	
832050.0 /	56.47447 (309,10)	57,49421 (22,9)	55.30994 (274, 9)	60.15633 (274, 9)		
832000.0 /	76.75300 (348,18)	111.44620 ( 35,20)	210.44740 (311, 9)	155.10020 (353, 9)	151.36800 (274, 9)	
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#### \*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

# \* HIGHEST 1-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) \* FROM ALL SOURCES \* \* FOR THE RECEPTOR GRID \*

	* MAXIMUM	VALUE EQUALS 4	02.06100 AND OCCURR	ED AT ( 818100.0	, 832000.0) *		ت_)
Y-AXIS /			X-AXIS (M	ETERS)			Г
(METERS) /	818000.0	818050.0	818100	.0 8'	18150.0	818200.0	}
					• • • • • • •		<u> </u>
833500.0 /	139.14680 (169, 9)	133.56330 (202,1)	J) 124.66050 (15	5 18) 116 5811(	(123,12)	103.56200 (117, 9)	_
833450.0 /	98.82685 (135,14)	91.41782 (213,1	B) 89.29675 (10		7 (106,15)	53.59219 (131,11)	Γ
833400.0 /	98.70586 (196,12)	84.49510 (216.1			7 (135,12)	47.25750 (220,10)	
833350.0 /	97.18684 (251,17)	82.79659 (135,1)			3 (251,16)	50.55739 ( 46,13)	· •
833300.0 /	94.23660 (194,14)	98.91244 (203,14			3 (251,16)	51.20642 (149, 9)	
833250.0 /	87.53699 (126,16)	94.47867 (207.1)			(251,16)	49.80814 (348,15)	
833200.0 /	94.75215 ( 29,14)	86.28033 (105,1)			2 (251,15)	85.34959 (197,13)	
833150.0 /	94.31381 ( 42,11)	97.55790 ( 46,14	4) 97.27705 (17)		(251,15)	86.96780 (152,14)	L
833100.0 /	100.27680 (277, 9)	90.83006 ( 57,1			(218,16)	88.46977 (261,15)	
833050.0 /	87.29899 (12.11)	100.24330 ( 35,1)			(245,15)	93.21052 (261,15)	<b>F</b> -3
833000.0 /	100.86570 ( 50,17)	100.78010 (271.1)				102.78510 ( 58,16)	
832950.0 /	92.48988 (271,18)	97.15551 (358.1)				105.00380 ( 58,16)	
832900.0 /	89.03725 (271,18)	96.08839 (42,	9) 94.19174 ( 6	1.16) 88.8492	1 (281, 9)	101.59110 ( 58,16)	Ļ
832850.0 /	84.22833 (42, 9)	84.90997 (341,1			7 (281, 9)	95.44476 ( 58,16)	
832800.0 /	85.35062 (42,9)	81.66615 ( 61.1			5 (281, 9)	88.27295 (58,16)	
832750.0 /	78.58389 (42, 9)	81.13044 ( 22,	9) 78.37581 (27	4, 9) 84.2347	9 (281, 9)	82.24539 ( 8,11)	
832700.0 /	83.59415 (309,10)	74.60475 (274,			5 (281, 9)	78.37302 ( 8,11)	
832650.0 /	82.17493 ( 22, 9)	81.87891 (274,	9) 77.99503 (	8, 9) 73.8543	5 ( 58, 16)	77.93496 (323,18)	
832600.0 /	81.47315 ( 22, 9)	82.83599 (274,	9) 85.27755 (	8, 9) 69.5277	3 ( 58, 16)	82.88744 (323,18)	r~~
832550.0 /	74.56250 ( 22, 9)	79.08142 (274,	9) 87.06872 (	8, 9) 65,1195	7 ( 58,16)	86.27435 (323,18)	
832500.0 /	74.75446 (274, 9)	72.43617 (274,	9) 84.61157 (	8, 9) 60.8087	5 ( 58,16)	88.34831 (323,18)	
832450.0 /	76.40927 (274, 9)	76.13558 ( 8,	9) 79.33044 (	8, 9) 56.6965	5 ( 58,16)	89.35122 (323,18)	•
832400.0 /	74.74978 (274, 9)	83.25138 ( 8,	9) 72.47044 (	8, 9) 54.5716	0 (323,18)	89.50142 (323,18)	
832350.0 /	70.66797 (274, 9)	86.53914 ( 8,		8,9) 58.9266	6 (323,18)	88.98698 (323,18)	_ <b>∏</b>
832300.0 /	65.12577 (274, 9)	86.32003 ( 8,			0 (323,18)	87.58167 (323,18)	
832250.0 /	66.14587 ( 8, 9)	83.70465 ( 8,		4,9) 64.9188	3 (323,18)	85.90022 (323,18)	L
832200.0 /	72.04396 ( 8, 9)	80.42207 ( 8,			2 (323,18)	84.05972 (323,18)	
832150.0 /	77.36387 ( 8, 9)	76.82578 ( 8,		· · · ·	1 (323,18)	82.11665 (323,18)	£ 15
832100.0 /	85.81789 ( 8, 9)	71.89427 ( 8,			6 (323,18)	80.11548 (323,18)	1
832050.0 /	91.40611 ( 8, 9)	67.88258 ( 8,			3 (323,18)	78.09467 (323,18)	L
832000.0 /	129.66660 ( 8, 9)	156.72960 ( 4,	9) 402.06100 (	4,9) 194.0695	0 (323,18)	143.92130 (323,18)	

\*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

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SGROUP

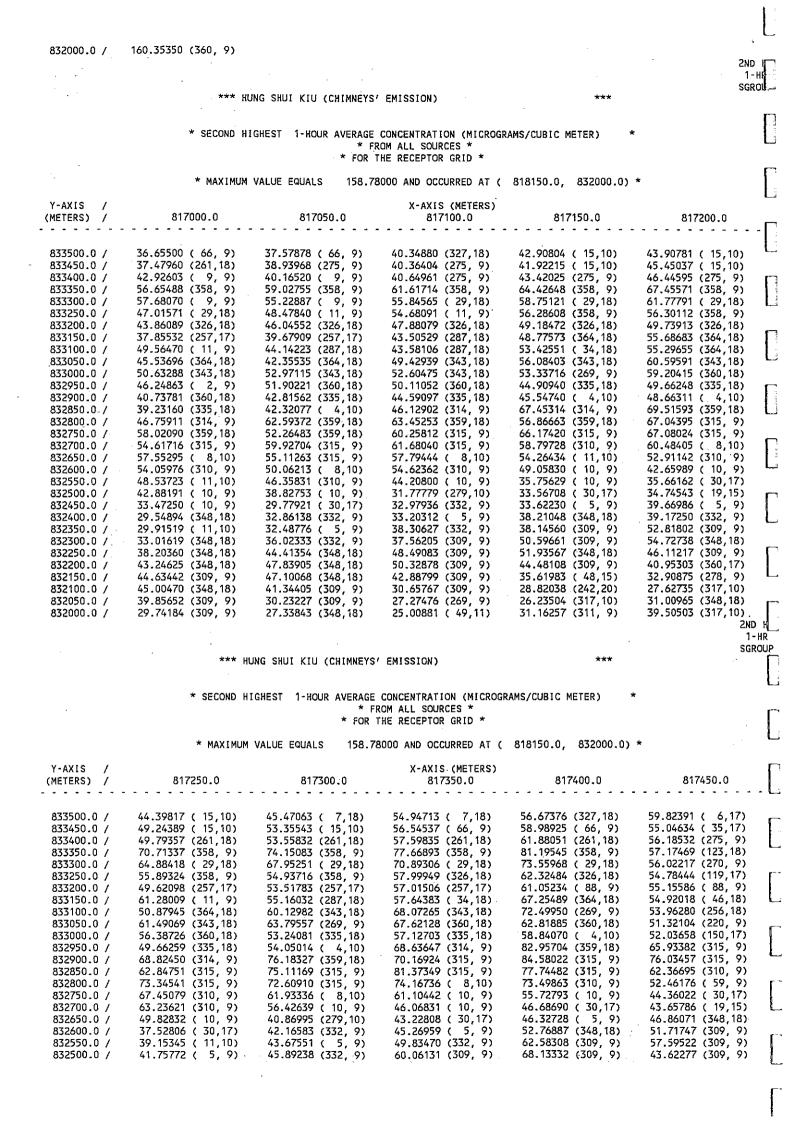
HIGH 1-HR SGROU

\* HIGHEST 1-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) \* FROM ALL SOURCES \*

## \* FOR THE RECEPTOR GRID \*

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		* MAXIMUM *	ALUE EQUALS 402.0	06100 AND OCCURRED AT (	818100.0, 832000.0)	*
	Y-AXIS / (METERS) /	818250.0	818300.0	X-AXIS (METERS) 818350.0	818400.0	818450.0
	833500.0 / 833450.0 / 833450.0 / 833450.0 / 833250.0 / 833250.0 / 833250.0 / 83250.0 / 832950.0 / 832950.0 / 832950.0 / 832950.0 / 832650.0 / 832650.0 / 832650.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832250.0 / 83200.0 /	108.35640 (123,16) 45.85555 (200,10) 51.34446 (271,14) 51.25290 ( $75,12$ ) 51.71737 (220,10) 56.93005 (125,14) 102.07240 (135,12) 110.39430 (135,12) 112.22890 ( $10,12$ ) 107.55130 ( $10,12$ ) 108.16390 ( $76,14$ ) 109.30300 ( $76,14$ ) 109.30300 ( $76,14$ ) 100.76020 ( $76,14$ ) 107.9560 ( $8,11$ ) 89.22613 ( $8,11$ ) 87.92613 ( $8,11$ ) 77.91693 ( $8,11$ ) 77.91693 ( $8,11$ ) 67.93272 ( $8,11$ ) 67.93273 ( $237,9$ ) 59.99521 ( $237,9$ ) 54.99417 ( $237,9$ ) 53.56716 ( $323,18$ ) 52.85213 ( $323,18$ ) 52.04249 ( $323,18$ ) 50.23868 ( $323,18$ ) 92.98611 ( $340,17$ )	115.52830 (274,12) 51.59096 (149,10) 53.94205 (200,10) 52.14876 (326,15) 50.14328 (131,10) 81.21339 (131,11) 101.11990 (304,13) 120.21560 (46,13) 125.85720 (149, 9) 118.94690 (348,15) 124.34260 (340,16) 121.78780 (340,16) 117.17970 (353,12) 109.47050 (353,12) 109.47050 (353,12) 109.47050 (353,12) 109.47050 (353,12) 109.47050 (237, 9) 95.85027 (237, 9) 95.85027 (237, 9) 91.32114 (237, 9) 93.67750 (237, 9) 93.67750 (237, 9) 93.63690 (237, 9) 82.00432 (237, 9) 82.00432 (237, 9) 75.07478 (237, 9) 75.07478 (237, 9) 68.37578 (237, 9) 68.37578 (237, 9) 68.37578 (237, 9) 68.37578 (237, 9) 68.37578 (237, 9) 68.37578 (237, 9) 86.09171 (340,13)	120.45510 (277,13) 92.20793 (251,14) 61.26640 (182,14) 61.47811 (131,12) 70.09254 (149,12) 74.91182 (127,12) 115.48140 (131,11) 130.47180 (75,12) 131.59990 ( $3,10$ ) 140.48460 (252, 9) 132.39800 (252, 9) 129.05160 (348,15) 124.68020 (348,15) 13.13250 (348,15) 105.11110 (340,16) 98.76303 (340,16) 91.02700 (340,16) 93.76303 (340,16) 91.02700 (340,16) 83.53831 (342,18) 83.13070 (237, 9) 90.66065 (237, 9) 91.78278 (237, 9) 91.65582 (237, 9) 91.65582 (237, 9) 91.65582 (237, 9) 84.05013 (237, 9) 84.05013 (237, 9) 81.36336 (237, 9) 75.69964 (237, 9) 117.22860 ( $9, 8$ )	119.33200 ( $35,14$ ) 84.81204 (170,15) 97.57313 (197,14) 90.07893 ( $64,14$ ) 97.78715 (131,13) 101.91610 (219,14) 111.96760 (200,10) 126.28220 (326,15) 135.45060 ( $77,18$ ) 129.68940 ( $3,10$ ) 143.58590 ( $42,10$ ) 136.41650 (252, 9) 129.61620 (252, 9) 111.79700 (252, 9) 111.56990 (333, 9) 111.56990 (333, 9) 111.56990 (333, 9) 111.56990 (342,18) 107.52520 (342,18) 107.52520 (342,18) 107.5250 (342,18) 107.57550 (360, 9) 72.06456 (360, 9) 72.06456 (360, 9) 72.79601 (237, 9) 74.01659 (237, 9) 74.01659 (237, 9) 74.44279 (237, 9) 74.88137 (237, 9) 141.97180 ( $6, 9$ )	119.12080 (170,15) 82.70554 (156,17) 94.13629 (123,14) 92.74429 (52,16) 94.24628 (131,13) 97.32346 (227,16) 109.75690 (149,10) 113.37590 (200,10) 126.74570 (72,13) 139.50490 (39,11) 137.22100 (77,18) 125.21860 (3,10) 127.68380 (42,10) 111.66000 (252, 9) 100.52000 (252, 9) 101.24620 (333, 9) 111.75150 (333, 9) 111.0630 (323, 9) 111.0640 (310,10) 106.44420 (310,10) 101.97070 (342,18) 99.26939 (342,18) 94.89014 (15, 9) 92.31763 (360, 9) 84.88000 (360, 9) 72.98430 (360, 9) 125.45370 (360, 9) HIGH 1-HR
		*** HU	NG SHUI KIU (CHIMNEY	S' EMISSION)	***	SGROUP
	,	* HIGHE				
	-		*	DNCENTRATION (MICROGRAMS FROM ALL SOURCES * THE RECEPTOR GRID *	/CUBIC METER) *	•
L	j	1	* * FOR	FROM ALL SOURCES *		*
	Y-AXIS / (METERS) /	1	* * FOR	FROM ALL SOURCES * THE RECEPTOR GRID *		*



832450.0 / 832400.0 / 832350.0 / 832250.0 / 832250.0 / 832200.0 / 8322150.0 / 832150.0 / 832200.0 / 83200.0 /	42.35077 (332, 9) 55.14729 (309, 9) 57.80727 (348,18) 47.76479 (309, 9) 46.95424 (214,18) 44.60711 (48,15) 30.15703 (278, 9) 32.58061 (277, 9) 44.09169 (317,10) 44.86507 (1,11)	57.56987 (309, 9) 61.20664 (348,18) 49.41519 (309, 9) 39.30037 ( 9, 9) 41.81043 (214,18) 33.48085 (126,16) 30.78208 (353, 9) 45.48278 ( 50,17) 48.59969 ( 35,13) 55.43859 (353, 9)	64.65125 (309, 9) 51.02969 (309, 9) 34.90218 ( 10,10) 33.15682 (104,18) 32.84309 ( 28, 9) 33.08106 (353, 9) 46.55802 ( 50,17) 48.68243 ( 42, 9) 51.09070 ( 42, 9) 43.78784 ( 42, 9)	52.56094 (309, 9) 37.40811 (104,18) 35.34012 (49,11) 40.22679 (311, 9) 34.45607 (353, 9) 34.13579 (353, 9) 34.58491 (353, 9) 36.26017 (353, 9) 39.07343 (353, 9) 42.44571 (353, 9)	36.85567 (104,18) 35.16164 (49,11) 33.70927 (317,10) 31.20749 (353, 9) 30.82475 (353, 9) 31.93078 (353, 9) 34.65193 (353, 9) 38.46832 (353, 9) 38.07315 (42, 9) 45.49704 (315, 9) 2ND HI 1-HR
	*** HU	NG SHUI KIU (CHIMNEYS'	EMISSION)	***	SGROUP
	* SECOND HI	* FR	CONCENTRATION (MICROGR ROM ALL SOURCES * THE RECEPTOR GRID *	AMS/CUBIC METER) *	
	* MAXIMUM			818150.0, 832000.0)	*
Y-AXIS / (METERS) /	817500.0	817550.0	X-AXIS (METERS) 817600.0	817650.0	817700.0
833500.0 /         833450.0 /         833450.0 /         83340.0 /         83350.0 /         83350.0 /         83350.0 /         83350.0 /         83350.0 /         83350.0 /         83350.0 /         83350.0 /         83350.0 /         833100.0 /         83300.0 /         83200.0 /         83200.0 /         83200.0 /         832700.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         83250.0 /         832250.0 /         832200.0 /         832100.0 /         832100.0 /         83200.0 /         83200.0 /         83200.0 /	71.24504 ( 17, 9) 57.37553 (327, 18) 60.08369 ( 35, 17) 62.23049 (123, 18) 60.86414 (214, 18) 60.23978 (119, 17) 55.96241 ( 88, 9) 60.06201 (269, 9) 56.32040 (363, 9) 53.69504 (349, 10) 62.89442 (359, 18) 78.52766 (315, 9) 67.67100 (315, 9) 60.28233 ( 59, 9) 48.51524 (279, 10) 47.38495 ( 19, 15) 46.66070 (348, 18) 52.53703 (309, 9) 59.57821 (309, 9) 43.77801 (309, 9) 39.51801 ( 1, 10) 37.93719 ( $49, 111$ ) 35.09024 ( $317, 10$ ) 32.10068 ( $50, 17$ ) 33.20586 ( 1, 11) 34.79146 ( $42, 9$ ) 37.09129 ( $42, 9$ ) 37.09129 ( $42, 9$ ) 43.31467 ( $42, 9$ ) 48.32695 ( 8, 10)	$\begin{array}{c} 84.26485 & (17, 9) \\ 61.03468 & (35, 17) \\ 66.24743 & (35, 17) \\ 67.82805 & (123, 18) \\ 66.53218 & (214, 18) \\ 65.98318 & (119, 17) \\ 58.70624 & (58, 15) \\ 64.98036 & (48, 15) \\ 60.60077 & (220, 9) \\ 57.65594 & (150, 17) \\ 70.14315 & (315, 9) \\ 79.22441 & (315, 9) \\ 79.22441 & (315, 9) \\ 79.22441 & (315, 9) \\ 79.22441 & (315, 9) \\ 66.11811 & (59, 9) \\ 52.82055 & (279, 10) \\ 51.44291 & (332, 9) \\ 49.41490 & (48, 17) \\ 52.56324 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23855 & (309, 9) \\ 61.23854 & (42, 9) \\ 43.60229 & (49, 11) \\ 36.09824 & (317, 10) \\ 34.73677 & (50, 17) \\ 36.20230 & (1, 11) \\ 38.29254 & (42, 9) \\ 40.88691 & (353, 9) \\ 42.72254 & (42, 9) \\ 44.74886 & (42, 9) \\ 44.74886 & (42, 9) \\ 47.75249 & (42, 9) \\ 48.52327 & (42, 9) \\ 48.52327 & (42, 9) \\ \end{array}$	91.38165 ( 17, 9) 66.31967 ( 83,18) 72.97698 ( 35,17) 73.95171 (161,17) 72.63512 (214,18) 71.70424 ( 38,13) 63.46560 ( 48,15) 69.52924 ( 48,15) 55.61242 (349,10) 62.87309 (314, 9) 78.25413 ( 8,10) 67.29719 ( 59, 9) 60.25233 ( 59, 9) 55.13116 ( 30,17) 53.10880 ( 48,17) 54.47572 (332, 9) 62.12086 (309, 9) 47.35236 ( 10,10) 45.23633 ( 1,10) 43.64053 ( 49,11) 37.91787 ( 50,17) 38.33332 ( 1,11) 39.45161 ( 42, 9) 41.57899 ( 42, 9) 43.82924 ( 42, 9) 47.98650 ( 42, 9) 47.98650 ( 42, 9) 45.52824 ( 353, 9) 50.32158 ( 42, 9)	87.05111 (17, 9) 75.33212 (83,18) 80.09417 (35,17) 80.51913 (161,17) 77.19345 (270, 9) 76.86343 (119,17) 74.16737 (48,15) 70.57483 (269, 9) 64.20931 (349,10) 71.52000 (315, 9) 77.76349 (315, 9) 69.72943 (59, 9) 58.95452 (42,11) 57.72894 (236, 9) 59.39050 (332, 9) 62.17608 (309, 9) 51.35246 (10,10) 48.05843 (1,10) 48.05843 (1,10) 42.35268 (42, 9) 44.59842 (42, 9) 44.59842 (42, 9) 44.59842 (42, 9) 47.02217 (42, 9) 49.31474 (42, 9) 52.37829 (42, 9) 41.10470 (105, 9) 44.88545 (11,10) 45.70105 (309,10)	97.50758 ( 7,18) 84.26239 ( 83,18) 86.36465 ( 71,18) 87.31964 (161,17) 82.46457 (270, 9) 80.56306 (119,17) 84.18430 ( 48,15) 67.34240 ( 48,15) 67.34240 ( 48,15) 66.76777 (220, 9) 78.80068 ( 8,10) 71.82380 ( 11,10) 63.53251 ( 42,11) 64.33507 (332, 9) 61.04484 (309, 9) 55.42246 ( 10,10) 52.50746 ( 49,11) 47.92600 (317,10) 46.84233 ( 50,17) 46.77026 ( 1,11) 44.77082 ( 42, 9) 52.70120 ( 42, 9) 52.70120 ( 42, 9) 53.18561 (353, 9) 43.37812 (353, 9) 43.37812 (353, 9) 44.74258 (309,10) 48.49572 (309,10) 48.57923 ( 42, 9) 59.34700 (309,10) 2ND HI 1-HR
	*** HU	NG SHUI KIU (CHIMNEYS'	EMISSION)	***	SGROUP
	* SECOND HI	* F.	CONCENTRATION (MICROG ROM ALL SOURCES * THE RECEPTOR GRID *	RAMS/CUBIC METER) *	
<b>L</b>		VALUE EQUALS 158.78	3000 AND OCCURRED AT (	818150.0, 832000.0)	*
Y-AXIS / (METERS) /	817750.0	817800.0	X-AXIS (METERS) 817850.0	817900.0	817950.0
833500.0 / 833450.0 / 833400.0 / 833350.0 / 833350.0 / 833250.0 / 833250.0 / 833150.0 / 833150.0 / 833150.0 / 833050.0 / 833000.0 / 832950.0 /	101.21460 (342,12) 92.29639 (9,16) 91.23642 (71,18) 93.90553 (161,17) 86.69151 (270, 9) 81.41224 (119,17) 88.34650 (58,15) 71.08780 (278, 9) 69.07013 (105, 9) 75.00877 (8,10) 66.22643 (42,11) 70.91965 (236, 9)	96.20242 ( 3, 9) 97.37859 ( 29,16) 93.49398 ( 71,18) 99.40966 (161,17) 93.18880 ( 38,13) 83.44352 ( 48,15) 88.58018 (220, 9) 83.04050 (220, 9) 78.82485 (278, 9) 72.85366 ( 11,10) 76.66483 (236, 9) 77.49576 (236, 9)	102.26250 (161,17) 99.52322 (119,17) 96.56528 (48,15) 77.98869 (342,16) 80.94371 (105, 9)	90.10128 (171,17) 92.28648 (83,18) 99.84527 (161,17) 100.03060 (119,17) 100.39800 (58,15) 93.92007 (278,9) 83.14422 (261,17) 82.94305 (131,9) 97.25393 (236,9)	137.97470 ( 2,17) 95.99666 (201,10) 93.40448 (196,12) 95.47990 (152,11) 89.42934 (196,18) 90.28445 (331,10) 91.09927 ( 7,11) 88.29706 (126, 9) 100.27770 ( 52,17) 100.58320 (341,15) 76.29152 (341,15) 85.14110 ( 35,13)

832900.0 / 832850.0 / 832800.0 / 832750.0 / 832700.0 / 832600.0 / 832600.0 / 832550.0 / 832500.0 / 832450.0 / 832400.0 / 832250.0 / 832250.0 / 832250.0 / 832250.0 / 832100.0 / 832050.0 /	69.45939 ( 46,16) 65.80208 (277, 9) 59.25565 (361,10) 57.23510 ( 49,11) 51.47595 ( 50,17) 52.55167 ( 50,17) 49.71660 ( 35,13) 47.98622 (361,11) 51.57155 ( 60, 9) 54.57831 ( 60, 9) 56.36790 ( 42, 9) 57.51641 ( 42, 9) 46.09734 (353, 9) 47.12840 (309,10) 52.06885 (309,10) 52.06885 (309,10) 52.147039 (341,18) 52.07557 ( 22, 9) 76.64870 (309, 9)	74.39188 (277, 9) 63.54382 (341,15) 60.92875 (22,17) 59.66745 (50,17) 58.77164 (50,17) 52.50356 (361,11) 54.09226 (60, 9) 60.15607 (60, 9) 58.42891 (42, 9) 60.35568 (42, 9) 48.73598 (353, 9) 50.54792 (309,10) 55.68695 (42, 9) 54.89188 (341,18) 54.78564 (341,18) 57.03950 (22, 9) 56.50891 (309,10) 53.21892 (236, 9) 110.03200 (355,14)	69.55727 (341,15) 62.24284 ( 22,17) 69.30993 ( 50,17) 64.61311 ( 50,17) 58.68967 (271,18) 65.43993 ( 60, 9) 63.96959 ( 60, 9) 63.82382 ( 42, 9) 50.78113 (353, 9) 55.67262 (309,10) 58.40857 ( 42, 9) 59.52190 (341,18) 60.52620 ( 22, 9) 63.14124 ( 22, 9) 57.69104 (309,10) 57.33667 ( 42,11) 53.78714 (277, 9) 52.19370 (277, 9) 120.18350 ( 22,19)	69.64513 ( 35,13) 78.14693 ( 35,13) 68.28139 ( 50,17) 68.91811 ( 60, 9) 70.36489 ( 60, 9) 68.40079 ( 42, 9) 55.34324 (358,10) 62.64093 (309,10) 61.55427 ( 42, 9) 63.48112 ( 22, 9) 63.48112 ( 22, 9) 65.09212 (309,10) 56.62818 (309,10) 57.50758 (274, 9) 57.76375 ( 42,11) 55.38695 (277, 9) 50.23088 ( 46,14) 51.44515 ( 35,13) 118.98690 ( 60, 9)	86.41800 ( 50,17) 73.28797 ( 35,13) 74.76329 ( 60, 9) 69.90659 (353, 9) 65.62091 (358,10) 70.81531 (309,10) 64.97290 ( 42, 9) 73.53558 ( 22, 9) 73.02643 (309,10) 62.91723 (309,10) 62.91723 (309,10) 62.72031 (274, 9) 61.36584 ( 22, 9) 52.57233 ( 22, 9) 46.70669 (319, 9) 50.96502 ( 46,14) 45.81185 ( 35,13) 51.62800 ( 8, 9) 58.10537 ( 8, 9) 129.90240 ( 8, 9) 2ND H 1-HH		
	* SECOND HI		CONCENTRATION (MICROG ROM ALL SOURCES * THE RECEPTOR GRID *	RAMS/CUBIC METER) *			
	* MAXIMUM	VALUE EQUALS 158.78	3000 AND OCCURRED AT (	818150.0, 832000.0)	*		
Y-AXIS / (METERS) /	818000.0	818050.0	X-AXIS (METERS) 818100.0	818150.0	818200.0		
833450.0 / 833400.0 / 833350.0 / 833250.0 / 833250.0 / 833200.0 / 833150.0 / 833100.0 / 833050.0 / 832950.0 / 832950.0 / 832850.0 / 832850.0 / 832850.0 / 832850.0 / 832850.0 /	128.62480 (258,18) 96.06396 (201,10) 97.37476 (119,18) 96.01855 (152,11) 93.11623 (127, 9) 84.03279 (280,13) 91.07760 (126,10) 92.94283 (236, 9) 100.27680 (341,15) 85.14711 (57,17) 99.02117 (35,13) 91.20308 (35,13) 76.19328 (358,10) 83.04644 (358,10) 83.04644 (358,10) 77.21124 (309,10) 74.10525 (22, 9) 78.80431 (309,10) 67.47806 (319, 9) 50.16285 (319, 9) 48.54699 (8, 9) 58.16980 (8, 9) 58.891192 (274, 9) 57.82046 (226, 9) 62.18078 (281, 9) 76.99667 (281, 9)	131.65640       (169,10)         91.35459       (171,15)         84.24819       (119,18)         80.39601       (312,13)         84.12926       (205,14)         91.75146       (108,12)         82.30454       (261,14)         95.64491       (261,14)         95.64491       (261,14)         95.95262       (360,16)         95.25220       (42,9)         93.23341       (341,16)         84.41674       (42,9)         78.53060       (22,9)         75.16044       (61,16)         73.95211       (22,9)         68.90701       (319,9)         63.22824       (226,9)         57.51741       (226,9)         57.51741       (226,9)         65.32034       8,9)         64.42085       (274,9)         63.10831       (274,9)         45.31979       (281,9)         56.10831       (274,9)         45.43172       (281,9)         54.27349       (281,9)         54.27349       (281,9)         54.27349       (281,9)         54.26466       (281,9)         56.46866       (281,9	78.73161 (274, 9) 77.80352 (226, 9) 68.59986 (226, 9) 66.74514 (281, 9) 64.92220 (281, 9) 62.30349 (281, 9) 59.22288 (281, 9) 55.92117 (281, 9) 52.56412 (281, 9) 49.42474 (58,16) 47.43736 (58,16) 51.55597 (281, 9) 57.17341 (281, 9) 58.97840 (58,16)	114.39270 (205,12) 73.88132 (197,11) 42.74731 (149, 9) 51.71176 (313,12) 51.65401 (313,12) 76.43499 (104,14) 87.31818 (218,16) 89.93262 (245,15) 91.19380 (61,16) 89.82542 (22,10) 84.09182 (77, 9) 86.63092 (226, 9) 81.42146 (58,16) 82.44110 (58,16) 80.90120 (58,16) 77.80238 (58,16) 72.82388 (281, 9) 61.44072 (281, 9) 56.29110 (281, 9) 52.79586 (348,14) 52.83475 (58,16) 49.24454 (58,16) 49.24454 (58,16) 50.83872 (8,11) 55.52771 (8,11) 55.20560 (8,11) 54.08392 (8,11) 55.20560 (61,20)	95.65446 (216,15) 37.88671 (108,10) 45.28329 (339,15) 48.97980 (220,10) 48.22461 (46,13) 49.76875 (149, 9) 75.99117 (251,15) 82.59338 (197,13) 85.52051 (152,14) 92.91481 (281, 9) 100.41240 (281, 9) 98.83701 (281, 9) 98.751948 (8,11) 85.49038 (8,11) 80.99246 (58,16) 74.05563 (58,16) 74.05563 (58,16) 74.24349 (8,11) 80.99246 (8,11) 70.08292 (8,11) 70.08292 (8,11) 51.84206 (8,11) 51.84206 (8,11) 51.84206 (8,11) 51.84206 (8,11) 51.84206 (8,11) 51.84206 (8,11) 51.4322 (8,11) 47.63128 (356, 9) 46.13432 (8,11) 113.11720 (22,14) 2ND H 1-HR		
	*** HL	NG SHUI KIU (CHIMNEYS'	EMISSION)	***	SGROUP		
* SECOND HIGHEST 1-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) * * FROM ALL SOURCES * * FOR THE RECEPTOR GRID *							
Y-AXIS /	* MAXIMUM	VALUE EQUALS 158.78	3000 AND OCCURRED AT ( X-AXIS (METERS)	818150.0, 832000.0)	*		
(METERS) /	818250.0	818300.0	818350.0	818400.0	818450.0		
833450.0 /	106.92330 (302,16) 45.50193 (266,12) 50.86794 (106,16)	92.77937 (216,13) 47.26927 (219,15) 53.68315 (266,12)	67.78086 (260,15)	117.39060 ( 33,17) 84.30018 (152,12) 72.05411 (304,16)	77.09228 (304,16)		

.

833350.0 /         833300.0 /         833300.0 /         833250.0 /         833200.0 /         833100.0 /         833100.0 /         833100.0 /         833100.0 /         83300.0 /         833000.0 /         832950.0 /         832950.0 /         832950.0 /         832850.0 /         832850.0 /         832650.0 /         832650.0 /         832650.0 /         832650.0 /         832650.0 /         832650.0 /         832650.0 /         832650.0 /         832250.0 /         832250.0 /         832250.0 /         832250.0 /         832200.0 /         832200.0 /         832150.0 /         832200.0 /         83200.0 /         83200.0 /         83200.0 /         83200.0 /         83200.0 /         83200.0 /         83200.0 /         83200.0 /         83200.0 /	51.13758 (131,10) 47.28318 (75,12) 52.68211 (252, 9) 82.49640 (125,14) 101.19640 (10,12) 103.75870 (251,16) 99.87525 (261,15) 102.74820 (8,11) 106.18870 (8,11) 104.63250 (8,11) 104.63250 (8,11) 104.63250 (8,11) 104.63250 (76,14) 81.93176 (76,14) 81.93176 (76,14) 76.03391 (76,14) 76.03391 (76,14) 70.54209 (76,14) 65.94330 (237, 9) 63.51402 (8,11) 59.46045 (8,11) 54.53787 (323,18) 54.15521 (323,18) 52.43996 (237, 9) 47.48743 (237, 9) 43.79060 (237, 9) 43.79060 (237, 9) 91.51950 (349,12)	51.26257 ( $42,12$ ) 49.52373 ( $39,11$ ) 65.22125 ( $261,13$ ) 100.97050 ( $220,10$ ) 113.42470 ( $149,9$ ) 121.89490 ( $69,14$ ) 117.71930 ( $69,14$ ) 117.71930 ( $69,14$ ) 117.43660 ( $353,12$ ) 121.21020 ( $353,12$ ) 121.21020 ( $353,12$ ) 113.10020 ( $340,16$ ) 105.49800 ( $77,11$ ) 100.44380 ( $353,12$ ) 91.64743 ( $237,9$ ) 88.30651 ( $77,11$ ) 70.18328 ( $77,11$ ) 70.18328 ( $77,11$ ) 70.18328 ( $77,11$ ) 64.92192 ( $77,11$ ) 60.76018 ( $76,14$ ) 55.33275 ( $76,14$ ) 50.02321 ( $76,14$ ) 46.96431 ( $76,14$ ) 45.58307 ( $22,14$ ) 44.23724 ( $22,14$ ) 42.91692 ( $22,14$ ) 41.62748 ( $22,14$ ) 85.17131 ( $237,9$ )	50.95211 (260,10) 69.13444 (234,12) 74.72964 (75,13) 113.17900 (271,14) 121.46470 (131,10) 130.81010 (42,10) 140.11100 (261,16) 132.06410 (261,16) 132.06410 (261,16) 109.14220 (252, 9) 105.72550 (340,16) 108.31590 (340,16) 99.28456 (348,15) 96.30437 (342,18) 90.87254 (342,18) 90.87254 (342,18) 83.41789 (353,12) 77.68649 (353,12) 77.68649 (353,12) 66.29137 (353,12) 61.20579 (353,10) 54.40816 (353,10) 51.09900 (353,10) 47.89523 (353,10) 44.82497 (353,10) 41.90451 (77,11) 39.45261 (77,11) 101.31560 (237, 9)	$\begin{array}{c} 73.93386 & (107,13) \\ 95.35721 & (234,12) \\ 86.99100 & (219,15) \\ 111.92320 & (266,12) \\ 125.06280 & (42,12) \\ 134.78180 & (22,13) \\ 119.76960 & (42,10) \\ 143.52820 & (3,10) \\ 136.18330 & (261,16) \\ 129.40310 & (261,16) \\ 117.37760 & (330, 9) \\ 111.34890 & (330, 9) \\ 111.34890 & (330, 9) \\ 105.78580 & (310,10) \\ 96.28000 & (310,10) \\ 91.19977 & (360, 9) \\ 90.32037 & (360, 9) \\ 78.30791 & (342,18) \\ 70.01099 & (342,18) \\ 64.71941 & (340,18) \\ 63.87782 & (340,18) \\ 59.84188 & (340,18) \\ 57.17457 & (340,18) \\ 54.31784 & (340,18) \\ 103.41380 & (237, 9) \\ \end{array}$	90.56843 (76,15) 94.12114 (188,10) 96.09170 (120, 9) 107.46560 (219,15) 113.34560 (266,12) 113.87830 (326,15) 134.46680 (77,18) 136.80900 (22,13) 117.76590 (42,10) 127.32650 (3,10) 115.12320 (252, 9) 111.52000 (261,16) 100.39600 (261,16) 101.11540 (330, 9) 111.59720 (330, 9) 112.93710 (330, 9) 107.86330 (333, 9) 101.45620 (342,18) 98.68941 (310,10) 96.79548 (15, 9) 94.35376 (342,18) 89.64272 (15, 9) 82.68433 (15, 9) 74.98943 (15, 9) 67.31250 (342,18) 60.69579 (342,18) 57.21486 (340,18) 105.34770 (340,18)
					2ND HI 1-HR SGROUP
-	· *** }	IUNG SHUI KIU (CHIMNEYS	' EMISSION)	***	
	* SECOND H		CONCENTRATION (MICROG ROM ALL SOURCES * THE RECEPTOR GRID *	RAMS/CUBIC METER) *	
	* MAXIMUM			818150.0, 832000.0)	
Y-AXIS / (METERS) /	818500.0		X-AXIS (METERS)		
		<b> </b>			
L 833500.0 /	125.17230 ( 36,11)		• • • • • • • • • • • • •		
	$\begin{array}{c} 125.17230 & ( \ 36, 11) \\ 88.62139 & ( \ 62, 18) \\ 90.10687 & ( 260, 14) \\ 96.78889 & ( \ 76, 15) \\ 98.24932 & ( \ 67, 11) \\ 98.82365 & ( 227, 16) \\ 99.06484 & ( 120, 9) \\ 99.06484 & ( 120, 9) \\ 99.06484 & ( 120, 9) \\ 119.29490 & ( 234, 9) \\ 113.76840 & ( 260, 10) \\ 116.76810 & ( \ 77, 18) \\ 130.26040 & ( \ 22, 13) \\ 114.40160 & ( \ 22, 13) \\ 105.03510 & ( \ 26, 10) \\ 107.34640 & ( \ 42, 10) \\ 100.63440 & ( \ 42, 10) \\ 100.63440 & ( \ 42, 10) \\ 100.63440 & ( \ 42, 10) \\ 100.63440 & ( \ 42, 10) \\ 92.63809 & ( 261, 16) \\ 86.11747 & ( 261, 16) \\ 84.18315 & ( 330, 9) \\ 97.63324 & ( 330, 9) \\ 104.95800 & ( 330, 9) \\ 104.95800 & ( 330, 9) \\ 104.95800 & ( 330, 9) \\ 101.09410 & ( 333, 9) \\ 94.02243 & ( 333, 9) \\ 94.02243 & ( 333, 9) \\ 99.47765 & ( 342, 18) \\ 89.80184 & ( \ 15, 9) \\ 87.32969 & ( 342, 18) \\ 84.96030 & ( 360, 9) \\ 86.09577 & ( 360, 9) \\ 82.52451 & ( \ 15, 9) \\ 153.29660 & ( \ 15, 9) \\ \end{array}$				HIGH 24-HR
833450.0 /         833400.0 /         833400.0 /         833350.0 /         833350.0 /         833250.0 /         833250.0 /         833200.0 /         833150.0 /         833150.0 /         833150.0 /         833150.0 /         833100.0 /         833000.0 /         832950.0 /         832950.0 /         832900.0 /         832900.0 /         832800.0 /         832750.0 /         832500.0 /         832550.0 /         832550.0 /         832550.0 /         832500.0 /         832500.0 /         832500.0 /         832500.0 /         832500.0 /         832500.0 /         832500.0 /         832500.0 /         832500.0 /         832150.0 /         832150.0 /         832150.0 /         832150.0 /         832150.0 /         832100.0 /	88.62139 ( 62, 18) 90.10687 (260, 14) 96.78889 ( 76, 15) 98.24932 ( 67, 11) 98.82365 (227, 16) 99.06484 (120, 9) 95.56972 (319, 14) 119.29490 (234, 9) 113.76840 (260, 10) 116.76810 ( 77, 18) 130.26040 ( 22, 13) 114.40160 ( 22, 13) 105.03510 ( 26, 10) 107.34640 ( 42, 10) 100.63440 ( 42, 10) 100.63440 ( 42, 10) 100.63440 ( 42, 10) 92.63809 (261, 16) 86.11747 (261, 16) 84.18315 (330, 9) 97.63324 (330, 9) 104.95800 (330, 9) 104.95800 (330, 9) 104.95800 (330, 9) 101.09410 (333, 9) 94.02243 (333, 9) 90.47765 (342, 18) 89.80184 ( 15, 9) 87.32969 (342, 18) 84.96030 (360, 9) 82.52451 ( 15, 9) 153.29660 ( 15, 9)	HUNG SHUI KIU (CHIMNEYS	; EMISSION)	***	

\* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) \* FROM ALL SOURCES \* \* FOR THE RECEPTOR GRID \*

\*

	* MAXIM	UM VALUE EQUALS	23.06605 AND OCCURRED AT (	818150.0, 832000.0)**	t محمد ا
Y-AXIS / (METERS) /	817000.0	817050.0	X-AXIS (METERS) 817100.0	817150.0	817200.0
833500.0 / 833450.0 / 833450.0 / 83350.0 / 83350.0 / 833250.0 / 833250.0 / 833250.0 / 83300.0 / 833000.0 / 832050.0 / 832900.0 / 832900.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832250.0 / 832200.0 / 83200.0 / 832000.0 / 83200.0 /	4.41776 ( 99, 1) 4.38255 ( 11, 1) 4.15445 ( 11, 1) 4.88189 ( 9, 1) 4.94230 ( 331, 1) 5.86150 ( 11, 1) 5.76264 ( 11, 1) 5.76264 ( 11, 1) 5.76264 ( 11, 1) 5.76264 ( 11, 1) 5.76269 ( 34, 1) 5.42959 ( 34, 1) 5.49002C ( 30, 1) 6.41925C ( 30, 1) 6.41925C ( 30, 1) 6.61125C ( 30, 1) 6.6771C ( 30, 1) 5.61725C ( 30, 1) 4.67805 ( 364, 1) 4.40096 ( 364, 1) 4.31058 ( 14, 1) 4.85413 ( 14, 1) 4.81655 ( 11, 1) 5.636950 ( 31, 1) 5.71026 ( 334, 1) 5.46664 ( 334, 1)	$\begin{array}{c} 4.63887 ( 99, \\ 4.40604 ( 11, \\ 4.22113 ( 11, \\ 4.88297 ( 9, \\ 5.27124 ( 331, \\ 6.23630 ( 11, \\ 6.92986 ( 11, \\ 5.64884 ( 11, \\ 5.58960 ( 364, \\ 6.18461 ( 34, \\ 5.54848 ( 336, \\ 5.85601 ( 334, \\ 6.06798 ( 334, \\ 6.06798 ( 334, \\ 6.06798 ( 334, \\ 6.06798 ( 334, \\ 6.06798 ( 334, \\ 6.06798 ( 334, \\ 6.06798 ( 334, \\ 6.03750 ( 30, \\ 7.032180 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.239930 ( 30, \\ 6.36103 ( 334, \\ 6.10387 ( 334, \\ 5.54226 ($	1) $4.61022 (99, 1)$ 1) $4.31228 (11, 1)$ 1) $4.99742 (315, 1)$ 1) $5.62235 (331, 1)$ 1) $6.64505 (11, 1)$ 1) $6.64505 (11, 1)$ 1) $7.19406 (11, 1)$ 1) $5.49736 (11, 1)$ 1) $5.49736 (11, 1)$ 1) $5.49736 (364, 1)$ 1) $5.97083 (364, 1)$ 1) $5.97083 (364, 1)$ 1) $5.87083 (364, 1)$ 1) $5.87132 (34, 1)$ 1) $5.85183 (30, 1)$ 1) $6.81972 (30, 1)$ 1) $6.81972 (30, 1)$ 1) $6.86466 (30, 1)$ 1) $5.73820 (30, 1)$ 1) $5.73820 (30, 1)$ 1) $5.0259 (14, 1)$ 1) $5.00259 (14, 1)$ 1) $5.03654 (14, 1)$ 1) $5.03854 (14, 1)$ 1) $6.13190 (11, 1)$ 1) $6.1405 (38, 1)$ 1) $6.2203 (334, 1)$ 1) $6.2845 (334, 1)$	5.09756 (99, 1) 4.91490 (99, 1) 4.49182c(126, 1) 5.40333 (315, 1) 5.97056 (331, 1) 7.09736 (11, 1) 7.45322 (11, 1) 5.97442 (364, 1) 6.25400 (364, 1) 6.31302 (336, 1) 6.45139 (334, 1) 6.73661 (334, 1) 6.73661 (334, 1) 6.51450c(30, 1) 7.30394c(30, 1) 7.30394c(30, 1) 7.30394c(30, 1) 7.34980c(30, 1) 5.1450c(30, 1) 5.13829 (14, 1) 5.57913 (14, 1) 5.57913 (14, 1) 5.57913 (14, 1) 5.31251 (14, 1) 5.15077 (239, 1) 6.47037 (11, 1) 7.23256c(38, 1) 7.14670 (334, 1) 6.61081 (334, 1) 6.01681 (14, 1)	5.39730 (318, 1) 5.24523 (99, 1) 4.79472c(126, 1) 5.85601 (315, 1) 6.31941 (11, 1) 7.60730 (11, 1) 7.70644 (11, 1) 6.40291 (364, 1) 6.40291 (364, 1) 6.44798 (336, 1) 6.44798 (336, 1) 6.46405 (334, 1) 6.86405 (334, 1) 6.86405 (334, 1) 6.86405 (334, 1) 7.06276c( 30, 1) 7.06276c( 30, 1) 7.09539c( 30, 1) 5.91553c( 30, 1) 5.91553c( 30, 1) 5.74441 (14, 1) 5.74441 (14, 1) 5.74441 (14, 1) 5.74441 (14, 1) 5.74441 (14, 1) 5.00626 (53, 1) 5.80187 (239, 1) 6.94614 (211, 1) 7.30892 (334, 1) 6.73015 (14, 1) 6.26552 (361, 1) HIGH 26.449
×	***	HUNG SHUI KIU (CHI)	INEYS' EMISSION)	***	24-HR SGROU
	* 110		GE CONCENTRATION (MICROGRAMS * FROM ALL SOURCES * FOR THE RECEPTOR GRID *	S/CUBIC METER) *	
	* MAXIMU	JM VALUE EQUALS	23.06605 AND OCCURRED AT (	818150.0, 832000.0) *	
Y-AXIS / (METERS) /	817250.0	817300.0	X-AXIS (METERS) 817350.0	817400.0	817450.0
833500.0 / 833450.0 / 833400.0 / 833350.0 / 833250.0 / 833250.0 / 833250.0 / 833250.0 / 833150.0 / 83300.0 / 832950.0 / 832950.0 / 832950.0 / 832850.0 / 832750.0 / 832750.0 / 832650.0 / 832550.0 / 83250.0 / 83250.	5.80987 (318, 1) 5.60610 (99, 1) 5.14717C(126, 1) 6.33780 (315, 1) 6.75276 (11, 1) 7.95914 (11, 1) 7.95914 (11, 1) 7.28013 (364, 1) 6.97605 (334, 1) 6.97605 (334, 1) 7.29731 (334, 1) 6.74077 (334, 1) 6.74077 (334, 1) 6.67697C(30, 1) 7.57061C(30, 1) 7.57061C(30, 1) 5.34029 (364, 1) 5.34029 (364, 1) 5.93633 (14, 1) 5.90718 (14, 1) 5.41187 (14, 1) 5.60949 (239, 1) 7.59932 (211, 1)	6.09211 ( 14, 6.40589 ( 14, 6.22517 ( 14,	1) $6.44459 (99, 1)$ 1) $6.03810C(126, 1)$ 1) $7.29234 (315, 1)$ 1) $7.29234 (315, 1)$ 1) $7.29234 (315, 1)$ 1) $7.29234 (315, 1)$ 1) $9.60598 (11, 1)$ 1) $8.53889 (11, 1)$ 1) $8.04998 (364, 1)$ 1) $7.45180 (334, 1)$ 1) $7.45180 (334, 1)$ 1) $7.45180 (334, 1)$ 1) $7.45180 (334, 1)$ 1) $7.53191C(30, 1)$ 1) $7.53191C(30, 1)$ 1) $6.02669C(30, 1)$ 1) $6.02669C(30, 1)$ 1) $6.02669C(30, 1)$ 1) $6.05894 (14, 1)$ 1) $6.05894 (14, 1)$ 1) $6.05894 (14, 1)$ 1) $4.99411 (14, 1)$ 1) $4.97424 (14, 1)$ 1) $4.98342 (11, 1)$ 1) $5.29307 (202, 1)$	6.93494 (318, 1) 6.91116 (291, 1) 6.59244c(126, 1) 7.77951 (315, 1) 8.29873 ( 11, 1) 10.46274 ( 11, 1) 8.87986C( 38, 1) 8.10034c( 38, 1) 8.02155 (151, 1) 8.09284 (335, 1) 7.57246 (335, 1) 7.57246 (335, 1) 7.00519C( 30, 1) 8.00885c( 30, 1) 7.63416c( 30, 1) 6.61474c( 30, 1) 6.63416c( 30, 1) 6.84644 ( 14, 1) 6.88532 ( 14, 1) 5.82939 ( 14, 1) 5.34999 ( 14, 1) 5.34999 ( 14, 1) 4.64368 ( 56, 1) 4.77865c(317, 1) 5.04327 (279, 1)	7.10796 (318, 1) $6.41029$ (99, 1) $6.63790c(126, 1)$ $7.74269c(126, 1)$ $7.74269c(126, 1)$ $7.61765$ (11, 1) $9.07243$ (11, 1) $9.07243$ (11, 1) $8.45877c(38, 1)$ $7.31091c(38, 1)$ $7.31091c(38, 1)$ $7.35856$ (335, 1) $6.27176$ (335, 1) $6.27176$ (335, 1) $6.26836c(30, 1)$ $7.13105c(30, 1)$ $6.50552$ (15, 1) $5.98803c(30, 1)$ $6.264670$ (14, 1) $6.26488$ (14, 1) $5.30257$ (14, 1) $5.02996$ (14, 1) $4.75830$ (56, 1) $4.43980$ (56, 1) $4.43980$ (56, 1) $4.26523$ (279, 1) $4.97853$ (279, 1)

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#### \*\*\* HUNG SHUI KIU (CHIMNEYS' EMISSION)

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# \* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) \* FROM ALL SOURCES \* \* FOR THE RECEPTOR GRID \*

#### \* MAXIMUM VALUE EQUALS 23.06605 AND OCCURRED AT ( 818150.0, 832000.0) \*

-		* MAXIMUM	VALUE EQUALS	23.06605 AND OCCURRED AT (	( 818150.0, 832000.0)	*
[ ] [ ]	Y-AXIS / (METERS) /	817500.0	817550.0	X-AXIS (METERS) 817600.0	817650.0	. 817700.0
	833500.0 / 833450.0 / 833400.0 / 833350.0 / 833300.0 / 833250.0 /	7.05689 (318, 1) 6.69957 ( 99, 1) 7.28462C(126, 1) 8.74563C(126, 1) 8.17029 ( 11, 1) 9.59053 ( 11, 1)	6.92304 ( 65, 7.17622 (206, 8.05295c(126, 9.96983c(126, 8.87199 ( 11, 9.79161 ( 11,	1)         7.84783 (206, 1)           1)         8.98347c(126, 1)           1)         11.37551c(126, 1)           1)         9.64721 (11, 1)	8.85686 (276, 1) 8.29281 (206, 1) 10.09534C(126, 1) 12.72944C(126, 1) 10.11757 ( 11, 1) 10.52153C( 38, 1)	9.94315 (276, 1) 8.79277 (276, 1) 11.25009c(126, 1) 13.48635c(126, 1) 9.88338 ( 11, 1)
	833200.0 / 833150.0 / 833100.0 / 833050.0 / 833000.0 / 832950.0 /	8.84494C(38,1) 7.90337 (151,1) 7.96692 (151,1) 7.30085 (335,1) 6.27801 (34,1) 7.30956C(30,1)	9.11614c( 38, 8.84574 (151, 7.97787c( 48, 6.93289 (335, 7.11052 (364, 8.04240 ( 15,	1)       9.18207C(38, 1)         1)       9.50677 (151, 1)         1)       8.16032C(48, 1)         1)       6.83581 (364, 1)         1)       8.05207C(30, 1)	8.81311C(38, 1) 9.67661 (151, 1) 8.14874C(48, 1) 7.58305C(30, 1) 8.84787 (15, 1) 7.51709C(30, 1)	10.67887C( 38, 1) 10.12655 (151, 1) 9.75025C( 48, 1) 7.41669C( 48, 1) 8.94910C( 30, 1) 8.50262 ( 15, 1) 7.90261C( 30, 1)
	832900.0 / 832850.0 / 832800.0 / 832750.0 / 832700.0 / 832650.0 / 832600.0 /	7.41829 (15, 1) 6.35606C(30, 1) 6.44315 (361, 1) 6.77896 (14, 1) 6.62164 (14, 1) 6.12875 (14, 1) 5.71706 (14, 1)	7.28983 ( 15, 6.70401c( 30, 6.95327 ( 14, 7.04538 ( 14, 6.61902 ( 14, 6.21263 ( 14, 5.27202 ( 14, 1, 6.21263 ( 14, 5.27202 ( 14, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	1)       7.32439 (361, 1)         1)       7.49549 (14, 1)         1)       7.18556 (14, 1)         1)       6.79539 (14, 1)         1)       6.53700 (56, 1)	7.60447 (361, 1) 7.94925 (14, 1) 7.81599 (14, 1) 7.43720 (14, 1) 7.25783 (56, 1) 7.01757 (56, 1)	8.35109 ( 14, 1) 8.48295 ( 14, 1) 8.11576 ( 14, 1) 8.08541 (104, 1) 7.40127 ( 56, 1) 6.32774 ( 56, 1)
	832550.0 / 832500.0 / 832450.0 / 832400.0 / 832350.0 / 832350.0 /	5.44995 (14, 1) 5.39505 (56, 1) 5.17582 (56, 1) 4.74091 (56, 1) 4.30900 (211, 1) 4.72249 (279, 1)	5.93209 ( 14, 5.95562 ( 56, 5.57662 ( 56, 5.00536 ( 56, 4.90565 (311, 4.43555 (211, 5.19682 (279,	1)         5.92551 (56, 1)           1)         5.57048 (311, 1)           1)         5.91904 (311, 1)           1)         5.20698 (311, 1)           1)         4.55168 (318, 1)	6.18974 ( 56, 1) 5.34049 ( 56, 1) 6.22932 (311, 1) 5.43446 (311, 1) 4.74599C(171, 1) 4.86363 (318, 1) 6.01921 (279, 1)	5.40115 ( 56, 1) 4.86541 ( 56, 1) 4.94339 (311, 1) 4.74724 (341, 1) 5.22639C(171, 1) 5.14367 (318, 1) 6.25138 (279, 1)
	832250.0 / 832200.0 / 832150.0 / 832100.0 / 832050.0 / 832000.0 /	5.35000 (279, 1) 4.90103 ( 34, 1) 5.51821 ( 34, 1) 5.26787 ( 34, 1)	5.66878 (279, 5.48011 ( 34, 5.68592 ( 34, 5.64371 ( 34, 6.00206C( 30, 7.80474C( 30,	1)         5.88935 (279, 1)           1)         5.90596 (34, 1)           1)         5.73812 (334, 1)           1)         5.628510(30, 1)           1)         6.620240(30, 1)	5.97250 (279, 1) 5.90328 (151, 1) 5.88146C( 48, 1) 6.60370C( 30, 1)	5.89662 (279, 1) 6.14715 (151, 1) 5.97590C( 48, 1) 7.14561C( 30, 1) 8.64004 ( 19, 1) 11.03826 ( 19, 1)
13						
		*** HU	NG SHUI KIU (CHIM)	NEYS' EMISSION)	***	HIGH 24-HR SGROUP
			ST 24-HOUR AVERAGE	NEYS' EMISSION) E CONCENTRATION (MICROGRAM * FROM ALL SOURCES * FOR THE RECEPTOR GRID *	*** IS/CUBIC METER) *	24-HR
		* HIGHE	ST 24-HOUR AVERAGE * f	E CONCENTRATION (MICROGRAM * FROM ALL SOURCES *		24-hr Sgroup
	Y-AXIS / (METERS) /	* HIGHE	ST 24-HOUR AVERAGE * f	E CONCENTRATION (MICROGRAM * FROM ALL SOURCES * FOR THE RECEPTOR GRID *		24-hr Sgroup
		* HIGHE * MAXIMUM	ST 24-HOUR AVERAGE * f VALUE EQUALS 2	E CONCENTRATION (MICROGRAM * FROM ALL SOURCES * FOR THE RECEPTOR GRID * 23.06605 AND OCCURRED AT ( X-AXIS (METERS) 817850.0 1) 13.35735 (205, 1) 1) 10.97739 (276, 1) 1) 10.79116C(171, 1) 1) 10.43799C(171, 1) 1) 10.43799C(171, 1) 1) 10.43799C(171, 1) 1) 10.51414 (279, 1) 1) 10.94072 (151, 1) 1) 10.94072 (151, 1) 1) 9.65167 (148, 1) 1) 9.21936 (19, 1) 1) 10.39592 (14, 1) 1) 10.73556 (14, 1) 1) 11.32838 (104, 1)	818150.0, 832000.0)	24-HR Sgroup

832350.0 / 832250.0 / 832200.0 / 832150.0 / 832100.0 / 832050.0 / 832000.0 /	14.52252 ( 14, 1) *** HU	21.61723 ( 14, 1) NG SHUI KIU (CHIMNEYS ST 24-HOUR AVERAGE CO * F	7.08428 ( 19, 1) 6.95944 ( 19, 1) 7.25005 (151, 1) 8.06091 (148, 1) 9.54303 ( 19, 1) 8.92442 ( 14, 1) 9.38135 (256, 1) 21.03756 (104, 1) * EMISSION) NCENTRATION (MICROGRAMS ROM ALL SOURCES * THE RECEPTOR GRID.*	17.57234 ( 56, 1) ***	7.07008 ( 19, 1) 7.06595 ( 19, 1) 8.14274 (148, 1) 8.65064 (256, 1) 8.46936 (104, 1) 8.81231 (104, 1) 9.66370 ( 19, 1) 16.72763 ( 19, 1) HIGH 24-HR SGROUP
	* MAXIMUM	VALUE EQUALS 23.0	6605 AND OCCURRED AT (	818150.0, 832000.0) *	C
Y-AXIS / (METERS) /	818000.0	818050.0	X-AXIS (METERS) 818100.0	818150.0	818200.0
833500.0 / 833450.0 / 833400.0 / 833350.0 / 833350.0 / 833250.0 / 833250.0 / 833150.0 / 833150.0 / 833050.0 / 832950.0 / 832950.0 / 832950.0 / 832950.0 / 832650.0 / 832650.0 / 832650.0 / 832550.0 / 832550.0 / 832550.0 / 832250.0 / 832150.0 / 832150.0 / 832050.0 / 832050.0 /	18.58838C(198, 1) 14.61192 (205, 1) 12.89066 (289, 1) 10.59438C(171, 1) 12.52128C(258, 1) 11.70921 (206, 1) 13.43812 (148, 1) 10.35228 (148, 1) 13.48440 (256, 1) 13.6625 (104, 1) 11.55280 (103, 1) 10.69926C(271, 1) 9.73513 (19, 1) 10.69926C(271, 1) 9.73513 (19, 1) 10.87934 (19, 1) 11.01719 (19, 1) 10.51140 (19, 1) 9.75994 (19, 1) 8.99197 (19, 1) 8.29353 (19, 1) 7.69522 (19, 1) 7.69522 (19, 1) 7.03256 (19, 1) 6.92633 (19, 1) 6.39730 (19, 1) 8.15903 (104, 1) 9.73144 (19, 1) 9.39319 (19, 1) 11.28747 (61, 1)	10.07764C(258, 1) 11.95143C(258, 1) 11.85282C(126, 1) 12.62117 (148, 1) 13.62625 (103, 1) 12.00919C(271, 1) 12.44396C(271, 1) 12.44396C(271, 1) 10.84692C(271, 1) 11.30459 ( 19, 1) 11.65299 ( 19, 1) 11.18220 ( 19, 1) 10.45734 ( 19, 1) 9.71150 ( 19, 1) 8.99959 ( 19, 1) 8.32571 ( 19, 1) 7.16555 ( 19, 1) 6.83633 ( 19, 1) 6.70770 ( 19, 1) 6.13750 ( 19, 1) 6.37950 ( 19, 1)	18.90081 (227, 1) 12.18315C(198, 1) 9.34551 (289, 1) 7.63587C(258, 1) 9.41084 (214, 1) 11.02917 (148, 1) 10.03370 (256, 1) 11.76730 (104, 1) 11.98821C(271, 1) 11.3349C( 22, 1) 12.27355C( 22, 1) 12.14110C( 22, 1) 11.71633 (19, 1) 11.29220 (19, 1) 10.64068 (19, 1) 9.87542 (19, 1) 9.07154 (19, 1) 7.52865 (19, 1) 6.86037 (19, 1) 6.86037 (19, 1) 6.35466 (61, 1) 6.35466 (61, 1) 6.35466 (61, 1) 6.35466 (61, 1) 6.35466 (61, 1) 6.83905 (61, 1) 7.28397 (61, 1) 7.88267 (61, 1) 8.19553 (81, 1) 8.45990 (81, 1) 19.05862 (347, 1)	13.72793 (173, 1) 8.71568c(198, 1) 5.05459 (251, 1) 5.52049 (251, 1) 5.89455 (251, 1) 5.88359 (251, 1) 8.90287 (104, 1) 11.12134 (104, 1) 11.90042 (104, 1) 11.28114 (19, 1) 12.41748 (19, 1) 12.41748 (19, 1) 12.43833 (19, 1) 11.60022 (19, 1) 9.71065 (81, 1) 9.71065 (81, 1) 9.71065 (81, 1) 9.41405 (81, 1) 8.06510 (81, 1) 7.69306 (81, 1) 7.69306 (81, 1) 7.69306 (81, 1) 7.69306 (81, 1) 5.84847 (61, 1) 5.84847 (61, 1) 5.81085 (81, 1) 6.07152 (354, 1) 6.89278c(271, 1) 7.30348c(271, 1) 7.54403c(271, 1) 23.06605 (61, 1)	5.18796 (213, 1) 4.70338 (213, 1) 5.71634 (251, 1) 9.33503 (303, 1) 10.90776c(271, 1) 12.26350 ( 81, 1) 12.77739 ( 81, 1) 12.55995 ( 81, 1) 11.09811 ( 81, 1) 10.20798 ( 81, 1) 9.33232 ( 81, 1) 8.72636 (354, 1) 8.72636 (354, 1) 7.67801 (354, 1) 7.67801 (354, 1) 6.71446 (354, 1) 5.90875 (354, 1) 5.90875 (354, 1) 5.88173 (354, 1) 5.88173 (354, 1) 6.46703 (354, 1) 6.46703 (354, 1) 6.89432 (354, 1) 7.07039 (354, 1) 18.19525c( 21, 1) HIGH
·	*** HUI	NG SHUI KIU (CHIMNEYS	' EMISSION)	***	24-HR SGROU
	* HIGHE:	* F	NCENTRATION (MICROGRAMS ROM ALL SOURCES * THE RECEPTOR GRID *	CUBIC METER) *	
	* MAXIMUM '	VALUE EQUALS 23.0	6605 AND OCCURRED AT (	818150.0, 832000.0) *	
Y-AXIS / (METERS) /	818250.0	818300.0	X-AXIS (METERS) 818350.0	818400.0	818450.0
833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 833150.0 / 833150.0 / 833050.0 / 833000.0 / 832950.0 / 832950.0 / 832850.0 /	10.37073 (166, 1) 4.53955C(92, 1) 4.48928 (131, 1) 4.20732 (131, 1) 4.59399 (213, 1) 5.71380 (213, 1) 9.25738 (251, 1) 11.31299 (299, 1) 11.99233 (299, 1) 11.54503 (299, 1) 10.92814C(21, 1) 10.74692C(21, 1) 10.32156C(21, 1) 9.82988 (354, 1)	9.02757C(219, 1) 5.73035C(170, 1) 4.66065C(92, 1) 4.35207 (131, 1) 4.11494 (131, 1) 6.37729 (131, 1) 10.09646 (213, 1) 11.75136 (213, 1) 11.34484 (251, 1) 10.66645 (251, 1) 12.2682C(21, 1) 12.96311C(21, 1) 12.92957C(21, 1) 12.43598C(21, 1)	9.74324 (340, 1)	16.27357C(170, 1) 16.60667 (182, 1) 15.62292 (182, 1) 6.93177 (131, 1) 9.84481C(234, 1) 11.82934 (149, 1) 9.33361C( 92, 1) 9.11138 (131, 1) 8.91692 (131, 1) 9.31223 ( 42, 1) 9.60451 (213, 1) 8.12249 (213, 1) 7.04451 (213, 1)	16.72665 (134, 1) 18.91303 (182, 1) 10.52029 (182, 1) 7.05588 (149, 1) 9.76744c(234, 1) 10.75224 (149, 1) 11.42168 (149, 1) 9.87202 (72, 1) 7.97443 (77, 1) 8.70165 (42, 1) 8.91245 (42, 1) 8.20189 (42, 1) 7.49189 (213, 1)

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	332800.0 /       9.35376 (354, 1)       11.71495C(21)         332750.0 /       8.81174 (354, 1)       10.91098C(21)         332700.0 /       8.24960 (354, 1)       10.10338C(21)         332650.0 /       7.69529 (354, 1)       9.33126C(21)	21, 1)       10.45262 (340, 1)       8.20829 (340, 1)       6.72195c( 97, 1)         21, 1)       10.14042 (340, 1)       8.50038 (340, 1)       6.21802c( 97, 1)	
	332600.0         /         7.16626 (354, 1)         8.61149c(21)           332550.0         /         6.67214 (354, 1)         7.94937c(21)           3325500.0         /         6.21594 (354, 1)         7.34708c(21)           332450.0         /         5.81695 (354, 1)         6.80015c(21)	21, 1)       9.04398 (340, 1)       8.73657 (340, 1)       6.75287C(310, 1)         21, 1)       8.49331C(21, 1)       8.82545 (340, 1)       6.93724 (340, 1)         21, 1)       7.99471C(21, 1)       8.80765 (340, 1)       7.05395 (340, 1)	
ع لا ا ع 1 آ	332400.0 / 5.54522 (354, 1) 6.29905c(21) 332350.0 / 6.30973 (77, 1) 5.84373c(21) 332300.0 / 5.55984 (354, 1) 5.75914 (354)	21, 1)       7.03392c(21, 1)       8.26964 (340, 1)       7.09855 (340, 1)         21, 1)       6.59041c(21, 1)       7.86177 (340, 1)       7.01109 (340, 1)         54, 1)       6.18152c(21, 1)       7.36242 (340, 1)       6.89216 (340, 1)	
	332250.0 /       5.69565C(22, 1)       5.54403 (354)         332200.0 /       5.49263 (354, 1)       5.34182C(21)         332150.0 /       5.54215 (354, 1)       5.15043C(21)         332100.0 /       5.82792 (354, 1)       5.04573C(271)	21, 1)       6.25549C(353, 1)       6.34961 (340, 1)       6.60377 (340, 1)         21, 1)       5.73294C(21, 1)       6.80543C(353, 1)       6.42810 (340, 1)         21, 1)       5.71208C(21, 1)       6.22067C(353, 1)       6.59320C(353, 1)	
	332050.0 / 6.21846 (354, 1) 5.01482C(271, 332000.0 / 17.51323 (354, 1) 11.17515C( 20,	20, 1) 9.90019C( 20, 1) 9.98884 (340, 1) 11.82234 (340, 1) HI(	GH - HR
	*** HUNG SHUI KIU (CH		ROUP
- 101-10 <b>10</b>		RAGE CONCENTRATION (MICROGRAMS/CUBIC METER) * * FROM ALL SOURCES * * FOR THE RECEPTOR GRID *	
	* MAXIMUM VALUE EQUALS	23.06605 AND OCCURRED AT ( 818150.0, 832000.0) *	
	(-AXIS / METERS) / 818500.0	X-AXIS (METERS)	
	333500.0 /       17.29711 (182, 1)         333450.0 /       14.36626 (182, 1)         333400.0 /       9.69313 (77, 1)         333350.0 /       8.10520c(107, 1)         333300.0 /       9.21945 (230, 1)         333350.0 /       9.30442c(135, 1)         333200.0 /       10.89271 (149, 1)         33350.0 /       11.10738 (50, 1)         333150.0 /       11.10738 (50, 1)         33300.0 /       10.17514 (72, 1)         33300.0 /       10.17514 (72, 1)         33300.0 /       10.17514 (72, 1)         33300.0 /       10.17514 (72, 1)         33300.0 /       10.17514 (72, 1)         33300.0 /       10.17514 (72, 1)         33300.0 /       6.54136c(20, 1)         332950.0 /       8.01698c(360, 1)         832850.0 /       6.5534c(20, 1)         3322850.0 /       6.69113c(97, 1)         332250.0 /       6.86730c(97, 1)         332250.0 /       6.86730c(97, 1)         332250.0 /       6.22166 (182, 1)         832250.0 /       6.38001 (340, 1)         832250.0 /       5.6846c(310, 1)         832250.0 /       5.66816c(310, 1)         832200.0 /       5.66846c(310, 1)         832200.0 / <td< td=""><td>Ζ</td><td>ID HI</td></td<>	Ζ	ID HI
	*** HUNG SHUI KIU (CH	24 SG	- HR SROUP
		AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) * * FROM ALL SOURCES * * FOR THE RECEPTOR GRID *	
	* MAXIMUM VALUE EQUALS	19.82199 AND OCCURRED AT ( 817950.0, 833500.0) *	2
	Y-AXIS / METERS) / 817000.0 817050.	X-AXIS (METERS) D.0 817100.0 817150.0 817200.0	<b>.</b>
	833500.0 /       4.23854 (11, 1)       4.37128 (11         83350.0 /       4.26815C(275, 1)       4.39193C(275         833400.0 /       4.09115C(275, 1)       4.17232C(275         833350.0 /       4.36564 (331, 1)       4.64405 (315         833300.0 /       4.82973 (11, 1)       5.16208 (11	75, 1)       4.52751C(275, 1)       4.75796 (65, 1)       5.09644 (65, 1)         75, 1)       4.27934C(275, 1)       4.43212 (11, 1)       4.58385 (11, 1)         15, 1)       4.93600 (331, 1)       5.22831 (331, 1)       5.51733 (331, 1)	

832350.0 / 832250.0 / 832250.0 / 832150.0 / 832100.0 / 832050.0 / 832000.0 /	* SECOND HI	* FR * FOR T	CONCENTRATION (MICROGR ROM ALL SOURCES * THE RECEPTOR GRID *	4.16171 (331, 1) 4.99435 (99, 1) 6.22136 (211, 1) 6.50772 (364, 1) 6.41943 (34, 1) 6.15820 (34, 1) 6.00648 (44, 1) 5.66110 (70, 1) *** AMS/CUBIC METER) * 817950.0, 833500.0) *	4.61908 ( 14, 1) 5.17795 ( 99, 1) 6.79513 (318, 1) 6.5140 (257, 1) 7.04999 ( 34, 1) 6.56962 (334, 1) 6.31477 ( 70, 1) 6.03900 ( 56, 1) 2ND 24-H SGRO
Y-AXIS / (METERS) /	817250.0	817300.0	X-AXIS (METERS) 817350.0	817400.0	817450.0
833500.0 / 833450.0 / 833400.0 / 833350.0 / 833300.0 / 833250.0 / 833200.0 / 833150.0 / 833150.0 / 833100.0 /	5.53583 ( 99, 1) 5.40133 ( 65, 1) 4.78499C(275, 1) 5.82419 (331, 1) 6.56535 (331, 1) 5.78026C(317, 1) 6.29890C( 38, 1) 6.71587C( 38, 1) 6.39224 (364, 1) 6.39224 (364, 1) 6.43850 (335, 1) 6.45839 (335, 1) 5.46140 (335, 1)	5.74224 ( 99, 1) 5.78571 (291, 1) 5.05241c(275, 1) 6.17575 (331, 1) 6.83182 (331, 1) 5.69522c(317, 1) 7.08824c( 38, 1) 7.28933c( 38, 1) 6.74019 (334, 1) 6.82765 (151, 1) 7.19391 (335, 1) 6.41667 (334, 1) 5.39657 (335, 1) 5.76142 (364, 1)	5.89849 (99, 1) 6.34840 (291, 1) 5.38640C(275, 1) 6.77106C(126, 1) 7.10741 (331, 1) 6.31986 (315, 1) 7.98986C(38, 1) 7.76535C(38, 1) 7.23372 (151, 1) 7.32083 (334, 1) 6.31957 (335, 1) 5.90706 (364, 1) 6.52241 (364, 1) 6.57943 (15, 1)	6.10379 ( 65, 1) 6.89179 ( 99, 1) 5.79912c(275, 1) 7.53323c(126, 1) 7.59520 ( 315, 1) 7.17945c( 38, 1) 8.87264 ( 11, 1) 7.95185 ( 364, 1) 7.84817 ( 334, 1) 7.79856 ( 334, 1) 7.15853 ( 334, 1) 6.24214 ( 34, 1) 6.88963 ( 364, 1) 7.16613 ( 15, 1) 6.49685 ( 364, 1)	6.50106 ( 65, 1) 6.29528 (291, 1) 5.68352C(275, 1) 6.95076 (315, 1) 6.99902 (315, 1) 7.41168C( 38, 1) 7.31936 (364, 1) 6.86828 (151, 1) 6.92809 (334, 1) 7.04686C( 48, 1) 6.01458 (334, 1) 6.26182 (364, 1) 6.39873C( 30, 1) 5.63144 (361, 1)

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# \* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) \* FROM ALL SOURCES \* \* FOR THE RECEPTOR GRID \*

 $\star$  MAXIMUM VALUE EQUALS ~ 19.82199 and occurred at ( ~ 817950.0, ~ 833500.0)  $\star$ 

L						
<u>.</u>	Y-AXIS / (METERS) /	817500.0	817550.0	X-AXIS (METERS) 817600.0	817650.0	817700.0
	833500.0 / 833450.0 / 833400.0 / 833350.0 / 833350.0 / 8333250.0 /	6.80569 ( 65, 1) 6.53113 (291, 1) 6.15914C(275, 1) 7.37052 (315, 1) 7.57039C(126, 1) 8.39073C( 38, 1)	6.89852 (276, 1) 6.92510 ( 99, 1) 6.68070C(275, 1) 7.78159 (315, 1) 8.45035C(126, 1) 9.21616C( 38, 1)	7.81805 (276, 1) 7.03834 ( 99, 1) 7.22478c(275, 1) 7.95719c(196, 1) 9.12196c(126, 1) 9.26114 ( 11, 1)	8.59447C(212, 1) 7.78532 (276, 1) 7.83690 (276, 1) 9.00513C(196, 1) 9.22475C(126, 1) 9.34098 (279, 1)	8.90507 (206, 1) 8.42415 (206, 1) 8.60516 (276, 1) 9.91960c(196, 1) 9.52601c(196, 1) 9.52593 (279, 1)
	833200.0 / 833150.0 / 833100.0 / 833050.0 / 833000.0 /	7.36181 (279, 1) 7.32419C( 38, 1) 7.49386C( 48, 1) 7.02544C( 48, 1) 6.19383 (364, 1)	7.72725 (279, 1) 7.24814C( 48, 1) 7.92076 (335, 1) 6.78762 (334, 1) 6.92770C( 30, 1)	7.45907 (279, 1) 8.10438C( 48, 1) 7.91079 (335, 1) 6.68849 ( 34, 1) 7.91823 ( 15, 1)	8.76996 (151, 1) 8.90885C( 48, 1) 7.80198 (334, 1) 7.25525 (364, 1) 8.45938C( 30, 1)	9.08052 ( 49, 1) 9.21606 (151, 1) 7.18035 ( 34, 1) 8.79483 ( 15, 1)
	832950.0 / 832900.0 / 832850.0 / 832800.0 /	7.01192 ( 15, 1) 7.03295C( 30, 1) 6.00564 ( 15, 1) 6.37135C( 30, 1)	7.70084C( 30, 1) 6.84958C( 30, 1) 6.50096 (361, 1) 6.90534 (361, 1)	7.58732C(30, 1) 6.34553 (361, 1) 7.02170 (14, 1) 6.73335 (361, 1)	7.29296 ( 15, 1) 7.43195C( 30, 1) 7.24381 (361, 1) 6.08823 (361, 1)	8.23356C( 30, 1) 7.58265 (361, 1) 7.68093 (361, 1) 6.63932 (355, 1) 7.40352 (104, 1)
	832750.0 / 832700.0 / 832650.0 / 832600.0 / 832550.0 /	6.44385 (361, 1) 5.71746 (361, 1) 5.05950 (361, 1) 4.92062 (104, 1) 5.37406 (104, 1)	6.21104 (361, 1) 5.41558 (361, 1) 5.39013 (104, 1) 5.88374 (104, 1) 5.72740 (104, 1)	5.76679 (361, 1) 5.95253 (104, 1) 6.50320 (104, 1) 6.21077 (104, 1) 5.33133 (104, 1)	6.61693 (104, 1) 7.23385 (104, 1) 6.77202 (104, 1) 5.64219 (104, 1) 4.78665 (43, 1)	7.91476 ( 56, 1) 7.39396 (104, 1) 5.97987 (104, 1) 5.08973 ( 43, 1) 4.73304 (341, 1)
	832500.0 / 832450.0 / 832400.0 / 832350.0 / 832350.0 /	5.31577 (104, 1) 4.79099 (104, 1) 4.03494 (104, 1) 4.30128 (_56, 1)	5.05314 (104, 1) 4.82372 (311, 1) 4.49189 ( 56, 1) 4.25614 (318, 1)	5.21010 ( 56, 1) 4.64179 ( 56, 1) 4.32073 (341, 1) 4.53349 (211, 1)	4.75578 ( 56, 1) 4.57677 (341, 1) 4.70770 (341, 1) 4.67357 ( 34, 1)	4.75409 (341, 1) 4.61392C(171, 1) 4.62148 (341, 1) 4.90197 (279, 1)
	832250.0 / 832200.0 / 832150.0 / 832100.0 /	4.18669 (318, 1) 4.84262C( 38, 1) 4.83772 (279, 1) 5.24259 (334, 1) 5.20202 (334, 1)	4.40550 (318, 1) 5.17434C( 38, 1) 5.20411 (151, 1) 5.57338 (334, 1) 5.26863 (341, 1)	4.59800 (318, 1) 5.41421C( 38, 1) 5.59228 (151, 1) 5.60726 ( 34, 1) 5.62764 ( 34, 1)	4.89689 (34, 1) 5.52618C(38, 1) 5.80614 (34, 1) 5.59960 (334, 1) 5.54067 (84, 1)	4.85113 ( 65, 1) 5.51745C( 38, 1) 6.00264C( 48, 1) 5.96077C( 30, 1) 6.77946 ( 19, 1)
	832050.0 / 832000.0 /	5.22434 (341, 1) 6.45114 ( 15, 1)	5.29326 ( 34, 1) 6.11441 ( 15, 1)	5.32408 ( 84, 1) 7.38857 ( 19, 1)	6.66700 ( 19, 1) 6.40564 ( 14, 1)	6.82142C( 30, 1) 10.19231 ( 14, 1) 2ND HI 24-HR SGROUP
		*** HU	NG SHUI KIU (CHIMNEYS	EMISSION)	***	
			* F9 * F0R	CONCENTRATION (MICROGR ROM ALL SOURCES * THE RECEPTOR GRID *		
			* F9 * F0R	ROM ALL SOURCES * THE RECEPTOR GRID * 2199 AND OCCURRED AT (		*
	Y-AXIS / (METERS) /		* F9 * F0R	ROM ALL SOURCES * THE RECEPTOR GRID *		* 817950.0
		* MAXIMUM	* Ff * FOR VALUE EQUALS 19.82 817800.0 11.35241 (276, 1) 9.60790C(212, 1) 9.76618 (276, 1)	20M ALL SOURCES * THE RECEPTOR GRID * 2199 AND OCCURRED AT ( X-AXIS (METERS) 817850.0 12.15099 (206, 1) 10.10975 (289, 1) 9.99187 (276, 1)	817950.0, 833500.0) 817900.0 13.20797 (344, 1) 11.39459 (289, 1) 10.03293 (276, 1)	817950.0 19.82199 (344, 1) 11.49663C(171, 1) 10.72632 (289, 1)
	(METERS) / 833500.0 / 833450.0 / 833400.0 / 833350.0 / 833300.0 / 833250.0 / 833200.0 / 833250.0 /	* MAXIMUM 817750.0 10.25477 (206, 1) 8.86403C(212, 1) 9.28771 (276, 1) 10.34698C(196, 1) 9.26644 ( 11, 1) 9.95465 (279, 1) 9.68796C( 48, 1) 8.91558 (334, 1)	* FF * FOR VALUE EQUALS 19.82 817800.0 11.35241 (276, 1) 9.60790C(212, 1) 9.76618 (276, 1) 10.41959C(196, 1) 9.79796C(196, 1) 10.11256C( 38, 1) 10.12376C( 48, 1) 8.44157 (266, 1)	20M ALL SOURCES * THE RECEPTOR GRID * 2199 AND OCCURRED AT ( X-AXIS (METERS) 817850.0 12.15099 (206, 1) 10.10975 (289, 1) 9.99187 (276, 1) 10.36536C(196, 1) 9.15717 (318, 1) 10.33573 (151, 1) 9.36000C( 48, 1) 9.46626 (266, 1)	817950.0, 833500.0) 817900.0 13.20797 (344, 1) 11.39459 (289, 1)	817950.0 19.82199 (344, 1) 11.49663C(171, 1)
	(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833250.0 / 833200.0 / 833100.0 / 833100.0 / 833050.0 / 833000.0 / 832950.0 /	* MAXIMUM 817750.0 10.25477 (206, 1) 8.86403C(212, 1) 9.28771 (276, 1) 10.34698C(196, 1) 9.26644 ( 11, 1) 9.95465 (279, 1) 9.68796C( 48, 1) 8.54840 (266, 1) 9.08431C( 30, 1) 7.02528 (361, 1) 7.96345 (361, 1)	* FF * FOR VALUE EQUALS 19.82 817800.0 11.35241 (276, 1) 9.60790C(212, 1) 9.76618 (276, 1) 10.41959C(196, 1) 10.41959C(196, 1) 10.11256C( 38, 1) 10.12376C( 48, 1) 8.44157 (266, 1) 9.55025 ( 84, 1) 8.23601 (148, 1) 8.35429 ( 19, 1) 8.21935 (355, 1)	ROM ALL SOURCES *           THE RECEPTOR GRID *           2199 AND OCCURRED AT (           X-AXIS (METERS)           817850.0           12.15099 (206, 1)           10.10975 (289, 1)           9.99187 (276, 1)           10.36536C(196, 1)           9.15717 (318, 1)           10.35573 (151, 1)           9.46626 (266, 1)           9.58123C(126, 1)           8.77929C(30, 1)           9.22635 (19, 1)           10.62826 (104, 1)	817950.0, 833500.0) 817900.0 13.20797 (344, 1) 11.39459 (289, 1) 10.03293 (276, 1) 9.81072 (140, 1) 9.47350C(258, 1) 10.39287 (49, 1) 9.03233 (280, 1) 10.36564 (148, 1) 9.28162 (19, 1) 9.85375 (19, 1) 11.58695 (14, 1) 11.04387 (14, 1)	817950.0 19.82199 (344, 1) 11.49663c(171, 1) 10.72632 (289, 1) 9.60959 (140, 1) 11.18060c(258, 1) 11.06328 (206, 1) 10.45609 (7, 1) 11.00645c(126, 1) 10.02485 (19, 1) 12.31389 (256, 1) 11.44457 (256, 1) 10.16151 (104, 1)
	(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833250.0 / 833200.0 / 833200.0 / 833150.0 / 833050.0 / 83300.0 / 832950.0 / 832950.0 / 832850.0 / 832850.0 / 8322750.0 / 832700.0 /	* MAXIMUM 817750.0 10.25477 (206, 1) 8.86403c(212, 1) 9.28771 (276, 1) 10.34698c(196, 1) 9.26644 ( 11, 1) 9.95465 (279, 1) 9.68796c( 48, 1) 8.91558 (334, 1) 8.91558 (334, 1) 8.54840 (266, 1) 9.08431c( 30, 1) 7.02528 (361, 1) 7.37759 (355, 1) 8.33376 (104, 1) 8.42784 ( 14, 1) 7.60224 ( 56, 1) 6.32537 ( 56, 1)	* FF * FOR VALUE EQUALS 19.82 817800.0 11.35241 (276, 1) 9.60790c(212, 1) 9.76618 (276, 1) 10.41959c(196, 1) 9.79796c(196, 1) 10.11256c( 38, 1) 10.12576c( 48, 1) 8.44157 (266, 1) 9.55025 (84, 1) 8.23601 (148, 1) 8.23601 (148, 1) 8.21935 (355, 1) 9.41840 (104, 1) 9.34125 (14, 1) 7.90103 (14, 1) 6.67613 (104, 1) 5.52365 (43, 1)	ROM ALL SOURCES *           THE RECEPTOR GRID *           2199 AND OCCURRED AT (           X-AXIS (METERS)           817850.0           12.15099 (206, 1)           10.10975 (289, 1)           9.99187 (276, 1)           10.36536C(196, 1)           9.15717 (318, 1)           10.33573 (151, 1)           9.46626 (266, 1)           9.58123C(126, 1)           8.77929C( 30, 1)           9.22635 ( 19, 1)           10.62826 (104, 1)           7.12553 (255, 1)           6.28987 ( 57, 1)           5.85019 (352, 1)	817950.0, 833500.0) 817900.0 13.20797 (344, 1) 11.39459 (289, 1) 10.03293 (276, 1) 9.81072 (140, 1) 9.473500(258, 1) 10.39287 (49, 1) 9.03233 (280, 1) 10.36564 (148, 1) 9.28162 (19, 1) 9.85375 (19, 1) 11.58695 (14, 1) 11.04387 (14, 1) 9.33404 (255, 1) 7.78551 (57, 1) 6.85581 (57, 1) 6.95137 (56, 1) 7.08504c(271, 1)	817950.0 19.82199 (344, 1) 11.49663c(171, 1) 10.72632 (289, 1) 9.60959 (140, 1) 11.18060c(258, 1) 11.06328 (206, 1) 10.45609 (7, 1) 11.00645c(126, 1) 10.02485 (19, 1) 12.31389 (256, 1) 11.44457 (256, 1) 10.16151 (104, 1) 8.39588 (57, 1) 7.77036 (56, 1) 8.19262 (56, 1) 7.58663 (73, 1)
	(METERS) / 833500.0 / 833450.0 / 833450.0 / 83350.0 / 83350.0 / 833250.0 / 833250.0 / 833200.0 / 833150.0 / 833150.0 / 833050.0 / 832950.0 / 832950.0 / 832850.0 / 832750.0 / 832750.0 / 832750.0 / 832750.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 / 832550.0 /	* MAXIMUM 817750.0 10.25477 (206, 1) 8.86403C(212, 1) 9.28771 (276, 1) 10.34698C(196, 1) 9.26644 ( 11, 1) 9.95465 (279, 1) 9.68796C( 48, 1) 8.91558 (334, 1) 8.91558 (334, 1) 8.91558 (334, 1) 7.02528 (361, 1) 7.02528 (361, 1) 7.37759 (355, 1) 8.33376 (104, 1) 8.42784 ( 14, 1) 7.60224 ( 56, 1) 6.32537 ( 56, 1) 5.35258 ( 43, 1) 5.02681 ( 56, 1) 4.84176 (341, 1) 4.65368 (341, 1)	* FF * FOR VALUE EQUALS 19.82 817800.0 11.35241 (276, 1) 9.60790C(212, 1) 9.76618 (276, 1) 10.41959C(196, 1) 9.79796C(196, 1) 10.11256C( 38, 1) 10.11256C( 38, 1) 10.12376C( 48, 1) 8.44157 (266, 1) 9.55025 (84, 1) 8.21935 (355, 1) 9.41840 (104, 1) 9.34125 (14, 1) 7.90103 (14, 1) 5.2365 (43, 1) 5.33313 (103, 1) 5.4208 (205, 1) 5.14276 (73, 1)	<pre>ROM ALL SOURCES * THE RECEPTOR GRID * 2199 AND OCCURRED AT (         X-AXIS (METERS)         817850.0         12.15099 (206, 1)         10.10975 (289, 1)         9.99187 (276, 1)         10.36536c(196, 1)         9.15717 (318, 1)         10.33573 (151, 1)         9.36000c( 48, 1)         9.46626 (266, 1)         9.58123c(126, 1)         8.77929c( 30, 1)         9.2635 ( 19, 1)         10.62826 (104, 1)         10.37159 ( 14, 1)         8.36309 ( 14, 1)         7.12553 (255, 1)         6.28987 ( 57, 1)         5.85019 (352, 1)         6.02771c(271, 1)         5.94003c(271, 1)         5.86490 ( 73, 1)</pre>	817950.0, 833500.0) 817900.0 13.20797 (344, 1) 11.39459 (289, 1) 10.03293 (276, 1) 9.81072 (140, 1) 9.47350C(258, 1) 10.39287 (49, 1) 9.03233 (280, 1) 10.36564 (148, 1) 9.28162 (19, 1) 9.28162 (19, 1) 9.85375 (19, 1) 11.58695 (14, 1) 11.58695 (14, 1) 11.64387 (14, 1) 9.33404 (255, 1) 7.78551 (57, 1) 6.8581 (57, 1) 6.95137 (56, 1) 7.02911 (56, 1) 6.62837 (73, 1) 6.86179 (362, 1) 6.57877 (362, 1)	817950.0 19.82199 (344, 1) 11.49663c(171, 1) 10.72632 (289, 1) 9.60959 (140, 1) 11.18060c(258, 1) 11.06328 (206, 1) 10.45609 (7, 1) 11.0045c(126, 1) 10.02485 (19, 1) 12.31389 (256, 1) 11.44457 (256, 1) 10.16151 (104, 1) 8.39588 (57, 1) 7.77036 (56, 1) 8.19262 (56, 1) 8.30337 (56, 1) 8.19262 (56, 1) 7.58663 (73, 1) 7.70675c( 22, 1) 7.50153c( 22, 1) 7.11615c( 22, 1)
	(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 833250.0 / 833250.0 / 833200.0 / 833200.0 / 83300.0 / 83300.0 / 83300.0 / 832950.0 / 832950.0 / 832950.0 / 832800.0 / 832750.0 / 832650.0 / 832550.0 / 832550.0 / 832550.0 / 832500.0 / 832550.0 / 832500.0 / 832550.0 / 832500.0 / 832500.0 / 832500.0 / 832500.0 / 832500.0 / 832300.0 / 832300.0 / 832300.0 / 832250.0 / 832250.0 / 832250.0 / 832250.0 /	* MAXIMUM 817750.0 10.25477 (206, 1) 8.86403C(212, 1) 9.28771 (276, 1) 10.34698C(196, 1) 9.26644 ( 11, 1) 9.95465 (279, 1) 9.68796C( 48, 1) 8.91558 (334, 1) 8.54840 (266, 1) 9.08431C( 30, 1) 7.02528 (361, 1) 7.02528 (361, 1) 7.37759 (355, 1) 8.33376 (104, 1) 8.42784 ( 14, 1) 7.60224 ( 56, 1) 6.32537 ( 56, 1) 5.35258 ( 43, 1) 5.02681 ( 56, 1) 4.84176 (341, 1) 4.65368 (341, 1) 4.85342C(171, 1) 4.95058 ( 56, 1) 5.09691 (279, 1) 5.93092 (155, 1)	<pre>* Ff * FOR VALUE EQUALS 19.82 817800.0 11.35241 (276, 1) 9.60790C(212, 1) 9.76618 (276, 1) 10.41959C(196, 1) 9.79796C(196, 1) 10.11256C( 38, 1) 10.12376C( 48, 1) 8.44157 (266, 1) 9.55025 (84, 1) 8.23601 (148, 1) 8.23601 (148, 1) 8.23601 (148, 1) 8.35429 (19, 1) 8.23601 (148, 1) 9.34125 (14, 1) 7.90103 (14, 1) 9.34125 (14, 1) 7.90103 (14, 1) 5.52365 (43, 1) 5.33313 (103, 1) 5.32337 (205, 1) 5.14276 (73, 1) 5.32520 (56, 1) 5.79329C(171, 1) 5.71744C(171, 1) 6.13966 (279, 1) 6.53041 (238, 1)</pre>	Receptor grid           Receptor grid	817950.0, 833500.0) 817900.0 13.20797 (344, 1) 11.39459 (289, 1) 10.03293 (276, 1) 9.81072 (140, 1) 9.47350C(258, 1) 10.39287 (49, 1) 9.03233 (280, 1) 10.36564 (148, 1) 9.28162 (19, 1) 9.85375 (19, 1) 11.58695 (14, 1) 9.33404 (255, 1) 7.78551 (57, 1) 6.83581 (57, 1) 6.95137 (56, 1) 7.02911 (56, 1) 6.62837 (73, 1) 6.86179 (362, 1)	817950.0 19.82199 (344, 1) 11.49663c(171, 1) 10.72632 (289, 1) 9.60959 (140, 1) 11.18060c(258, 1) 11.06328 (206, 1) 10.45609 (7, 1) 11.00445c (126, 1) 10.02485 (19, 1) 12.31389 (256, 1) 11.44457 (256, 1) 10.16151 (104, 1) 8.39588 (57, 1) 7.77036 (56, 1) 8.19262 (56, 1) 7.58663 (73, 1) 7.71233c( 22, 1) 7.50153c( 22, 1)
	(METERS) / 833500.0 / 833450.0 / 833400.0 / 83350.0 / 83350.0 / 833250.0 / 833200.0 / 833200.0 / 83300.0 / 83300.0 / 83300.0 / 832950.0 / 832950.0 / 832950.0 / 832850.0 / 832750.0 / 832650.0 / 832650.0 / 832650.0 / 832550.0 / 832550.0 / 832400.0 / 832400.0 / 832400.0 / 832350.0 / 832400.0 / 832400.0 / 832400.0 / 832350.0 / 832400.0 / 832400.0 / 832400.0 / 832400.0 / 832400.0 / 832350.0 / 832400.0 /	* MAXIMUM 817750.0 10.25477 (206, 1) 8.86403c(212, 1) 9.28771 (276, 1) 10.34698c(196, 1) 9.26644 (11, 1) 9.95465 (279, 1) 9.68796c(48, 1) 8.91558 (334, 1) 8.91558 (334, 1) 8.94840 (266, 1) 9.08431c(30, 1) 7.02528 (361, 1) 7.96345 (361, 1) 7.96345 (361, 1) 7.37759 (355, 1) 8.33376 (104, 1) 8.42784 (14, 1) 7.60224 (56, 1) 6.32537 (56, 1) 5.35258 (43, 1) 4.85342c(171, 1) 4.85342c(171, 1) 4.85342c(171, 1) 4.85342c(171, 1) 4.95058 (56, 1) 5.09691 (279, 1) 5.39126 (19, 1)	* FF * FOR VALUE EQUALS 19.82 817800.0 11.35241 (276, 1) 9.60790C(212, 1) 9.76618 (276, 1) 10.41959C(196, 1) 10.41959C(196, 1) 10.11256C(38, 1) 10.12376C(48, 1) 8.44157 (266, 1) 9.55025 (84, 1) 8.23601 (148, 1) 8.23601 (148, 1) 8.24035 (355, 1) 9.41840 (104, 1) 9.34125 (14, 1) 7.90103 (14, 1) 5.52365 (43, 1) 5.33313 (103, 1) 5.43208 (205, 1) 5.14276 (73, 1) 5.32520 (56, 1) 5.71744C(171, 1) 6.13966 (279, 1)	ROM ALL SOURCES *           THE RECEPTOR GRID *           2199 AND OCCURRED AT (           X-AXIS (METERS) 817850.0           12.15099 (206, 1)           10.10975 (289, 1)           9.99187 (276, 1)           10.36536C(196, 1)           9.15717 (318, 1)           10.35573 (151, 1)           9.36000C(48, 1)           9.46626 (266, 1)           9.58123C(126, 1)           8.77929C(30, 1)           9.26355 (19, 1)           10.62826 (104, 1)           10.37159 (14, 1)           8.36309 (14, 1)           7.12553 (255, 1)           6.28987 (57, 1)           5.86019 (352, 1)           6.02771C(271, 1)           5.86490 (73, 1)           5.86763 (362, 1)           5.86763 (362, 1)           5.85476C(171, 1)	817950.0, 833500.0) 817900.0 13.20797 (344, 1) 11.39459 (289, 1) 10.03293 (276, 1) 9.81072 (140, 1) 9.473500(258, 1) 10.39287 (49, 1) 9.03233 (280, 1) 10.36564 (148, 1) 9.28162 (19, 1) 9.85375 (19, 1) 11.58695 (14, 1) 11.58695 (14, 1) 11.04387 (14, 1) 9.33404 (255, 1) 7.78551 (57, 1) 6.85381 (57, 1) 6.95137 (56, 1) 7.02911 (56, 1) 7.02911 (56, 1) 6.62837 (73, 1) 6.86179 (362, 1) 6.43458c(22, 1) 6.43458c(22, 1) 6.09857c(171, 1) 6.14102c(126, 1)	817950.0 19.82199 (344, 1) 11.49663c(171, 1) 10.72632 (289, 1) 9.60959 (140, 1) 11.18060c(258, 1) 11.06328 (206, 1) 10.45609 (7, 1) 11.00645c(126, 1) 10.02485 (19, 1) 12.31389 (256, 1) 11.44457 (256, 1) 10.16151 (104, 1) 8.39588 (57, 1) 7.77036 (56, 1) 8.19262 (56, 1) 7.58663 (73, 1) 7.70675c( 22, 1) 7.50153c( 22, 1) 7.11615c( 22, 1) 6.61514c( 22, 1) 6.6351cc( 22, 1) 5.67322c(171, 1) 5.59959 (203, 1)

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2ND HI 24-HR SGROUP :

#### \* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) \* FROM ALL SOURCES \* \* FOR THE RECEPTOR GRID \*

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			FOR THE RECEPTOR GRID *		•
	* MAXIMUM	VALUE EQUALS	19.82199 AND OCCURRED AT (	817950.0, 833500.0) *	
Y-AXIS / (METERS) /	818000.0	818050.0	X-AXIS (METERS) 818100.0	818150.0	818200.0
833500.0 / 833450.0 / 833400.0 / 833350.0 / 833250.0 / 833250.0 / 833200.0 / 833150.0 / 833150.0 / 833050.0 / 832050.0 / 832950.0 / 832950.0 / 832850.0 / 832650.0 / 832650.0 / 832650.0 / 832650.0 / 832250.0 / 83200.0 /	18.54229 (344, 1) 12.00577 (289, 1) 11.62837 (241, 1) 9.94434 (288, 1) 12.29725 (279, 1) 11.11662 (151, 1) 13.22567C(126, 1) 9.92935C(171, 1) 12.81053 (104, 1) 12.95659 (103, 1) 10.42279 (104, 1) 9.50445 (103, 1) 9.35503 (56, 1) 9.38874 (56, 1) 9.38874 (56, 1) 9.38874 (56, 1) 9.38876 (22, 1) 9.40503C(22, 1) 9.40503C(22, 1) 8.81263C(22, 1) 8.81263C(22, 1) 8.81263C(22, 1) 5.74905C(22, 1) 5.74905C(22, 1) 5.74905C(22, 1) 5.74905C(22, 1) 5.74905C(22, 1) 5.74905C(22, 1) 5.74025 (104, 1) 5.46402 (61, 1) 5.46402 (61, 1) 8.13112 (104, 1) 8.48212 (61, 1) 8.90785 (61, 1) 11.17473 (19, 1)	18.62510 (264, 12.96268 (202, 9.64653 (209, 9.81147 (288, 10.14759 (206, 10.65334 (152, 9.50096C(171, 11.40914 (103, 12.87149 (104, 11.52534 (103, 9.45165 (56, 10.29502C(22, 11.24214C(22, 11.32815C(22, 10.84500C(22, 9.97637C(22, 8.90349C(22, 6.77583C(22, 6.77583C(22, 6.26525 (57, 5.90404 (59, 5.69274 (61, 5.56513 (61, 5.565513 (61, 5.565513 (61, 5.565513 (61, 7.94346 (81, 7.94346 (81, 7.94346 (81, 8.00155 (81, 13.82679 (347,	1) $11.20536$ (227, 1)1) $8.59919$ (205, 1)1) $7.09574$ (288, 1)1) $7.99209$ (206, 1)1) $9.36492$ (273, 1)1) $8.73133$ (280, 1)1) $8.73133$ (280, 1)1) $11.25383$ (103, 1)1) $11.25383$ (103, 1)1) $11.51190$ (104, 1)1) $10.84710$ (303, 1)1) $11.51190$ (104, 1)1) $11.67351$ (73, 1)1) $11.67351$ (73, 1)1) $11.67351$ (73, 1)1) $11.301600$ (22, 1)1) $0.933350$ (22, 1)1) $8.16365$ (59, 1)1) $7.70441$ (59, 1)1) $6.73554$ (81, 1)1) $6.69314$ (61, 1)1) $6.30035$ (81, 1)1) $6.30035$ (81, 1)1) $6.51629$ (81, 1)1) $6.51629$ (81, 1)1) $7.14144$ (81, 1)1) $7.88648$ (61, 1)1) $7.81730$ (354, 1)	8.57619C(197, 1) 4.33416 (299, 1) 5.12997 (299, 1) 5.24020 (299, 1) 4.97625 (299, 1) 7.34432 (251, 1) 9.46547 (303, 1) 10.78972 (303, 1) 10.24990 (303, 1)	15.63571C(162, 1)         3.93407 (121, 1)         3.77141C(304, 1)         3.77141C(304, 1)         3.97824 (251, 1)         4.28783 (251, 1)         3.82158 (326, 1)         6.31463 (303, 1)         8.27978 (251, 1)         10.60401 (81, 1)         11.62134C(271, 1)         11.31226C(271, 1)         10.09682 (354, 1)         10.09682 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (354, 1)         9.68267 (22, 1)         5.93447 (33, 1)         5.65268 (354, 1)         5.43517C(22, 1)         5.292920C (22, 1)         5.83866 (51, 1)         6.17084 (51, 1)         6.36297C(21, 1)         17.78988 (354, 1)         2ND H         24-HR
	*** HL	ING SHUI KIU (CHIMM	NEYS' EMISSION)	***	SGROUP
		GHEST 24-HOUR AVER	NEYS' EMISSION) RAGE CONCENTRATION (MICROGA * FROM ALL SOURCES * FOR THE RECEPTOR GRID *		SGROUP
	* SECOND HI	GHEST 24-HOUR AVER	RAGE CONCENTRATION (MICROG) * FROM ALL SOURCES *	RAMS/CUBIC METER) *	
Y-AXIS / (METERS) /	* SECOND HI	GHEST 24-HOUR AVER	RAGE CONCENTRATION (MICROG) * FROM ALL SOURCES * FOR THE RECEPTOR GRID *	RAMS/CUBIC METER) *	

1								
	832250.0 / 832200.0 / 832150.0 / 832100.0 / 832050.0 / 832000.0 /	5.58445 (354, 1)       5.22077c         5.43233c(22, 1)       5.21114         5.20911c(271, 1)       5.12914         5.25954c(271, 1)       4.75367c         5.50885 (51, 1)       4.81967         14.90451c(21, 1)       11.14612	(354, 1) (77, 1) (21, 1) (354, 1)	5.73289 (354, 1) 5.60634C( 21, 1) 5.42982C(353, 1) 5.01907C(353, 1) 4.85668C(353, 1) 7.71659 ( 60, 1)	6.33413 5.93470 5.77830 5.62726	(354, 1) C(353, 1) (340, 1) (340, 1) (340, 1) (340, 1) C(360, 1)	5.64660 (354, 5.31211 (354, 6.28330c(353, 6.27510 (340, 6.06856c(353, 11.36139c(360,	1) 1) 1) 1) 1) 2ND HI
Lj								24-HR
		*** HUNG SHUI KIU	(CHIMNEYS'	EMISSION)		***		SGROUP
		* SECOND HIGHEST 24-HOL	IR AVERAGE C		MAS/CURTC	4676D) *		
			* FRO	M ALL SOURCES * E RECEPTOR GRID *		121287		
		* MAXIMUM VALUE EQUALS	19.821	99 AND OCCURRED AT (	817950.0,	833500.0) *		
	Y-AXIS / (METERS) /	818500.0		X-AXIS (METERS)				
11.				<b></b>				
	833500.0 /	17.29388 ( 71, 1)		•				
	833450.0 /	10.99072C(145, 1)						
	833400.0 /	9.39432 (123, 1)						
	833350.0 / 833300.0 /	7.35968 (123, 1) 8.98298 (231, 1)						
	833250.0 /	8.58273 ( 50, 1)						
	833200.0 /	9.00053 ( 50, 1)						
	833150.0 /	9.11146 (149, 1)						
	833100.0 /	8.92217 ( 72, 1)						
	833050.0 /	7.50930 (260, 1)						
Ē	833000.0 /	7.59164 (72, 1)						
	832950.0 /	7.29254 (77, 1)		4				
L	832900.0 / 832850.0 /	6.32161 ( 42, 1) 6.07226 ( 42, 1)						
	832800.0 /	5.97096 (213, 1)						
	832750.0 /	5.92309 (213, 1)						
	832700.0 /	5.95568 (213, 1)				•		
	832650.0 /	6.31103 (252, 1)						
	832600.0 /	6.07991C( 97, 1)						
	832550.0 /	5.71961 (330, 1)						
	832500.0 / 832450.0 /	5.40268 ( 9, 1) 5.39354 ( 9, 1)				· .		
L	832400.0 /	4.96319C(265, 1)						
	832350.0 /	5.40805 (340, 1)						
<u>-</u> -،	832300.0 /	5.44953 (340, 1)						
1.	832250.0 /	4.751230(310, 1)						
L	832200.0 /	4.50536 (354, 1)						
	832150.0 /	4.47444C(353, 1)						
	832100.0 / 832050.0 /	5.53508C(353, 1)						
	832000.0 /	5.77572c(353, 1) 9.50877 (340, 1)						
L								
R	UN ENDED ON 04-0	01-96 AT 19:46:58						
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Li								

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# Appendix 2

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Emission Factors for the Dust Emission Impact Assessment

Environmental	Impact Assessment				
	· · · · · · · · · · · · · · · · · · ·				
Dust emission	from unpaved road with dust mit	igation measu	ires		
	industrial unpaved road (kg/v-km), E =	Ť	]	k(1.7)(s/12)(S/48)(W/2.7	10.7(w/410.5
where	k =	particle size multi	plier (dimensionless) =	0.8	
· · · · · · · · · · · · · · · · · · ·	s =		d surface materials (%) =	4.8	
	S =	mean vehicle spe	ed (km/hr) =	5	
	W =	mean vehicle wei	ght (Mg) =	8	unladen
	= W	mean vehicle wei	ght (Mg) =	24	laden
	w =	mean number of		10	
	· · · · · · · · · · · · · · · · · · ·				
Emission factor from	industrial unpaved road (kg/v-km or g/v-m))	 2		0.1916	unladen
	industrial unpaved road (kg/v-km or g/v-m))		-	0,4135	
i				1	
	· · · · · · · · · · · · · · · · · · ·				····· ··· ···
Dust emission	from loading and unloading of m	aterials			
	truck loading (kg/Mg), E =	k(0.0016)(U/2.2)1	3/ (M/2)1 4		1
Enilosion labior for	Habridaanig (Kanig) =	1(0.0010)(0.0.0)			· · · · · · · · · · · · · · · · · · ·
where	k =	particle size multi	plier (dimensionless) =	0.74	÷
		mean wind speed		1.0	
	M =	material moisture		2.0	
Emission factor for lo	ading each truck =	0.0004	kg/Mg		
Capacity of each truc		12.50			
Number of loadings i	n an hour =	6			
	spoil or construction material handled =		Mg/hr		
max. dust emission r	ate =	0.01	g/s		
Duct or include	from excavation/earthwork				<u> </u>
Emission factor for	excavation (kg/Mg), E =		k(0.0016)(U/2.2)1.3/ (M/2)1.4		
	le —		l	0.74	
where	k=	l'	plier (dimensionless) =	1.0	
·		mean wind speed	· · · · · · · · · · · · · · · · · · ·		
	M =	material moisture	content (%) =	2.0	
Emission factor for e	xcavation =	0.0004	ka/Ma		<u> </u>
			m3/hr/excavator		
max. excavation rate					
max. excavation rate max. excavation rate		1	Mg/hr		

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# Appendix 3

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Typical FDM Result Files for the Dust Emission Impact Assessment FDM - (DATED 91109)

IBM-PC VERSION (1.01) (C) COPYRIGHT 1991, TRINITY CONSULTANTS, INC. SERIAL NUMBER 9181 SOLD TO EHS CONSULTANTS LTD RUN BEGAN ON 8/08/96 AT 13:42:45

RUN TITLE: Engineering Works for Hung Shui Kiu (D1,L1)

INPUT FILE NAME: A3.DAT OUTPUT FILE NAME: A3.LST MET DATA READ FROM FILE NAME: LFS94S.BIN PLOT OUTPUT WRITTEN TO FILE NAME: A3.RAW

CONVERGENCE OPTION 1=OFF, 2=ON	1
MET OPTION SWITCH, 1=CARDS, 2=PREPROCESSED	2
PLOT FILE OUTPUT, 1=NO, 2=YES	2
MET DATA PRINT SWITCH, 1=NO, 2=YES	1
POST-PROCESSOR OUTPUT, 1=NO, 2=YES	1
DEP. VEL./GRAV. SETL. VEL., 1=DEFAULT, 2=USER	: 1
PRINT 1-HOUR AVERAGE CONCEN, 1=NO, 2=YES	3
PRINT 3-HOUR AVERAGE CONCEN, 1=NO, 2=YES	1
PRINT 8-HOUR AVERAGE CONCEN, 1=NO, 2=YES	1
PRINT 24-HOUR AVERAGE CONCEN, 1=NO, 2=YES	3
PRINT LONG-TERM AVERAGE CONCEN, 1=NO, 2=YES	3
BYPASS RAMMET CALMS RECOGNITION, 1=NO, 2=YES	2
NUMBER OF SOURCES PROCESSED	24
NUMBER OF RECEPTORS PROCESSED	3
NUMBER OF PARTICLE SIZE CLASSES	20
NUMBER OF HOURS OF MET DATA PROCESSED	8760
LENGTH IN MINUTES OF 1-HOUR OF MET DATA	60.
ROUGHNESS LENGTH IN CM	10.00
SCALING FACTOR FOR SOURCE AND RECPTORS	1.0000
PARTICLE DENSITY IN G/CM**3	2.50
ANEMOMETER HEIGHT IN M	10.00

PREPROCESSED METEOROLOGICAL DATA SELECTION SWITCHES 

GENERAL PARTICLE SIZE CLASS INFORMATION

PARTICLE SIZE CLASS	CHAR. DIA. (UM)	GRAV. SETTLING VELOCITY (M/SEC)	DEPOSITION VELOCITY (M/SEC)	FRACTION IN EACH SIZE CLASS
	4 0000000	**		
1	1.0000000	**	**	.0100
2 3	2.0000000		**	.0100
	3.0000000	**	**	.0600
4	5.0000000	**	**	.0300
5	7.0000000	**	**	.0200
6	9.0000000	**	**	.0100
7	10.0000000	**	**	.0500
8	20.0000000	**	**	-0400
9	40.0000000	**	**	.0300
10	60.0000000	**	**	.0300
11	80.0000000	**	**	.0200
12	*****	**	**	.0800
13	*****	. **	**	.1500
14	******	**	**	.0700
15	******	**	**	.1700
16	*****	**	**	.1500
17	*****	**	**	.0300
18	****	**	**	-
	*****	**	**	.0200
19	******			.0100
20	*******	**	**	.0100

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\*\* COMPUTED BY FDM

RECEPTOR COORDINATES (X,Y,Z)

839., 2.) ( 415., 839., 3.) ( 415., 839., 5.)

415.,

SOURCE INFORMATION

түре	ENTERED EMIS. RATE (G/SEC, G/SEC/M OR G/SEC/M**2)	TOTAL EMISSION RATE (G/SEC)	WIND SPEED FAC.	X1 (M)	Y1 (M)	X2 (M)	Y2 (M)	HEIGHT (M)	WIDTH (M)
. 1	.010000000	.01000	1.300	414.	822.	0.	0.	.50	.00
1	.010000000	.01000	1.300	414.	822.	0.	0.	1.50	.00
	.000027000	.00670	.000	310.	831.	313.	583.	1.00	1.00
2	.000027000	.00374	.000	313.	583.	325.	445.	1.00	1.00
2	.000027000	.00259	.000	325.	445	382.	368.	1.00	1.00
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.000027000	.00235	.000	419.	822.	414.	735.	1.00	1.00
2	.000027000	.00179	.000	414.	735.	393.	672.	1.00	1.00
2	.000027000	.00178	.000	393.	672.	403.	607.	1.00	1.00
2	.000027000	.00456	.000	403.	607.	407.	438.	1.00	1.00
2	.000027000	.00251	.000	313.	583.	403.	607.	1.00	1.00
2	.000027000	00129	.000	414.	735.	461	726.	1.00	1.00
	.000027000	00237	.000	461.	726.	545.	752.	1.00	1.00
2	.000027000	.00490	.000	310.	831.	491	820.	1.00	1.00
2	.000057000	.01414	.000	310.	831.	313.	583.	1.00	1.00
2	.000057000	.00790	.000	313.	583.	325.	445.	1.00	1.00
2	.000057000	.00546	.000	325.	445.	382.	368	1.00	1.00
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.000057000	.00497	.000	419.	822.	414.	735	1.00	1.00
2	.000057000	.00379	.000	414	735.	393.	672.	1.00	1.00
. 2	.000057000	.00375	.000	393.	672.	403.	607.	1.00	1.00
2	.000057000	.00964	.000	403.	607.	407.	438.	1.00	1.00
	.000057000	00531	.000	313.	583.	403.	607.	1.00	1.00
2 2 2	.000057000	.00273	.000	414.	735.	461.	726.	1,00	1.00
2	.000057000	.00501	.000	461.	726.	545.	752.	1.00	1.00
2	.000057000	.01034	.000	310.	831.	491.	820.	1.00	1.00
	=	===========							
TOTAL	EMISSIONS	.12760							

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TOTAL EMISSIONS .12760 NOTE: SOME SOURCE EMISSION RATES ARE A FUNCTION OF WIND SPEED AND TOTAL IS NOT CORRECT

TOP 50 TABLE FOR 1 HOUR AVERAGES

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RANK	RECEPTOR	X-COORDINATE	Y-COORD INATE	ENDING HOUR	CONCENTRATION	DEPOSITION
						· · · · · · · · · · · · · · · · · · ·
1	1	415.0	839.0	2746	554.5076	71.7764
2	1	415.0	839.0	5386	518.8418	62.7807
3	1	415.0	839.0	2744	508.2182	61.7127
4	1	415.0	839.0	3841	501,1585	55,9794
5	1	415.0	839.0	5184	488.7755	58,9588
6	1	415.0	839.0	2598	470,5970	13,9748
7	1	415.0	839.0	3944	467.0109	47.9900
8	1	415.0	839.0	5191	464.4807	43.3025
9	1	415.0	839.0	3964	460,0042	38,1378
10	1	415.0	839.0	2766	456.9429	38.0295
11	1	415.0	839.0	2736	455.4417	42.4077
12	1	415.0	839.0	5310	447,3566	45.9872
13	1	415.0	839.0	3915	447.3231	46.0389
14	1	415.0	839.0	3940	441.7697	57.3347
15	1	415.0	839.0	3943	440.3566	49,4703
16	1	415.0	839.0	3966	436.0661	31.4009
17	1	415.0	839.0	3891	432.5409	44.5745
18	1	415.0	839.0	4015	430.3077	35.4712
19	1	415.0	839.0	5313	430.2410	35.5580
20	1	415.0	839.0	4017	416.6812	38.8271
21	1	415.0	839.0	2908	416.6497	38.8722
22	1	415.0	839.0	3896	415.9586	29.9638
23	1	415.0	839.0	2768	415.8935	30.0409
24	1	415.0	839.0	2885	406.9790	25.0387
25	1	415.0	839.0	3842	397.8658	40.7421
26	1	415.0	839.0	3942	383.2048	43.1954
27	1	415.0	839.0	3938	374.6373	19.4019
28	1	415.0	839.0	5813	367.1660	5.2177
29	1	415.0	839.0	6633	351.4712	12.7454
30	1	415.0	839.0	5337	350,0260	29.0464
31	1	415.0	839.0	5453	349.3050	6.6694
32	1.	415.0	839.0	5287	341.6382	44.1609
33	1	415.0	839.0	3937	335.0357	17.3491
34	1	415.0	839.0	3579	332.2050	20.2474
35	1	415.0	839.0	3826	330.7283	37.1380
36	1	415.0	839.0	2863	328.1211	12.0083
37	1	415.0	839.0	5311	326.1099	30.5378
38	1	415.0	839.0	5192	324.2287	23.4212
39	1	415.0	839.0	2597	314.1663	16.3539
40	1	415.0	839.0	4014	312.1566	25.8111
41	1	415.0	839.0	4016	307.5317	31.7089

42 43 44 45 46 47 47 48 49 50	1 1 1 1 1 1 1 1	415.0 415.0 415.0 415.0 415.0 415.0 415.0 415.0 415.0 415.0	839.0 839.0 839.0 839.0 839.0 839.0 839.0 839.0 839.0	5193 2622 1587 3871 4948 2575 8285 2096 5456	307.1188 307.0510 304.8596 301.5207 299.4665 297.6552 293.3834 289.0085 285.0653	28.7243 28.8237 2.4930 15.5689 3.0980 13.6806 17.9143 10.3870 8.4123	•	
HIGHES		IIGHEST VALUES		· · ·				
RECEPTO					OUR DEPOSITION	SECOND HIGH E	NDING HOUR	DEPOSTION
1 2 3	415	5.0 839	9.0 554 9.0 163 9.0 31	.0121 2746.	71.7764 13.2351 1.7323	518.8418 152.5242 28.2932		62.7807 11.3298 1.2841
		HOUR AVERAGES						
	RECEPTOR X-	COORDINATE	Y-COORDINATE	ENDING HOUR	CONCENTRATION	DEPOSITION		
$\begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 20 \\ 21 \\ 223 \\ 24 \\ 25 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ 32 \\ 33 \\ 34 \\ 5 \\ 36 \\ 37 \\ 38 \\ 39 \end{array}$	1 1 1 1 1 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1	$\begin{array}{c} 415.0\\ 41$	839.0 839.0	4032C 5328C 2784C 2760C 5208C 3912C 2928C 3984C 2904C 3864C 2616C 3960C 5400C 3888C 3936C 5472C 3840C 5352C 2736C 8304C 2640C 4008C 2880C 4032C 5304C 2880C 3944C 2880C 3944C 2880C 3944C 2880C 3944C 2880C 3944C 2880C 3944C 2880C 3944C 2880C 3944C 2880C 3944C 2880C 3944C 3984C 3984C 3984C 3984C 3984C 3984C 3984C	113.3894 103.4679 102.8284 99.1501 98.5495 96.5275 91.6382 89.0692 72.9985 65.2439 63.3262 62.9419 59.4582 59.3135 55.7344 54.0923 52.6298 51.8898 50.1460 46.9121 44.0379 39.0408 38.5727 38.4296 36.6720 35.4027 35.2140 34.2939 33.9128 32.8223 32.4559 31.9615 31.9342 31.3444 31.0574 30.4515 29.6819 29.6343	10.7551 9.8840 7.4803 11.3993 9.6733 7.4224 7.7335 6.1075 4.7424 6.4813 3.4619 3.7028 5.8395 3.0520 5.7679 1.8076 5.83950 4.4443 4.7423 2.5231 3.8075 2.7285 2.0912 2.2761 3.3306 3.3398 3.4714 1.9822 1.4866 3.2656 1.5642 2.3783 1.7650 1.8505 2.3658 2.5784 1.2779 1.6657		
40 41 42 43 44 45 46 47 48 47 48 50	1 1 2 1 2 1 2 1 2 1	415.0 415.0 415.0 415.0 415.0 415.0 415.0 415.0 415.0 415.0	839.0 839.0 839.0 839.0 839.0 839.0 839.0 839.0 839.0 839.0 839.0	7704c 1008c 3120c 2904c 6648c 5832c 5352c 3600c 3864c 4608c 4248c	26.9781 26.3992 24.0260 23.8629 22.4112 20.5969 20.0930 19.8291 19.7985 19.7370 19.5496	.9647 .6937 1.2793 1.1071 .7961 .2998 1.1231 1.1653 1.1492 2.2265 1.1152		

HIGHEST AND SECOND HIGHEST VALUES FOR 24 HOUR AVERAGES

RECEPTOR	X-COORDINATE	Y-COORDINATE	HIGHEST VALUE	ENDING HOUR	DEPOSITION		ENDING HOUR	DEPOSTION
· 1	415.0	839.0	195.6076	3960.C	18.5736	113.3894	4032.C	10.7551
2	415.0	839.0	62.9419	3960.C	3.7028	38.4296	4032.C	2.2761
3	415.0	839.0	5.1629	3960.C	.2187	4.8593	3264.C	.2498

#### TOP 50 TABLE FOR LONG TERM AVERAGES

RANK	RECEPTOR	X-COORD INATE	Y-COORDINATE	ENDING HOUR	CONCENTRATION	DEPOSITION
1	1	415.0	839.0	8760C	12.5883	.8833
2	2	415.0	839.0	8760C	4.7472	.2140
3	3	415.0	839.0	8760C	.9040	.0289
4	0	.0	.0	0	.0000	.0000
5	0	.0	.0	0	.0000	.0000
6	0	.0	.0	0	.0000	.0000
7	0	.0	.0	0	.0000	.0000
8	0	.0	.0	0	.0000	.0000
9	0	-0	.0	0	.0000	.0000
10	0	.0	.0	0	.0000	.0000
11	0	.0	.0	0	.0000	.0000
12	0	.0	.0	0	.0000	.0000
13	0	.0	.0	0	.0000	.0000
14	0	.0	.0	0	.0000	.0000
15	. 0	.0	.0	0	.0000	.0000
16	0	.0	.0	0	.0000	.0000
17	0	.0	.0	0	.0000	.0000
18	0	.0	.0	0	.0000	.0000
19	0	.0	.0	0	.0000	.0000
20	0	.0	.0	0	.0000	.0000
21	0	.0	.0	0	.0000	.0000
22	0	.0	.0	0	.0000	.0000
23	0	.0	.0	0	.0000	.0000
24	0	.0	.0	0	.0000	.0000
25 26	0 0	.0	.0	0	.0000	.0000
20	0	.0 .0	.0 .0	0	.0000	.0000 .0000
28	0	.0	.0	0	.0000	.0000
29	0	.0	.0	0	.0000	.0000
30	Ő	.0	.0	. 0	.0000	.0000
31	ő	.0	.0	0	.0000	.0000
32	ŭ	.0	.0	Ő	.0000	.0000
33	ŭ	.0	.0	0	.0000	.0000
34	õ	.0	.0	0	.0000	.0000
35	õ	.0	.0	ŏ	.0000	.0000
36	Ō	.0	0	ŏ	.0000	.0000
37	õ	.0	.0	ŏ	.0000	.0000
38	õ	.0	.0	õ	.0000	.0000
39	õ	.0	.0	õ	.0000	.0000
40	õ	.0	.0	õ	.0000	.0000
41	õ	.0	.0	õ	.0000	.0000
42	Ō	.0	.0	õ	.0000	.0000
43	0	.0	.0	ō	.0000	.0000
44	Ō	.0	.0	ō	.0000	.0000
45	Ō	.0	.0	õ	.0000	.0000
46	Ō	.0	.0	ō	.0000	.0000
47	Ō	.0	.0	ō	.0000	.0000
48	Ō	.0	.0	Ō	.0000	.0000
49	Ū	.0	.0	ō	.0000	.0000
50	0	.0	.0	ō	.0000	.0000

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RUN ENDED ON 8/08/96 AT 14:45:20

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# Appendix 4

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# Predicted Traffic Data on the Proposed Roads for the Vehicular Emission Impact Assessment

Road	Location	i Lie	tht Vehs/Ha	рци	<b>.</b>	N	ehs / hour
anton en el Reconstruction		Car	Taxi	LGV	PV Tel.	M/Hav.	Ger Tot
ບາ	Λ	- 108	314	164	1546	347-	397
	B	(002	412	2.93	1707	434	412
	С	1186	488	346	2020		434
D2	D	634	263	186	1088	187	189
	٦ ر	482	404	287	1673	242	242
ł.1	f	157	58	28	343	גר 42	27
i	G	313	119	57	499	38	38
	Н	- 323	155	s7	499	51	51
	1	421 457	168	74 81	650	47	47
	К	497	183	88	765	49	49
	t.	475	115	84	734	41	49
L2	м	407	150	71	628	56	56
	N	202	74	3.6	312	40	40
	0	175	65	31	ا تد	7.C 2.E	2.5
	P	145	90	44	379	17	32
	Q	122	45		189	<b> </b>	17
1,3	R	317	117	56	490	54	54
L4	S S	319	117	57	493	29	2.9
ļ	i	57	- Ji	10	9%	4	4
	U 	57	21	10	88	4	4
L5	V	24	11	5	45	20	20
L6	W	214	79	37	330	35	35
	XX	108	40	18	166	18	18
L11	Y	3,5	12	6	51	5	5
	Ζ.	111	4(	(9	171	12	12
L12	M.	212	78	38	328	'21	21
	88	203	75 17	36	314	20	20
	CC DD	45		8	70	2 20	2
L13'	f	203	75	<u>}6</u>	314		
	50	45	17	8	10	<u>د</u>	2
1.14	FF	114	41	20	.176	8	8
L15	CC	197	72	35	304	50	50
		197	72	35	304	50	50
CPR		1172	490	348	2030	2.84	284
{		1014	4(7 (150	296	1707	234	234
	KK LL	1161 (191	478	338	1977	2.4.K 2.57	268
			490	348	2027		257
ma	yor .	58.7=%	24.167.	17.11%	( M, DX, UPA		

0984/NIA WP/ala

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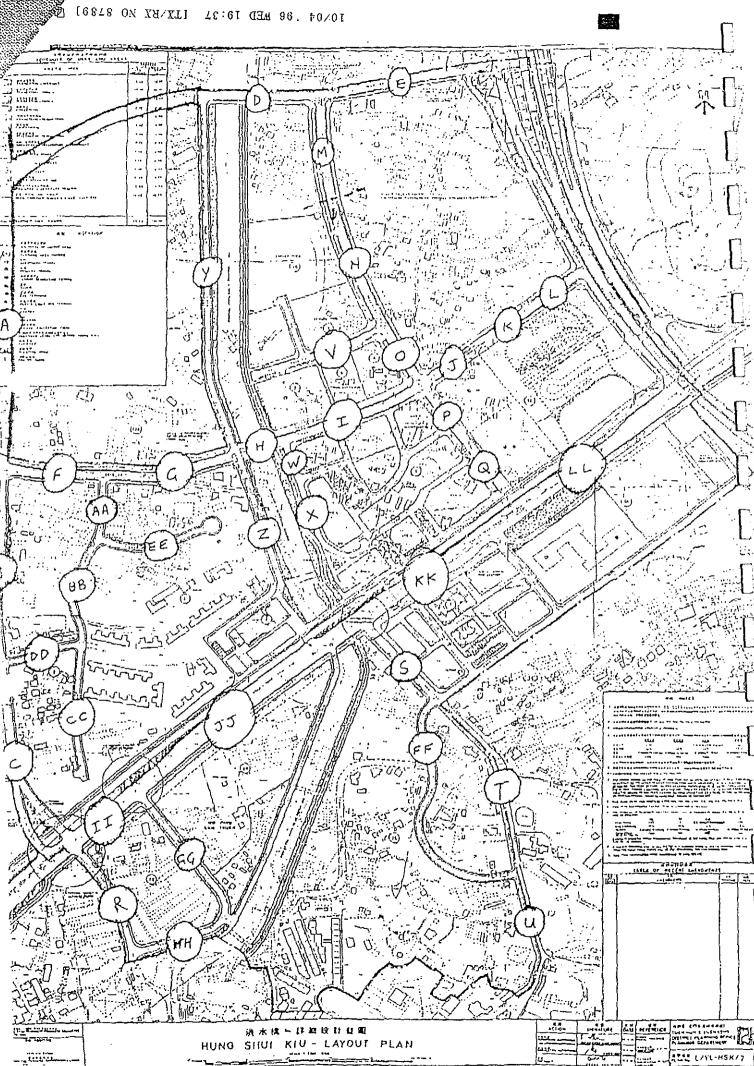
Refer to LIIAM HHJ.NET

Table 2 2011 PM

Road	Location	Lia	ht Vens/Ho	)UF		Good Ush	know</th
		Car	"[a×1"	LĠV	PY Tot	H17V 1007a	GVTO
DT	Λ	706	306	281	1293	472	47.2
	В	728	315	270	1333	478	478
	Ç	87.6	379	348	1603	515	515
D2	U	397	172	- 158	727	154	154
[	Ē.	607	263	· 242	1112	208	208
L1 -	F	35	28	15	· 73	10	10
	G	159	127	64	350	4.9	49
	Ы	155	124	62.	341	4.)	42
	ŧ	205	164	83	452	55	
ĺ	ļ	241	193	96	530	574	54
	К	267	214	107	538	5.6	56
	ť.	282	225	113	620	3:2	5.2
L2	м	185	148	73	406	56	56
	N	93	75	37	205	41	41
	U U	82	66	33	1.81	. 31	31 33
	с Ч	133	106	33 \$3	J90	33	11
	Q	66	53	27	146		[
L3	R	109	87	44	240	53	. 53
L4	S	168	135	67	370	36	36
	Ţ	3.5	28	14	7/	4	ų
	UU	35	28	14	17	Ц.	4.
<u>L5</u>	V	18	15	7	40	20	20
1.6	w	106	85	42	233	41	41
	Х	53	4.3	21	117	20	20
L11	Ŷ	17	14	7	38	7	7
	1	49	39	19	101	11	11
L12	M	135	108	54	297	38	38
	88	124	91	54 49	272	35	35
	CC	18	15	7	40	2	2
	מס	124	91	49	272		38
L13	FF	18	15	7	40	2	2
L14	FF	71	57	-28	156	10	10
L15	CG	60	48	24	۲32	50	50
	III	60	43	24	132	50	50
CPR		741	321	294	1356	352	352
	11	667	290	265	1224	303	303
•	КК	710	-334	306	1410	318	318
{	L.L.	809	350	322	1481	325	325
/11		54.63,7,			(DJ. DJ. CP)		<u></u>
4.64	·		40 66 /m	21.121		-	

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9984/HIA.WP/ele



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9.4 QQ3# 62:67 01-50-3661

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Ch. K.

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### Appendix 5

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Typical Caline4 Result Files for the Vehicular Emission Impact Assessment IBM-PC VERSION (1.90) (C) COPYRIGHT 1987, TRINITY CONSULTANTS, INC. SERIAL NUMBER 7997 SOLD TO E.H.S. CONSULTANTS LIMITED RUN BEGAN ON 08-05-97 AT 00:11:44

CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 1

JOB: Hung Shiu Kiu-traffic emission impact RUN: CO -AM (WORST CASE ANGLE) POLLUTANT: CO

#### I. SITE VARIABLES

Ŭ=	1.0	M/S	Z0=	10.	CM		ALT =	Ο.	(M)
BRG=	WORST	CASE	VD=	.0	CM/S				
CLAS =	4	(D)	 VS=	.0	CM/S				
MIXH=	500.	м	AMB=	.0	PPM				
SIGTH=	12.	DEGREES	TEMP=	25.5	DEGREE	(C)			

#### II. LINK VARIABLES

	LINK DESCRIPTION	*		COORDI Y1	INATES X2	(M) ¥2	*	TYPE	VPH	ef (g/mi)	H (M)	W (M)
		-*					*					
Α.	D		17544					FL	1277	13.4	5.0	10.0
₿.	E	*	17672	33291	17851	33317	*	FL.	1915	13.4	5.0	10.0
с.	М	*	17672	33291	17690	33142	*	AG	684	14.6	.0	10.0
D.	N	*	17690	33142	17749	32998	*	AG	352	14.5	.0	10.0
Ε.	0	*	17749	32998	17797	32929	*	AG	296	14.5	.0	10.0
F.	P	*	17800	32930	17850	32808	*	AG	411	14.5	.0	10.0
G.	Q	*	17850	32808	17892	32799	*	AG	206	14.5	.0	10.0
H.	н	*	17522	32818	17591	32846	*	AG	537	14.6	.0	10.0
I.	I	*	17591	32846	17797	32929	*	FL	701	14.6	3.0	10.0
J.	JL	*	17797	32929	17987	33066	*	AG	817	14.6	.0	10.0
к.	FF	*	17803	32501	17813	32421	*	AG	184	14.6	.0	10.0
L.	FF	*	17813	32421	17797	32377	*	AG	184	14.6	.0	10.0
М.	T	*	1,781,9	32527	17890	32456	*	AG	92	14.6	.0	10.0
N.	т	*	17890	32456	17911	32317	*	AG	92	14.6	.0	10.0
о.	U	*	17911	32317	17821	32532	*	AG	92	14.6	. 0	10.0

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 2

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JOB: Hung Shiu Kiu-traffic emission impact RUN: CO -AM (WORST CASE ANGLE) POLLUTANT: CO

#### III. RECEPTOR LOCATIONS

	*	COOR	DINATES	(M)
RECEPTOR	*	х	Y	z
	_ * _			
1. 285	*	17565	33286	5.0
2. 585	*	17564	33284	5.0

3.	1085	*	17568	33279	5.0
4.	2B6	*	17666	32880	3.0
5.	5B6	*	17665	32883	3.0
б.	10B6	*	17664	32888	3.0
7.	287	*	17818	32461	1.5
8.	587	*	17821	32462	1.5
9.	10B7	*	17826	32463	1.5
10.	5.5B8	*	17691	33284	5.0
11.	105B8	*	17694	33281	5.0
12.	5.5B9	*	17848	33314	5.0
13.	1089	*	17847	33310	5.0
14.	5.5B1.0	*	17955	33059	1.5
15.	10B10	*	17952	33062	1.5
16.	5.511	*	17802	32948	1.5
17.	10B11	*	17803	32953	1.5
18.	5.512	*	17710	33129	1.5
19.	10812	*	17714	33131	1.5

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 3

JOB: Hung Shiu Kiu-traffic emission impact RUN: CO -AM (WORST CASE ANGLE) POLLUTANT: CO

IV. MODEL RESULTS (WORST CASE WIND ANGLE )

RECEPTOR	* *	BRG (DEG)	* *	PRED CONC (PPM)	* * *	A	B	, C	CONC/I (PPN D		F	G	H
1. 285	*	85.	*	2.4	*	2.1	. 3	.0	.0	.0	.0	. 0	.0
2. 5B5	*	79.	*	1.7	*	1.5	.3	.0	.0	.0	.0	.0	.0
3. 1085	*	79.	*	. 9	*	.6	.3	.0	.0	.0	.0	.0	.0
4. 2B6	*	72.	*	1.5	*	.0	.0	. 0	.0	.0	.0	.0	.0
5. 5B6	*	80.	*	. 9	*	.0	.0	.0	.0	.0	.0	.0	.0
6. 10B6	*	82.	*	. 5	*	.0	.0	.0	.0	.0	.0	.0	.0
7. 2B7	*	195.	*	. 2	*	.0	.0	. 0	. 0	.0	.0	.0	.0
8.5B7	*	356.	*	.1	*	. 0	.0	.0	.0	.0	.0	. 0	.0
9. 10B7	*	357.	*	. 2	*	. 0	.0	.0	.0	.0	.0	.0	.0
10. S.SB8	*	282.	*	1.3	*	- 8	. 3	.1	. 0	.0	.0	.0	.0
11. 105B8	*	284.	*	. 9	*	.7	.1	.1	.0	.0	.0	.0	.0
12. 5.5B9	*	265.	*	3.6	*	.1	3.4	.0	.0	. 0	.0	.0	.0
13. 10B9	*	273.	*	2.2	*	.1	2.1	.0	.0	.0	.0	.0	.0
14. 5.5B10	*	218.	*	.6	*	.0	.0	. 0	.0	.0	.0	.0	.0
15. 10B10	*	221.	*	.5	*	.0	.0	.0	.0	.0	.0	.0	.0
16. 5.511	*	170.	*	.7	*	.0	.0	.0	.0	. 0	.3	.0	.0
17. 10Bll	*	172.	*	.6	*	.0	. 0	.0	.0	. 0	. 3	. 0	.0
18. 5.512	*	333.	*	.5	*	.1	. 0	. 4	.0	.0	.0	. 0	. 0
19. 10B12	*	330.	*	.4	*	.1	.0	.3	.0	.0	. 0	. 0	. 0

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 4

JOB: Hung Shiu Kiu-traffic emission impact RUN: CO -AM (WORST CASE ANGLE) POLLUTANT: CO IV. MODEL RESULTS (WORST CASE WIND ANGLE)

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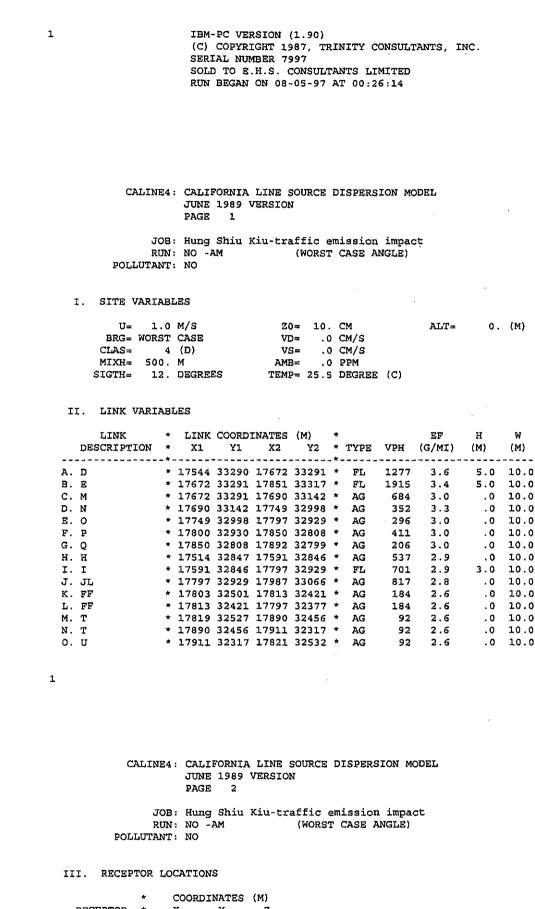
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	* *				NC/LII (PPM)	NK		`
RECEPTOR	*	I	J	к	L	м	N	0
1. 2B5	*	.0	.0	. 0	.0	.0	 •0	 .0
2. 5B5	*	. 0	.0	.0	.0	. 0	.0	.0
3. 10B5	*	.0	.0	.0	. 0	.0	.0	.0
4. 2B6	*	1.4	.1	.0	.0	. 0	.0	.0
5. 5B6	*	. 9	.0	.0	.0	.0	.0	. 0
6. 10B6	*	.5	.0	.0	.0	.0	- Ó	. 0
7.2B7	*	.0	.0	.1	.1	.0	- 0	. 0
8. 5B7	*	.0	.0	.0	.0	.0	.0	.0
9. 10B7	*	.0	.0	.0	.0	.0	.0	. 0
10. 5.5B8	*	.0	.0	.0	.0	.0	- 0	. 0
11. 105B8	*	.0	.0	.0	.0	.0	.0	.0
12. 5.5B9	*	.0	.0	. 0	. 0	. 0	.0	.0
13. 10B9	*	.0	.0	.0	.0	.0	.0	.0
14. 5.5B10	*	.0	.6	.0	. 0	.0	.0	. 0
15. 10B10	*	- 0	.4	.0	. 0	.0	.0	.0
16. 5.511	*	- 0	.4	.0	. 0	. 0	.0	.0
17. 10B11	*	.0	.3	.0	.0	.0	.0	.0
18. 5.512	*	- 0	.0	.0	.0	.0	.0	.0
19. 10B12	*	.0	.0	.0	.0	. 0	.0	.0

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RUN ENDED ON 08-05-97 AT 00:12:03



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	*	COOR	(M)	
RECEPTOR	*	х	Y	z
1. 2B5	*	17565	33286	5.0
2. 5B5	*	17564	33284	5.0

*	17568	33279	5.0	
*	17666	32880	3.0	
*	17665	32883	3.0	
×	17664	32888	3.0	
*	17818	32461	1.5	
*	17821	32462	1.5	
*	17826	32463	1.5	
*	17691	33284	5.0	
*	17694	33281	5.0	
*	17848	33314	5.0	
*	17847	33310	5.0	
*	17955	33059	1.5	
*	17952	33062	1.5	
*	17802	32948	1.5	
*	17803	32953	1.5	
*	17710	33129	1.5	
*	17714	33131	1.5	
	* * * * * * * * * * * *	<pre>17566 17665 17665 17664 17818 17821 17826 17826 17691 17694 17848 17847 17955 17952 17802 17803 17710</pre>	<ul> <li>17566 32880</li> <li>17665 32883</li> <li>17664 32888</li> <li>17818 32461</li> <li>17821 32462</li> <li>17826 32463</li> <li>17691 33284</li> <li>17694 33281</li> <li>17847 33310</li> <li>17955 33059</li> <li>17952 33062</li> <li>17802 32948</li> <li>17803 32953</li> <li>17710 33129</li> </ul>	<pre>* 17666 32880 3.0 * 17665 32883 3.0 * 17665 32888 3.0 * 17664 32888 3.0 * 17818 32461 1.5 * 17821 32462 1.5 * 17826 32463 1.5 * 17691 33284 5.0 * 17694 33281 5.0 * 17694 33281 5.0 * 17847 33310 5.0 * 17955 33059 1.5 * 17952 33062 1.5 * 17802 32948 1.5 * 17803 32953 1.5 * 17710 33129 1.5</pre>

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 3

JOB: Hung Shiu Kiu-traffic emission impact RUN: NO -AM (WORST CASE ANGLE) POLLUTANT: NO

IV. MODEL RESULTS (WORST CASE WIND ANGLE )

ŔĬ	SCEPTOR	* *	BRG (DEG)	* * * *	PRED CONC (PPM)	* *	A	B	c	CONC/I (PPI D		F	G	н
1.	285	*- *	85.	*	.4	*	.3	.1	.0	.0	.0	.0	.0	.0
2.	5B5	*	79.	*	.3	*	.2	.0	.0	.0	. 0	.0	.0	.0
3.	1085	*	78.	*	. 2	*	.1	.0	. 0	.0	. 0	. 0	.0	.0
4.	286	*	72.	*	. 2	*	.0	.0	.0	.0	.0	.0	.0	.0
5.	5B6	*	80.	*	.1	*	.0	.0	.0	.0	.0	.0	.0	. 0
6.	10B6	*	82.	*	.1	*	.0	.0	.0	.0	.0	.0	.0	. 0
7.	287	*	353.	*	.0	*	.0	.0	.0	.0	.0	.0	.0	. 0
8.	5B7	*	355.	*	.0	*	.0	.0	.0	.0	. 0	.0	.0	.0
9.	1087	*	356.	*	.0	*	.0	.0	0	.0	.0	.0	.0	.0
10.	S.5B8	*	282.	*	. 2	*	.1	. 1	. 0	.0	.0	.0	.0	.0
11.	10B8	*	284.	*	.1	×	.1	.0	.0	.0	.0	.0	.0	. 0
12.	5.5B9	*	265.	*	.6	*	.0	. 5	.0	.0	.0	.0	.0	.0
13.	1089	*	273.	*	.3	*	.0	.3	.0	.0	.0	. 0	. 0	. 0
14.	5.SB10	*	218.	*	.1	*	.0	.0	.0	.0	.0	.0	.0	.0
15.	10B10	*	221.	*	.1	*	.0	.0	.0	.0	.0	.0	.0	. 0
16.	5.5811	*	169.	*	.1	*	.0	. 0	.0	. 0	.0	.0	. 0	.0
17.	10811	*	172.	*	.1	*	.0	.0	.0	. 0	.0	.0	.0	. 0
18.	5.5B12	*	333.	*	.1	*	.0	.0	.0	. 0	.0	. 0	.0	. 0
19.	10B12	*	330.	*	1	*	.0	.0	.0	.0	.0	.0	.0	. 0

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 4

JOB: Hung Shiu Kiu-traffic emission impact RUN: NO -AM (WORST CASE ANGLE) POLLUTANT: NO IV. MODEL RESULTS (WORST CASE WIND ANGLE)

(CONT.)

.

		*				NC/LI (PPM)	NK		
R	ECEPTOR	*	I	J	к	L	М	N	0
1.	2B5	*	.0	.0	.0	.0	.0	.0	.0
2.	585	*	.0	. 0	.0	.0	. 0	. 0	.0
3.	1085	*	.0	.0	.0	.0	.0	. 0	. 0
4.	2B6	*	. 2	.0	.0	.0	.0		.0
5.	586	*	.1	.0	.0	.0	.0	. 0	. 0
б.	10B6	*	.1	.0	.0	.0	. 0	. 0	. 0
7.	287	*	.0	.0	.0	.0	.0	. 0	.0
8.	5B7	*	.0	.0	.0	.0	.0	.0	.0
9.	1087	*	.0	. 0	.0	.0	.0	. 0	.0
10.	5.5B8	*	.0	.0	.0	.0	.0	. 0	. 0
11.	1088	*	.0	.0	.0	.0	.0	.0	. 0
12.	5.5B9	*	.0	.0	.0	.0	.0	. 0	. 0
13.	10B9	*	- 0	.0	.0	.0	.0	.0	.0
14.	5.5B10	*	.0	.1	.0	.0	.0	. 0	.0
15.	10B10	*	.0	.1	.0	.0	.0	.0	. 0
16.	5.5B11	*	.0	. 0	.0	.0	.0	.0	.0
17.	10811	*	.0	. 0	.0	.0	.0		. 0
18.	5.5B12	*	.0	. 0	.0	. 0	.0	. 0	. 0
19.	10B12	*	.0	.0	.0	.0	.0	. 0	.0

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RUN ENDED ON 08-05-97 AT 00:26:34

IBM-PC VERSION (1.90) (C) COPYRIGHT 1987, TRINITY CONSULTANTS, INC. SERIAL NUMBER 7997 SOLD TO E.H.S. CONSULTANTS LIMITED RUN BEGAN ON 08-05-97 AT 00:25:25

CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 1

JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-AM (WORST CASE ANGLE) POLLUTANT: RSP-AM (NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL)

I. SITE VARIABLES

U=	1.0	M/S	Z0=	10.	CM		ALT =	Ο.	(M)
BRG=	WORST	CASE	VD=	.0	CM/S				
CLAS=	4	(D)	VS=	0	CM/S	· · · ·			
MIXH=	500.	М	AMB=	. 0	PPM				
SIGTH=	12.	DEGREES	TEMP=	25.5	DEGREE	(C)			

#### II. LINK VARIABLES

	LINK DESCRIPTION	*	LINK Xl	COORDI Y1	INATES X2	(M) ¥2	* * *	TYPE	VPH	EF (G/MI)	. н (М)	W (M)
Α.	D	*	17544	33290	17672	33291	*	FL	1277	.3	.0	10.0
в.	Е	*	17672	33291	17851	33317	*	FL	1915	.3	.0	10.0
с.	М	*	17672	33291	1,7690	33142	*	AG	684	.3	.0	10.0
D.	N	*	17690	33142	17749	32998	*	AG	352	3	.0	10.0
E.	0	*	17749	32998	17797	32929	*	AG	296	.3	0	10.0
F.	P	*	17800	32930	17850	32808	*	AG	ä <b>411</b>	.3	.0	10.0
G.	Q	*	17850	32808	17892	32799	*	AG	206	.3	.0	10.0
H.	H	. *	17514	32847	17591	32846	*	AG	537	. 2	.0	10.0
I.	I	*	17591	32846	17797	32929	*	FL	701	. 2	.0	10.0
J.	JL	*	17797	32929	17987	33066	*	AG	817	. 2	.0	10.0
К.	FF	*	17803	32501	17813	32421	*	AG	184	.2	.0	10.0
L.	FF	*	17813	32421	17797	32377	*	AG	184	.2	.0	10.0
М.	T .	*	17819	32527	17890	32456	*	AG	92	.2	. 0	10.0
Ν.	Т	*	17890	32456	17911	32317	*	AG	. 92	. 2	.0	10.0
ο.	U	*	17911	32317	17821	32532	*	AG	92	.2	.0	10.0

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 2

JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-AM (WORST CASE ANGLE) POLLUTANT: RSP-AM (NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL) 1

#### III. RECEPTOR LOCATIONS

RECEPTOR	* *	х	DINATES Y	z
1. 2B5 2. 5B5	*	17565 17564	33286	5.0 5.0

з.	1085	*	17568	33279	5.0
4.	286	*	17666	32880	3.0
5.	5B6	*	17665	32883	3.0
б.	10B6	*	17664	32888	3.0
7.	2B7	*	17818	32461	1.5
8.	5B7	*	17821	32462	1.5
9.	1087	*	17826	32463	1.5
10.	5.588	*	17691	33284	5.0
11.	1088	*	17694	33281	5.0
12.	5.5B9	*	17848	33314	5.0
13.	10B9	*	17847	33310	5.0
14.	5.5B10	*	17955	33059	1.5
15.	10B10	*	17952	33062	1.5
16.	5.5811	*	17802	32948	1.5
17.	10B11	*	17803	32953	1.5
18.	5.5B12	*	17710	33129	1.5
19.	10B12	*	17714	33131	1.5

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 3

JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-AM (WORST CASE ANGLE) POLLUTANT: RSP-AM (NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL)

IV. MODEL RESULTS (WORST CASE WIND ANGLE )

RI	CEPTOR	* *	BRG (DEG)	* *	PRED CONC (PPM)	* * *	A	B	с	CONC/I (PPN D		F	G	н
1.	2B5	*	85.	*	34.3	*	25.2	8.6	.5	.0	.0	.0	.0	. 0
2.	585	*	83.	*	30.4	*	21.6	8.4	.5	.0	.0	.0	.0	. 0
3.	10B5	*	79.	*	23.3	*	15.0	7.9	.4	. 0	.0	.0	.0	.0
4.	286	*	71.	*	20.9	*	. 0	.0	.0	.0	.3	.4	.0	.0
5.	5B6	*	78.	*	15.1	*	.0	. 0	.0	.0	. 1	.6	.0	. 0
6.	10B6	*	82.	*	10.4	*	.0	.0	.0	.0	.1	.7	.0	.0
7.	2B7	*	353.	*	3.2	*	.3	. 8	.3	. 3	. 2	. 2	.0	.0
8.	5B7	*	355.	*	3.1	*	. 2	. 9	.2	.2	.2	.3	.0	.0
9.	10B7	*	356.	*	3.4	*	.1	. 9	. 2	. 2	. 2	.4	. 0	.0
10.	5.588	*	69.	*	27.4	*	.0	27.4	.0	.0	. 0	.0	. 0	.0
11.	1088	*	283.	*	22.1	*	16.7	2.8	2.7	.0	.0	.0	.0	.0
12.	5.5B9	*	264.	*	45.0	*	3.3	41.3	.4	.0	.0	. 0	.0	.0
13.	1089	*	269.	*	36.6	*	2.9	33.4	.3	.0	.0	. 0	.0	.0
14.	5.5B10	*	218.	*	11.1	*	.0	.0	. 0	.0	.0	. 7	.0	.0
15.	10810	*	221.	*	9.2	*	.0	.0	.0	.0	. 1.	.6	.0	. 0
16.	5.5B11	*	169.	*	14.0	*	.0	.0	.0	.0	.1	6.8	.1	.0
17.	10B11	*	172.	*	11.9	*	.0	.0	.0	. 0	. 0	5.5	. 0	.0
18.	5.5B12	*	333.	*	9.8	*	2.6	.1	7.1	.0	. 0	. 0	.0	.0
19.	10B12	*	330.	*	8.7	*	2.7	.0	6.0	.0	.0	.0	.0	.0

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 4

JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-AM (WORST CASE ANGLE) POLLUTANT: RSP-AM

### (NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL)

### IV. MODEL RESULTS (WORST CASE WIND ANGLE)

RECEPTOR	*	I	J		NC/LII (PPM) L	ńk M	N	o
1. 2B5	*	.0	.0	.0	.0	.0	.0	.0
2. 5B5	*	.0	.0	.0			-	
3. 10B5	*	. 0	.0	.0				
4. 2B6		18.1	2.1	.0	.0		+	-
5. 5B6	*	13.6	.8	. 0	.0	.0	. 0	.0
6. 10B6	*	9.1	.5	.0	. 0	.0	.0	.0
7.2B7	*	.5	. 2	.3	.0	.1	.0	
8. 5B7	*	.4	.3	.1	.0	.2	- 0	.2
9. 10B7	*	• •	.4	.0	.0	.3	. 0	. 4
10. 5.5B8		.0	.0	.0	.0	.0	.0	.0
11. 10B8	*	.0	.0	.0	.0	.0	.0	.0
12. 5.5B9	*	.0	.0	.0	. 0	.0	.0	.0
13. 1089	*	.0	.0	.0	.0	.0	.0	.0
14. 5.5B10	*	.1	10.3	.0	.0	.0	- 0	. 0
15. 10B10	*	.4	8.2	.0	.0	.0	٠0	. 0
16. 5.5B11	*	.1	6.8	.0	.0	.1	-1	
17. 10B11	*	.1	6.0	. 0	.0	.1	.1	.1
18. 5.5B12	*	. 0	.0	.0	.0	.0	.0	. 0
19. 10B12	*	۰.	.0	.0	.0	.0	.0	. 0

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### RUN ENDED ON 08-05-97 AT 00:25:45

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IBM-PC VERSION (1.90) (C) COPYRIGHT 1987, TRINITY CONSULTANTS, INC. SERIAL NUMBER 7997 SOLD TO E.H.S. CONSULTANTS LIMITED RUN BEGAN ON 08-05-97 AT 00:30:12

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 1 JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-PM (WORST CASE ANGLE) POLLUTANT: RSP-PM

(NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL)

I. SITE VARIABLES

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U=	1.0	M/S	Z0=	10.	CM		ALT =	٥.	(M)
BRG=	WORST	CASE	VD=	.0	CM/S				
CLAS=	6	(F)	VS=	.0	CM/S				
MIXH=	500.	м	AMB=	. 0	PPM				
SIGTH=	5.	DEGREES	TEMP=	25.5	DEGREE	(C)			

#### II. LINK VARIABLES

	LINK	*	LINK	COORDI	INATES	(M)	*			EF	н	W
E	DESCRIPTION	*	Xl	Yl	X2	¥2	*	TYPE	VPH	(G/MI)	(M)	(M)
		*-					. * .					
A. [	)	*	17544	33290	17672	33291	*	FL	881	.3	.0	10.0
B. 5	2	*	17672	33291	17851	33317	*	FL	1320	.3	.0	10.0
C. M	1	×	17672	33291	17690	33142	*	AG	462	.3	.0	10.0
D. N	1	*	17690	33142	17749	32998	*	AG	246	. 4	.0	10.0
Е. С	)	×	17749	32998	17797	32929	*	AG	212	.4	.0	10.0
F. 4	2	×	17800	32930	17850	32808	*	AG	325	.3	.0	10.0
G. (	2	*	17850	32808	17892	32799	*	AG	163	.3	.0	10.0
н. F	ł	*	17514	32847	17591	32846	*	AG	383	.3	.0	10.0
I. 1	[	*	17591	32846	17797	32929	*	FL	507	. 3	.0	10.0
J. J	JL	*	17797	32929	17987	33066	*	AG	672	.3	.0	10.0
к. в	FF	*	17803	32501	17813	32421	*	AG	186	.3	.0	10.0
L. E	?F	*	17813	32421	17797	32377	*	AG	186	.2	.0	10.0
м. 1	6	*	17819	32527	17890	32456	*	AG	81	.3	.0	10.0
N. 7	C	*	17890	32456	17911	32317	*	AG	81	. 3	.0	10.0
0. t	Ţ	*	17911	32317	17821	32532	*	AG	81	.3	.0	10.0

CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 2

JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-PM (WORST CASE ANGLE) POLLUTANT: RSP-PM (NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL)

III. RECEPTOR LOCATIONS

	*	COOR	COORDINATES				
RECEPTOR	*	х	Y	· 2			
	-*-						
1. 2B5	×	17565	33286	5.0			
2. 5B5	*	17564	33284	5.0			

з.	10BS	*	17568	33279	5.0
4.	2B6	*	17666	32880	3.0
5.	5B6	*	17665	32883	3.0
6.	1086	*	17664	32888	3.0
7.	2B7	*	17818	32461	1.5
8.	5B7	*	17821	32462	1.5
9.	10B7	*	17826	32463	1.5
10.	5.588	*	17691	33284	5.0
11.	10B8	×	17694	33281	5.0
12.	5.5B9	*	17848	33314	5.0
13.	1089	*	17847	33310	5.0
14.	5.5B10	*	17955	33059	1.5
15.	10B10	*	17952	33062	1.5
16.	5.5B11	*	17802	32948	1.5
17.	10B11	*	17803	32953	1.5
18.	5.5B12	*	17710	33129	1.5
19.	10B12	*	17714	33131	1.5

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#### CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 3

JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-PM (WORST CASE ANGLE) POLLUTANT: RSP-PM (NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL)

#### IV. MODEL RESULTS (WORST CASE WIND ANGLE )

RECEPTOR	* *	BRG (DEG)	* * *	PRED CONC (PPM)	* *	А	В	с	CONC/L (PPM D		F	G	н
1. 2B5	*	86.	*	48.3	*	31.0	16.7	.6	.0	.0	.0	. 0	.0
2. 585	*	84.	*	42.5	*	25.9	16.2	.4	. 0	.0	.0	.0	. 0
3. 10B5	*	82.	*	31.3	*	13.7	17.2	.3	. 0	.0	.0	. 0	.0
<b>4. 2B6</b>	*	70.	*	31.2	*	.0	.0	.0	.0	.4	.6	.0	.0
5. 5B6	*	74.	*	20.8	*	.0	.0	. 0	.0	. 1	. 9	. 0	.0
6. 10B6	*	77.	*	13.5	*	.0	.0	.0	.0	.1	1.0	.0	.0
7. 2B7	*	360.	*	5.1	*	. 0	1.6	.0	.0	.1	1.4	.0	. 0
8. SB7	*	360.	*	5.6	*	. 0	1.5	. 0	.0	.1	1.4	.0	.0
9. 10B7	*	359.	*	6.3	*	. 0	1.7	.0	.0	.1	1.5	.0	.0
10. 5.5B8	*	74.	*	30.6	*	. 0	30.6	.0	.0	.0	.0	.0	.0
11. 10B8	*	278.	*	23.5	×	20.7	.1	2.7	. 0	.0	.0	.0	.0
12. 5.589	*	264.	*	61.2	*	б.9	54.0	.4	. 0	.0	.0	.0	.0
13. 10B9	*	266.	*	47.6	*	6.4	40.9	. 3	.0	.0	.0	.0	.0
14. 5.5B10	*	226.	*	15.8	*	.0	.0	. 0	.0	.0	1.0	.0	.0
15. 10B10	*	225.	*	13.1	×	.0	.0	. 0	.0	.0	1.0	.0	.0
16. 5.5B11	*	166.	*	19.0	*	.0	.0	.0	.0	.0	11.2	.0	.0
17. 10B11	*	170.	*	15.8	*	.0	. 0	.0	.0	. 0	8.1	0	.0
18. 5.5B12	*	341.	*	11.5	*	2.7	.1	8.7	.0	.0	.0	.0	.0
19. 10812	· *	339.	*	10.1	*	2.8	.1	7.3	.0	.0	.0	.0	.0

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CALINE4: CALIFORNIA LINE SOURCE DISPERSION MODEL JUNE 1989 VERSION PAGE 4 ŝ

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JOB: Hung Shiu Kiu-traffic emission impact RUN: RSP-PM (WORST CASE ANGLE) POLLUTANT: RSP-PM

### (NOTE: OUTPUT IN MICRO-GRAMS/METER\*\*3. IGNORE PPM LABEL)

### IV. MODEL RESULTS (WORST CASE WIND ANGLE)

	*							
RECEPTOR	*	I	J	ĸ	Ľ	М	N	0
1. 285	*	.0	. 0	.0	.0	. 0	.0	
2. SB5	*	. 0	.0	. 0	.0	.0	.0	.0
3. 10BS	*	.0	. 0	. 0	.0	.0	.0	.0
4.2B6	*	27.0	3.2	.0	. 0	0	.0	.0
5. 5B6	*	18.6	1.1	.0	. 0	.0	. 0	.0
6. 10B6	*	11.7	.7	.0	.0	. 0	. 0	.0
7. 2B7	*	.1	1.3	.0	.0	.3	. 0	.3
8. 587	*	.1	1.4	.0	. 0	.4	.0	.6
9. 10B7	*	.1	1.3	.0	.0	.6	.0	. 9
10. 5.5B8	*	- 0	.0	.0	.0	.0	.0	. 0
11. 1038	*	.0	. 0	.0	.0	. 0	.0	. 0
12. 5.5B9	*	.0	. 0	.0	.0	. 0	.0	.0
13. 1089	*	. 0	.0	.0	.0	. 0	. 0	.0
14. 5.5BlO	*	.3	14.5	. 0	.0	.0	.0	. 0
15. 10B10	*	۰3	11.7	. 0	. 0	. 0	. 0	. 0
16. 5.5B11	*	- 0	7.6	.0	.0	.0	.1	. 0
17. 10B11	×	.0	6.9	.0	.0	.1	. 3	.3
18. 5 <i>.</i> 5B12	*	.0	. 0	.0	.0	.0	.0	.0
19. 10812	*	. 0	.0	.0	.0	.0	. 0	.0

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RUN ENDED ON 08-05-97 AT 00:30:31

# Appendix 6

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# Sample for Calculation on Construction Noise Impact

### Un-mitigated

F

Constru	iction Noise Impact at Hung Sh	ui Kiu (witl	out mitigat	ion measures	)			
lstance fi	om source e.g.	8.5	m					
tage I	I Site Clearance Work, Excavation for Roa	d Allanment		-				
tage	Equipment used at one working zone							
		··	·		<u> </u>			· · · · · · · · · · · · · · · · · · ·
D. Code	PME used	SWL, dB(A)	Nos, used		Screening	% on time	Correction, dB(A)	SPL at NSR, dB(A)
NP 030	Buildozer	115	1	26.6	0.0	50.0	3.0	85.4
NP 141	LORY	112		26.8	0.0	25,0	6.0	79.4
NP 081	I Excavator	112	1	26.6	0.0	25.0	6.0	79,4
	Cumulative PNL =	85.4	L		íí			
	Contection for facade =	3.0						
	CNL =		dB(Å)		i			
							1	
tage 3	Installation of Underground Drains, Serv	ces Utilities &	Manhole					
	Equipment used at one working zone	1						
	PME used	SWL, dB(A)	Nos. used		Screening	% on time	Correction, dB(A)	SPL at NSR, dB(A)
VP 141	Lorry	112	1 1	26.6	0.0	25.0	6.0	79.4
NP 048	Mobile Crane	112	1	26.6	0,0	25.0	6,0	79,4
NP 047	Concrete Mixer	109		26.6	0.0	50.0	3.0	79.4
NP 170	Poker	113	1	26.6	0.0	50,0	3.0	83,4
NP 102	Generator	100	1	26,8	0.0	100.0	0,0	73.4
	Cumulative PNL =				<u> </u>			
	Correction for facade =	3.0	i		i i			
	ICNL #	88.1	IdB(A)		ii			
	<u></u>		1		<u> </u>		-	
tage 4	Formation of road sub-base				[	•		
	Equipment used at one working zone	···			i	· · · · · · · · · · · · · · · · · · ·	1	
I.D. Code		SWL, dB(A)	Nos. used	Dist. Attn.,dB(A)	Screening	% on time	Correction, dB(A) +	SPL at NSR, dB(A)
NP 030	Buldozer	115		26.8	0.0	50.0	3.0	85.4
NP 141	iar	112		28.6	0.0	25.0	6.0	79.4
NP 185	Road roller	108	i	26.6	0.0	50.0	3.0	78.4
			!					
	Cumulative PNL =	86.4	· · · · · · · · · · · · · · · · · · ·	<b>-</b>			<u> </u>	
	CNL =	1 89.4	(dB(A)					
				1		· · · · · · · · · · · · · · · · · · ·		
tage 5	Road surfacing and finishing works (2 m	onths)			<u> </u>		· · · · ·	
I.D. Cade		SWL, dB(A)	Nos. used	Dist. Attn.,dB(A)		% on time	Correction, dB(A)	SPL at NSR, dB(A)
I.D. Caue	PMc uses	I STYL, UD(A)	1 1002-0360	Disc Add., 00(A)	screening i	74 OR LINN	Correction, ub(A)	OFL ALNOR, UDIAL
NP 021	Bar Bender	90	<u></u>	26,6	0.0	25.0	8.0	57.4
NP 141	Lony	112		26.6	0.0	25.0	6.0	79,4
NP 044	Concrete Lony Mixer	109		26.6	0,0	25.0	6,0	76.4
NP 047	Concrete Pump	109	1	28.8	0.0	25.0	6.0	76.4
NP 170	Poker	113	1	28.8	_0.0	25.0	6.0 1	50,4
NP 004	or Asphalt paver	1 109	1	26.6	0.0	50.0	3.0	79.4
NP 185	Road roller	108	<u>├</u>	20.0	0.0 1	50.0	3.0	78.4
	4	1	1	1				
	Cumulative PNL =	62.9		1				
	Correction for facade =	3.0	IdB(A)					
	1. INTER-	0.8	1		+		<u> </u>	. <u> </u>
NSR	Distance from source	Stage 1	Stage 3	Stage 4	Stage 5		1	
C3	8.5	68,4	88.1	89.4	85.9			

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onstru	uction Noise Impact a	t Hung Shi	u Kiu (with s	ilenced equ	ipment)				
stance fr	rom source	e.g.	8.5	m					
tage 1	Site Clearance Work, Excav	ation for Road	i Allaoment	L	i				· · · · · · · · · · · · · · · · · · ·
	Equipment used at one wor				,				
	<u> </u>			<u> </u>	!				
.D. Code	PME used		SWL, dB(A)	Nos. used	Dist. Attn.,dB(A)	Screening	% on time	Correction, dB(A)	SPL at NSR, dB(A)
CNP 030	Bulidozer		100	1	25.6	0.0	50,0	3.0	70.4
CNP 141	Lony		100	1	26.6	0.0	25.0	6.0	67.4
CNP 081	Excavator		112		26.6	0.0	25.0	6.0	79,4
	Cumulative PNL =		79.7	<u> </u>					~ <u></u>
	Correction for facade #		1 3,0		;				
<u> </u>	CNL =		82.7	dB(A)	<u> </u>				
				<u> </u>	; ;				
Stage 3	Installation of Underground	Drains, Servi	ces Utilities & Ma	nhole	i	1		<u></u> i	·
	Equipment used at one wor	king zone		1		i			
<b>.</b>	PME used		SWL, dB(A)	Nos. used	Dist. Attn.,dB(A)	Screening	% on time	Correction, dB(A)	SPL at NSR, dB(A)
CNP 141 CNP 048	Lony Mobile Crane		110	1	26.6	0.0	25.0 25.0	6.0	77.4
	!or		1		: 20.0	1			
CNP 047	IConcrete Pump		105	1	26.6	0.0	50.0	3.0	75.4
CNP 170 CNP 102	Poker		1 110	1	26,6	0.0	50.0 100,0	3.0	<u>80.4</u> 73.4
		· · · · · · · · · · · · · · · · · · ·		·	20.0	0.0	100,0		
	Cumulative PNL =		82.2		i	1			
	Correction for facade =		3.0	(d8(A)	<u></u>				
					<u> </u>	i i			
	ļ			<u> </u>					
Stage 4	Formation of road sub-base				l				
	Equipment used at one wo	rking zone		·	(	!			
I.D. Code CNP 030	i PME used iBuildozer		SWL, dB(A)	Nos, used	Olst. Attn.,dB(A) 26.6	Screening   0.0	% on time 50.0	Correction, dB(A) 3.0	SPL at NSR, dB(A) 70.4
CNP 141	(Lony		1 110	1 1	26.6	0.0	25.0	6.0	77.4
	lor				· · · · · · · · · · · · · · · · · · ·				
CNP 165	Road roller		108	1	26.6	0.0	50.0	3.0	78.4
	Cumulative PNL =		78,4	<u> </u>		i — 1			
	Correction for facade =		3.0		·				
,	CNL =		81.4	(dB(A)	1				
				1	1	1 1			
Stage 5	Road surfacing and finishing	ng works (2 m	onths)	<u> </u>					
1.D. Code	PME used		SWL, dB(A)	Nos. used	Oist. Attn.,dB(A)	Screening	% on time	Correction, dB(A)	SPL at NSR, dB(A)
1.0. COUN			3012, 00(6)	1103. 0540	CIAL AULUDIAN	i acreening		Contraction, dury	
CNP 021	Bar Bender		90	1	26.6	0.0	25.0	6.0	57.4
CNP 141	or		110	1	28.6	0.0	25.0	6,0	77.4
CNP 044	Concrete Lorry Mixer		109	1	26.6	0.0	25.0	6.0	78.4
CNP 047	Concrete Pump		105	1	26,6	0.0	25.0	6.0	72.4
CNP 170	Poker		110	1	25.6	0.0	25.0	6.0	77.4
CNP 004	Asphalt paver		109	1	28.6	0.0	50.0	3.0	79.4
CNP 185	Road roller		108	1	26.6	0.0	50.0	3.0	78,4
	Cumulative PNL =		51.9	<u> </u>	1				
	Correction for facade =		3.0	<u>i                                     </u>	1		· · · · · · · · · · · · · · · · · · ·		
	CNL =		84,9	IdB(A)	1				
NED	Ot to part to an			1	Stane 4			·	
NSR	Distance from se	ource	Stage 1	0.0400		Stage 5		<b> </b>	
C3	8.5		\$2,7	85,2	81.4	84,9		I	

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#### silenced & screened

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Construction Noise Impact at Hung Shi Istance from source e.g.		m		1	···- ··	·	
	10.0		· · · · · ·			+	
tage 1 Site Clearance Work, Excavation for Road	d Alignment			· · · · · ·			
Equipment used at one working zone			· · · · · · · · · · · · · · · · · · ·				
D. Code PME used	SWL, dB(A)	Nos. used	Dist. Attn.,dB(A) 26.6	Screening	% on time 50.0	Correction, dB(A) 3.0	SPL at NSR, dB(A)
ior	<u> </u>		20.0				65,4
NP 141 LOTY	100	1	26.6	5.0	25.0	6.0	62.4
NP 081 Excavator	1 112	1	26.6	5.0	25.0	6.0	74,4
;Overall SWL, dB(A) ;Cumulative PNL =	74,7		<u> </u>				·
Correction for facade #	3.0		· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·
CNL =		dB(A)	· · · · · · · · · · · · · · · · · · ·	1			
			1				
tage 3 Installation of Underground Drains, Servi	ces Utilities &	Manhole		l			
Equipment used at one working zone	1		<u>i</u>	]			
PME used	SWL, dB(A)	Nos. used	Dist. Attn.,dB(A)	Screening	% on time	Correction, dB(A)	SPL at NSR, dB(A)
NP 141 ILony NP 048 Mobile Crane	110		26.6	5.0 10.0	25.0 25.0	6.0	72,4
			, 20,0	(0.0	23.0	0.0	02.9
NP 047 Concrete Pump	105	1	26.6	10,0	50.0	3.0	65.4
NP 170 Poker	110	1	26.6	10.0	50.0	3.0	70,4
NP 102 (Generator	100	1	28.6	10.0	100.0	0.0	63,4
Overall SWL, dB(A)	72.8			1			
Correction for facade =	1 3.0		· · · · · · · · · · · · · · · · · · ·				
CNL =		dB(A)	<u> </u>		·		· · · · · · · · · · · · · · · · · · ·
	1		<u> </u>	<u>     i</u>		· · · ·	
tage 4 Formation of road sub-base			· _				
Equipment used at one working zone							
I.D. Code   PME used	SWL, dB(A)	Nos. used	Dist. Attn.,dB(A)		% on time	Correction, dB(A)	SPL at NSR, dB(A)
NP 030 Buildozer	100	1		1 5.0	50.0 25.0	3.0	65.4
INP 141 ILONY	110		26.6	5.0	25.0	0.0	72.4
NP 185 Road roller	1 108		26.6	5.0	50.0	3.0	73.4
Overall SWL, d8(A)			1				
Cumulative PNL =	1 73,4		!	1			
Correction for facade =	3.0	1	<u>i</u>	<u> </u>			· · · · · · · · · · · · · · · · · · ·
CNL =	76.4		· · · · · · · · · · · · · · · · · · ·	· · · · · ·			
itage 5  Road surfacing and finishing works (2 m	onths)	l					<u> </u>
I.D. Code PME used	SWL, dB(A)	Nos, used	Dist. Attn.,dB(A)	Screening	% on time	Correction, dB(A)	SPL at NSR, dB(A)
NP 021  Bar Bender	90		26.6	5.0	25.0	6.0	52.4
NP 021 IBal Bender	1 110	1	26.6	5.0	25.0	6.0	72.4
	1 10		20.0	0.0	40,0	4.4	72.4
NP 044 Concrete Lorry Mixer	1 109	1	1 26.6	5.0	25.0	6.0	71.4
NP 047 Concrete Pump	105	1	26.6	10.0	25.0	6.0	62.4 -
NP 170 IPoker	1110	1	28,6	10.0	25.0	6.0	67.4
NP 004 Asphalt paver	109	1	26.6	5.0	50.0	3.0	74,4
NP 185 Road roller	108	<del>       </del>	26.6	5.0	50.0	3.0	73.4
Overall SWL, dB(A)		1		1			
Cumulative PNL =	76.9	1					
Correction for facade =	3.0	2013		<u> </u>			
[CNL ≠	79.9	dB(A)		<u>i</u>	·	<u> </u>	
NSR Distance from source	l Store f	Ctore 7	Etras d			<u>_</u>	
				STADAS			
	and from courses	ance from source	nce from source Stone 1 Stage 3	nce from source Stane 1 Stane 3 Stane 4	nce from source Stage 1 Stage 3 Stage 4 Stage 5	Ince from source Stane 1 Stane 3 Stane 4 Stane 5	Ince from source Stage 1 Stage 3 Stage 4 Stage 5

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### **Construction Noise Impact**

Sample on Calculation of "Period of Exceedance" at NSRs after the use of silenced PME and Mobile Noise Barriers/ Enclosures as Mitigation Measures

#### APPENDIX

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	n calculation of "Period of Exceedance" a					
NSR	Distance from source	Phase 1	Phase 2	Phase 3	Phase 4	Phase 5
C2	6.5	80,0	<u>N/A</u>	78,1	78.7	82,3
		L,				
Stage 1	Site Clearance Work, Excavation for Road A	lignment				
	Rate of Roadworks	15	m/day			
		· · ·				
Day	Distance of NSR from noise source (m)	PNL, dB(A)	Max. Period of Exc	ceedance (day)		
1 '	30.7	66.5	1.5			
1.5	23.4	68.9				
2	16.3	72.0				
	9.9	76.3			·	·
2.5						
2.75	7.5	78.7				
3	6.5	80.0				
3.25	7.5	78.7				
3.5	9.9	76.3				
4	16.3	72.0				
4,5	23.4	68,9				
5	30.7	66.5			· · · · · ·	
		·				
•		1	<u> </u>			
se 3	Installation of Underground Drains, Service					
	Rate of Roadworks	10	m/day			
Day	Distance of NSR from noise source (m)	PNL, dB(A)	Max. Period of Exc	eedance (day)		
1	21.0	67.9	1.5		· · · · · · · · · · · · · · · · · · ·	
1.5	16.3	70.1				
2	11.9	72.9		1		
2,5	8.2 .	76.1				
2.75	7.0	77.5			· · · · ·	
3	6,5	78.1				
3.25	7.0	77.5				
3.5	8.2	76.1	•			
4	11,9	72.9				
4.5	16.3	70.1				
*****						
5	21.0	67,9		··		
se 4	Formation of road sub-base	ļ				
	Rate of Roadworks	50	m/day			
Day	Distance of NSR from noise source (m)	PNL, dB(A)	Max. Period of Exc	eedance (day)		
1	100,2	55.0	0.4	T		
1.5	75.3	57.4				
				+		
2	50.4	60.9	·   · =			
2.5	25.8	\$6.7	•			
2.75	14.1	72.0				·
3	6.5	78,7				
3.25	14.1	72.0				
3.5	25.8	65.7			· · · · · · · · · · · · · · · · · · ·	
4	50.4	60,9				h
					<u> </u>	
4.5	75.3	57,4			<u> </u>	
5	100.2	55,0				
		<u> </u>			<u>-</u>	
	Road surfacing and finishing works (2 mon	ths)				·
se 5		25	m/day			
se 5	Rate of Roadworks					
se 5	Rate of Roadworks					· · · · ·
			May Deried of Fur	reedance (daw)		1
Day	Distance of NSR from noise source (m)	PNL, dB(A)	Max. Period of Exc	ceedance (day)		
Day 1	Distance of NSR from noise source (m) 50,4	PNL, dB(A) 64.5	Max. Period of Exc 1	ceedance (day)		
Day 1 1.5	Distance of NSR from noise source (m) 50,4 38,1	PNL, dB(A) 64.5 66.9		ceedance (day)		
Day 1	Distance of NSR from noise source (m) 50.4 38.1 25.8	PNL, dB(A) 64.5		ceedance (day)		
Day 1 1.5	Distance of NSR from noise source (m) 50,4 38,1	PNL, dB(A) 64.5 66.9		ceedance (day)		
1 1.5 2	Distance of NSR from noise source (m) 50.4 38.1 25.8	PNL, dB(A) 64.5 66.9 70.3 75.5		ceedance (day)		
Day 1 1.5 2 2.5 2.75	Distance of NSR from noise source (m)           50,4           38,1           25.8           14,1           9,0	PNL, dB(A) 64.5 66.9 70.3 75.5 79.4		Ceedance (day)		
Day 1 1.5 2 2.5 2.75 3	Distance of NSR from noise source (m)           50,4           38,1           25,8           14,1           9,0           6,5	PNL, dB(A) 64.5 66.9 70.3 75.5 79.4 82.3		Ceedance (day)		
Day 1 1.5 2 2.5 2.75 3 3.25	Distance of NSR from noise source (m)           50,4           38.1           25.8           14.1           9.0           6,5           9.0	PNL, dB(A) 64.5 66.9 70.3 75.5 79.4 82.3 79.4		Ceedance (day)		
Day 1 1.5 2 2.5 2.75 3	Distance of NSR from noise source (m)           50,4           38.1           25.8           14.1           9.0           6,5           9.0           14.1	PNL, dB(A) 64.5 66.9 70.3 75.5 79.4 82.3		ceedance (day)		
Day 1 1.5 2 2.5 2.75 3 3.25	Distance of NSR from noise source (m)           50,4           38.1           25.8           14.1           9.0           6,5           9.0	PNL, dB(A) 64.5 66.9 70.3 75.5 79.4 82.3 79.4		ceedance (day)		
Day 1 1.5 2 2.5 2.75 3 3.25 3.5	Distance of NSR from noise source (m)           50,4           38.1           25.8           14.1           9.0           6,5           9.0           14.1	PNL, dB(A) 64.5 66.9 70.3 75.5 79.4 82.3 79.4 79.4 75.5		ceedance (day)		

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## Letter from the HKHS



香港房屋協會 HONG KONG HOUSING SOCIETY

Founded 1948 Incorporated by Government Ordinance 1951

DKSL/HSK-810-001(2/96)/jc **Our Reference** 

Your Reference 26 February 1996

> EHS Consultants Limited 22/F Loyong Court Commercial Bldg 220 Lockhart Road Hong Kong

Attn: Dr Sarah Liao

Dear Sirs

### Proposed Housing Development in Hung Shui Kiu Area 13

Thank you for your letter of 7 February 1996.

Please be advised that the proposed development is still under preliminary planning stage and as such no detailed building design has been formulated. For your reference, I have enclosed the latest approved planning brief in respect of the project. It should be noted that the site will be zoned for "Residential (Group A)" in the Ping Shan Outline Zoning Plan.

Incidentally, I append hereunder the proposed development programme for your information:-

	<u>Target Commencement Date</u>	<u>Target Completion Date</u>
Phase I	Late 1999	2002
Phase II	Early 2000	2002

Please feel free to contact me should you need any further assistance.

Yours faithfully

Daniel-Lac

Property Development Manager 總辦事處:香港銅鑼灣告士打道280號世界貿易中心29樓 電話:2839 7888 圖文傳真: 2882 2001 Head Office: 29th Floor, World Trade Centre, 280 Gloucester Road, Causeway Bay, Hong Kong. Tel: 2839 7888

#### 4. Site Constraints and Opportunities

#### 4.1 Constraints

The constraints on the development of Area 13 for rental housing are summarized below:

#### (a) <u>Land Status and Tenure</u>

The proposed site is largely held under private ownership. It will have to be resummed and the estimated time required for land resumption is about 28 months from the date of submission of Clearance Application Form.

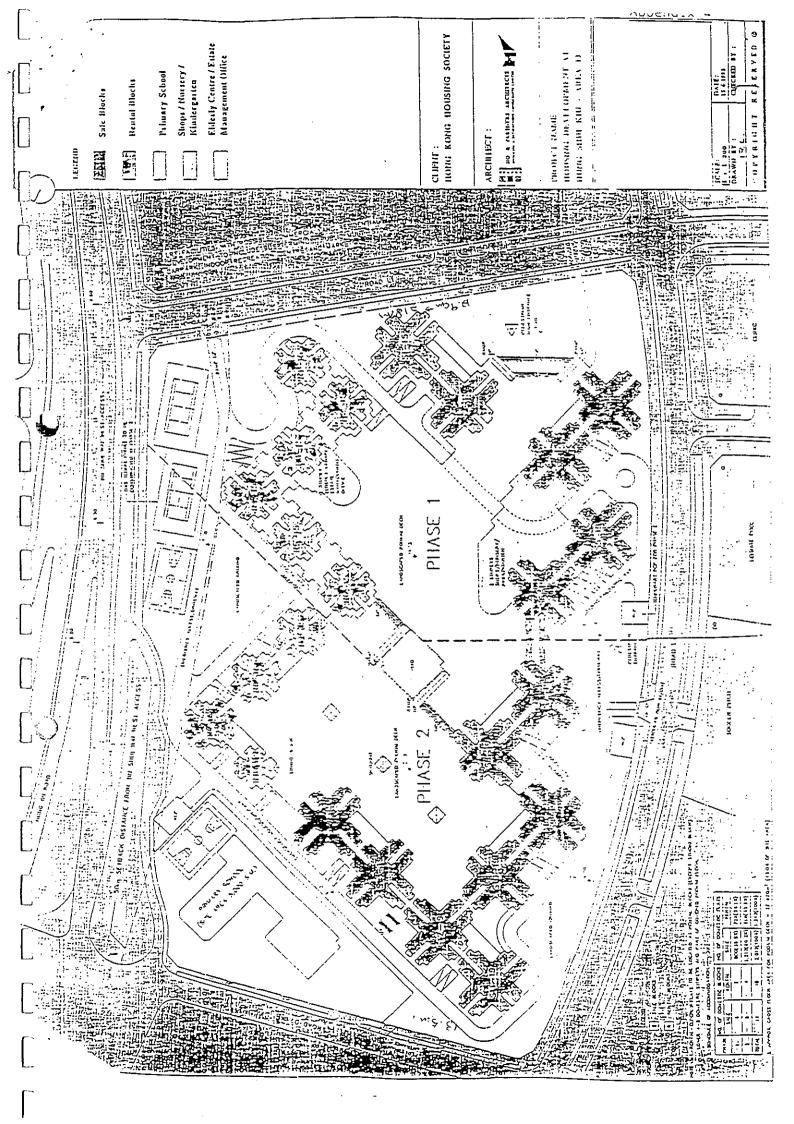
#### (b) <u>Noise and Air Pollution</u>

The eastern side of the proposed estate will be facing the Tin Shui Wai West Access which is one of the major access in and out of Tin Shui Wai New Town. The access is linked to a flyover (PWP Item No. 308THB) across Castle Peak Road joining TSW West Access and the Yuen Long Highway which lands at the southern part of the site. This would be a major source of noise pollution. Given the proposed flyover development and the heavy traffic on the TSW West Access, building setback of 50m is proposed as a noise buffer as well as the provision of a 4m high-120m long noise barrier wall along the West Access has been included as part of the project. The development should also make full use of suitable noise tolerant shielding elements such as commercial centre, multi-storey carparks or landscape features etc. to screen the residential block from Furthermore, the residential blocks should be the roads. positioned and designed so that the angle of view of the roads from the noise sensitive portion of the buildings could be minimized. Moreover, the proposed housing development may also subject to possible air pollution. A possible source of air pollution will be from the emission of vehicles using the West Another source of air pollution is possibly from the Access. sucke emitted from chimneys at the Kiu Tau Wai Industrial Area in the North-east. It is suggested that HKHS should explore all potential mitigation measures and solutions in consultation with EPD when undertaking the Environmental Impact Assessment; during the detailed design stage.

#### (c) <u>Visual Intrusion</u>

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> The main source of visual intrusion will be from the container storage depots in the north and north-east many of which are in existence prior to the gazetting the draft Ping Shan Development Permission Area Plan. These container storage yards are tolerated under the Town Planning Ordinance. Containers stacked seven high will block off some of the view of the residents. The proposed flyover from Yuen Long Highway across Castle Peak Road that land onto the West Access right in front of the site is another source of visual intrusion.



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# Site-specific Pollution Control Clauses

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### Proposed Environmental Pollution Clauses for Hung Shiu Kiu Development

#### 1. GENERAL SPECIFICATION FOR ENVIRONMENTAL PROTECTION

- (a) All works are to be carried out in such a manner as to cause as little inconvenience as possible to nearby residents, properties and to the public in general, and the Contractor shall be held responsible for any claims which may arise from such inconvenience.
- (b) Water shall be used to prevent dust rising and the Contractor shall take every precaution to prevent the excavated materials from entering into public drainage system
- (c) The Contractor shall carry out the Works in such a manner as to minimise adverse impacts on the environment during execution of the Works.
- (d) The Contractor shall comply with all current legislation and regulations including:-
  - Noise Control Ordinance (Cap 400)
  - Air Pollution Control Ordinance (Cap 311)
  - Water Pollution Control Ordinance (Cap 358)
  - Dumping at Sea Act 1974 (Overseas Territory Order) 1975
  - Merchant Shipping (Oil Pollution) (Hong Kong) Order 1975
  - Summary Offences Ordinance (Cap 228)
  - Factories and Industrial Undertakings Ordinance (Cap 59)
  - Waste Disposal Ordinance (Cap 354)
  - Public Cleansing and Prevention of Nuisances (Regional Council) By-Laws (Cap 132)
  - Public Cleansing and Prevention of Nuisances (Urban Council) By-Laws (Cap 132)
  - Building Ordinance (Cap 123)
  - Building Ordinance (Application to New Territories) Ordinance (Cap 121)
  - Public Health and Municipal Services Ordinance (Cap 132)
  - Waste Disposal (Chemical Waste) (General) Regulation (Cap 354)
- (e) The provisions of this section shall not be applicable in the case of emergency work necessary for the saving of life or property or the safety of the Works.
- (f) The Contractor shall be responsible for ensuring no earth, rock or debris is deposited on public or private rights of way as a result of its operation, including any deposits arising from the movement of plant or vehicles. For site formation works the Contractor shall provide a washpit or a wheel washing and/or vehicle cleaning facility at all the exists from the Site. Water in wheel washing facilities shall be changed at frequent intervals and sediments shall be removed regularly. The Contractor shall provide a hard surfaced road between the wheel washing facilities, and the public or private right of way onto which the exit joins.
- (g) The Contractor shall at all times ensure that all existing stream courses and drains within and adjacent to the site are kept safe and free from any debris and any excavated materials arising from the Works. The Contractor shall ensure that chemicals and concrete agitator washings are not deposited in watercourses.
- (h) All water and other liquid waste products arising on the Site shall be collected, removed from Site via a suitable and properly designed temporary drainage system and disposed of at a location and in a manner that shall not cause either pollution or nuisance. In addition, the effluents shall comply with the standards stated in the "Technical Memorandum on Standards

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for Effluent discharged into Drainage and Sewerage System, Inland and Coastal Waters" for the appropriate Water Control Zone, whether or not the Zone has been declared as one subject to control of discharges.

- (i) The Contractor shall construct, maintain, remove and reinstate as necessary temporary drainage works and take all other precautions necessary for the avoidance of damage to works of adjacent contracts or to adjacent properties by flooding and silt washed down from the Works. He shall also provide adequate precautions to ensure that no spoil or debris of any kind is allowed to be pushed, washed down, fall or be deposited on land adjacent to the Site.
- (j) In the event of any spoil or debris from the Works being deposited on adjacent land or any silt washed down to any area, then all such spoil, debris and silt shall be immediately removed and the affected land and areas restored to their natural state by the Contractor to the satisfaction of the Resident Engineer.
- (k) No burning of debris, construction wastes or vegetation shall be allowed on the Site.
- (1) The Contractor shall segregate construction waste materials into inert and non-inert and chemical waste categories, and he shall dispose of them as follows:-
  - Inert construction waste material when deemed suitable for reclamation or land formation shall be disposed of at public dumping areas.
  - Inert material deemed unsuitable for reclamation or land formation and non-inert construction waste material shall be disposed of at public landfills.
  - Chemical wastes as defined by Schedule 1 of the Waste Regulations (Chemical) 1992, should be stored in accordance with approved methods defined in the Regulations and the chemical waste disposed of at the Chemical Waste Treatment Facility located at Tsing Yi.
- (m) All constructional Plant and equipment used on the Contract shall be fitted with a means of suppressing radio and television interference to the satisfaction of the Resident Engineer.
- (n) The Resident Engineer may require construction plant and equipment intended to be used on the Works to be made available for inspection and approval to ensure that it meets the requisite environmental standards.
- (o) The Contractor shall not install any furnace, boiler or other similar plant or equipment using any fuel that may produce air pollutants without the prior written consent of the Director of Environmental Protection (DEP) pursuant to the Air Pollution Control Ordinance.
- (p) The Contractor shall arrange methods of working to minimise noise impacts, and shall provide experienced personnel with suitable training to ensure that these methods are implemented.
- (q) The Contractor shall devise, arrange methods of working and carry out the works in such a manner so as to minimise noise impacts on the surrounding environment, and shall provide experienced personnel with suitable training to ensure that these methods are implemented.
- (r) The Contractor shall ensure that all plant and equipment to be used on the site are properly maintained in good operating condition and noisy construction activities shall be effectively sound-reduced by means of silencers, mufflers, acoustic linings, shields acoustic sheds, screens or other means to avoid disturbance to any nearby noise sensitive receivers.

(s) Notwithstanding the requirements and limitations set out in clause (h) above and subject to compliance with clauses (s) and (t) above, the Resident Engineer may upon application in writing by the Contractor, allow the use of any equipment and the carrying out of any construction activities for any duration provided that he is satisfied with the application which, in his opinion, to be of absolute necessity and adequate noise insulation has been provided to the educational institutions to be affected, or of emergency nature, and not in contravention with the Noise Control Ordinance in any respect.

#### 2. ENVIRONMENTAL MONITORING AND AUDIT REQUIREMENT

#### (a) Trigger, Action and Target Levels

The basic method of recording any changes in the environmental conditions is through monitoring of air quality and noise level. It has become a common practice to apply a range of environmental limits termed Trigger, Action and Target (TAT) levels to provide a framework for the interpretation of monitoring results. These levels are defined as follows :

Trigger -

Trigger levels provide an indication of deteriorating ambient environmental quality.

#### Action -

Action levels indicate the necessity to adopt appropriate remedial actions to prevent the environmental quality from going beyond the target limits. If levels go above target, appropriate remedial action, including critical review of plant and work methods would be required.

#### Target -

Target levels are stipulated in relevant pollution control ordinances, or HKPSG, or established by EPD for a particular project. These are the maximum levels at which the works should proceed.

TAT levels should be established after the completion of baseline monitoring to provide effective environmental management of the project.

Trigger, action and target levels must be realistic and related to existing conditions as well as statutory guidelines. Levels should not be set too low. If levels are set too low a continuous series of exceedances will diminish the effectiveness of monitoring. In case where exceedances of guidelines and statutory standards already exist, levels must take account of this. Alternatively, if levels are set too high, they will not be useful in indicating deteriorating conditions which could be controlled by mitigation measures.

#### 3. NOISE POLLUTION CONTROL

#### General Specification

- (a) The Contractor shall, when necessary, apply as soon as possible for a construction noise permit in accordance with the Noise Control (general) Regulations, display the permit as required and copy to the Resident Engineer.
- (b) Before the commencement of any work, the Contractor shall submit to the Resident Engineer for approval the method of working, equipment and sound-reducing measures intended to be used on the site.

- (c) The contractor shall take all necessary measures to ensure that the operation of all mechanical equipment and construction processes on or off the site shall not cause any unnecessary and excessive noise which may disturb any occupant of any nearby dwellings, schools, hospitals, or premises with similar sensitivity to noise. The Contractor shall submit to the Resident Engineer for his approval details of all Constructional Plant concurrent with his monthly report including methods of use and construction operations together with proposed measures for limiting noise therefrom that shall include, but not be limited to the relocation of noise emitting plant, the use of silencers, mufflers, acoustic sheds or shields, or acoustic sheds or screens and shall be based upon the best reasonable practice. Information on the types and models of silenced equipment and acoustic treatment for unsilenced equipment shall be included. The Contractor shall use all such measures and shall maintain all plant and silencing equipment in good condition so as to minimise the noise emission during construction works.
- (d) The Contractor's attention is drawn to the fact that Regulations under the Noise Control Ordinance are made form time to time. Those currently in force (December 1992) are :
  - Noise Control (Hand Held Percussive Breakers) Regulations
  - Noise Control (Air Compressors) Regulations
  - Noise Control (Hearing Protection) Regulations
  - The Factories and Industrial Undertakings (Noise at Work) Regulations

Two subsidiary Technical Memorandum are also available regarding construction noise issues:-

- Technical Memorandum (TM) on Noise from Construction Work Other Than Percussive Piling, TM(i)
- Technical Memorandum on Noise from Percussive Piling, TM(ii)

There is also a new version of the Technical Memorandum on Noise from Construction Work in Designated Areas, TM(iii), which governs the noise generated from the use of Specified Powered Mechanical Equipment other than Percussive Piling and/or the carrying out of Prescribed Construction Work within designated areas. This document shall be referenced to for future construction related noise issues.

- (e) The Contractor shall supply documentation to the Resident Engineer to demonstrate that all equipment complies with current equipment noise limits.
- (f) The Contractor shall be responsible for obtaining and complying with the requirements of EPD regarding identification of NSR's and conditions attached to CNP. All correspondence with EPD and each issued CNP shall be copied to the Resident Engineer.
- (g) The Contractor's attention is drawn to the fact that other construction works in the vicinity of the Site will be taken into account by EPD in assessing applications for CNP.

#### Non-Statutory Noise Control

(h) In addition to the requirements imposed by the Noise Control Ordinance, to control noise generated from equipment and activities for the purpose of carrying out any construction works other than percussive piling during the time period from 0700 to 1900 hours on any

day not being a general holiday (including Sundays), the following requirements shall also be complied with:

- i. The noise level measured at 1m from the most affected external facade of the nearby noise sensitive receivers from the construction works alone during any 30 minute period shall not exceed an equivalent sound level (Leq) of 75dB(A).
- ii. The noise level measures at 1m from the most affected external facades of the nearby schools from the construction works along during any 30 minutes period shall not exceed an equivalent sound level (Leq) of 70dB(A) [65 dB(A) during school examination periods]. The Contractor shall liaise with the schools and the Examination Authority to ascertain the exact dates and times of all examination periods during the course of the Contract.
- (i) Should the limits stated in the above sub-clauses (d) i. & ii. be exceeded, the construction shall stop and shall not recommence until appropriate measures acceptable to the Resident Engineer that are necessary for compliance have been implemented.
- (j) Any stoppage and reduction in output resulting from compliance with this clause shall not entitle the Contractor to any extension of time for completion or additional costs whatever.

#### To Provide Sound Level Meter

- (k) The Contractor shall provide an approved integrating sound level meter to IEC 651:1979 (Type 1) and 804 : 1985 (Type 1) or its equivalent and the manufacturer's recommended sound level calibrator for the exclusive use of the Resident Engineer at all times. The Contractor shall maintain the equipment in proper working order and provide a substitute when the equipment are out of order or otherwise not available.
- (1) The sound level meter including the sound level calibrator shall be certified by the manufacturers every two years to ensure they perform the same levels of accuracies as stated in the manufacturer's specifications. That is to say at the time of measurements, the equipment shall have been verified within the last two years.
- (m) Portable equipment should be made available for ad-hoc noise measurements as when compliance is in doubt or as required by the Resident Engineer. The location and frequency shall be decided at the discretion of the Resident Engineer and all cost including equipment shall be borne by the Main Contractor.

#### Environmental Monitoring and Auditing

(n) The following are general guidelines for Environmental Monitoring and Auditing requirements for the Hung Shiu Kiu Development. The Environmental Monitoring and Auditing manual shall be referred to for details.

#### **Baseline Monitoring**

- (o) The baseline monitoring should be carried out in all of the monitoring stations identified by the Resident Engineer for at least two consecutive weeks prior to the commissioning of the construction works. A set of background data shall be available for each of the following schedule:-
  - 3 times a week during daytime (0700-1900) on different days, any days other than general holidays including Sundays;
  - 3 times a week during the evening (1900-2300) of all days;
  - during daytime and evening (0700-2300) of general holidays (including all Sundays);

• 3 times a week during all night periods (2300-0700).

#### Regular Monitoring

(p) The Main Contractor shall ensure that the noise levels from construction activities when measured at 1 meter from site boundary during any 5-minute period shall not exceed an equivalent continuous sound level (Leq) of 75dB(A) at all times.

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(q) The Main Contractor shall be responsible for producing a work plan detailing the noise monitoring tasks. The plan should detail the location of monitoring, noise criteria, the personnel, measuring equipment and monitoring schedule. The monitoring schedule should specify that a minimum of 3 measurements shall be taken on each Saturday and Sunday (if working is permitted) between 10:00 - 11:00 hours, 11:00 - 12:00 hours and 14:00 - 15:00 hours. The results of noise monitoring should be summarised in the Main Contractor's monthly report to highlight whether or not the construction activity has complied with the noise criteria. Recommendations should be given by the Main Contractor, where required, for improvements to noise control of construction methods.

#### DUST SUPPRESSION MEASURES

#### General Specification

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- (a) The Contractor shall undertake at all time to prevent dust nuisance as a result of his activities. The air pollution control system shall be operated whenever the plant is in operation.
- (b) The Contractor shall at his own cost, and to the satisfaction of the Resident Engineer, install effective dust suppression equipment and take such other measures as may be necessary to ensure that at the site boundary and any nearby sensitive receivers the concentration of airborne dust shall not exceed 0.5 milligrams per cubic meter at standard temperature (25°C) and pressure (1.0 bar) average one hour, and 0.26 milligrams per cubic metre, at standard temperature (25°C) and pressure (1.0 bar) averaged over 24 hours.
- (c) In the process of material handling, any material which has the potential to create dust shall be treated with water or sprayed with wetting agent.
- (d) If after commencement of the Works the Constructional plant, equipment or methods of working are believed by the Resident Engineer to be causing serious air pollution impacts they shall be inspected and remedial proposals shall be drawn up by the Contractor, consented to by the Resident Engineer and implemented. In developing these remedial measures the contractor will be expected to inspect and review all dust sources that may be contributing to the pollution impacts. Where such remedial measures include the use of additional or alternative Construction Plant or equipment such Constructional Plant or equipment shall not be used on the Works until the Resident Engineer's consent has been given. Where remedial measures include maintenance or modification of Constructional Plant or equipment which has received the consent of the Resident Engineer such Constructional Plant or equipment shall not be used on the Works until such maintenance or modification is completed and the adequacy of the maintenance of modification is demonstrated to the satisfaction of the Resident Engineer.
- (e) Where dusty material are being discharged to vehicle from conveying system at a fixed transfer point, a three-sided roofed enclosure with a flexible curtain across the entry shall be provided. Exhaust should be provided for this enclosures and vented to a fabric filter system.
- (f) Any vehicles with an open load carrying area used for moving materials which have the potential to create dust shall have properly fitting site and tail boards. Materials having the potential to create dust shall not be loaded to a level higher than the side and tail boards, and shall be covered by a clean tarpaulin. The tarpaulin shall be properly secured and shall extended at least 300mm over the edges of the sides and tail boards.
- (g) Stockpiles of sand and aggregates greater than 20m<sup>3</sup> shall be enclosed on three sides, with wall extending above the pile and 2 metres beyond the front of the pile. In addition, water sprays shall be provided and used to dampen stored materials and when receiving raw material.
- (h) The Contractor shall frequently clean and water the site to minimises the fugitive dust emissions.
- (i) The Contractor shall restrict all motorised vehicles to a maximum speed of 5 km per hour and confine haulage and delivery vehicles to designated roadways inside the site. Areas of the roadway longer than 100m where movement of motorised vehicles exceed 100 vehicular movements/days or as directed by the Resident Engineer shall be furnished with a hard pavement surfacing.

- (j) Areas within the Site where there is a regular movement of vehicles shall have an approved hard surface and be kept clean of loose surface material.
- (k) Wheel washing facilities shall be installed and used by all vehicles leaving the site. No earth, mud, debris, dust and the like shall be deposited on public roads. Water in the wheel cleaning facility shall be changed at frequent intervals and sediments pool shall be usable prior to any earthworks excavation activity on site. The Contractor shall also provide a hard-surfaced road between washing facility and the public road.
- (1) The Contractor shall not install any furnace, boiler or other plant or equipment or use any fuel that might generate excessive smoke or any other pollutants without the prior consent of the Resident Engineer. Unless specifically instructed by the Resident Engineer, the Contractor shall not light fires on site for the burning of debris or any other matter.
- (m) The Contractor's attention is drawn to the Air Pollution Control Ordinance and its current subsidiary legislation, particularly the Air Pollution (Furnaces, Ovens, and Chimneys) (Installation and Alteration) Regulations, Air Pollution Control (Smoke) Regulations and Air Pollution Control (Specified Process) Regulations.
- (n) The Contractor shall arrange his blasting techniques so as to minimise dust generation.
- (o) The Contractor shall ensure that completed earthworks are sealed and hydroseeded and planted as soon as practicable with regard to growing season.
- (p) The Contractor shall minimise the extent of soil exposed at any one time.

#### To Provide Dust Monitoring Equipment:

- (q) The TSP monitor should be a high volume sampler as referenced in the USEPA Standard Method 40, CFR Part 50, Appendix B or its equivalent. Equipment list shall be submitted for approval by the Resident Engineer prior to commencement of monitoring work.
- (r) Portable 1-hour Dust Meter should be made available to perform ad-hoc air monitoring when sources of dust are in doubt or as required by the Resident Engineer. The location and frequency shall be decided at the discretion of the Resident Engineer and all cost including equipment shall be borne by the Main Contractor.

#### Baseline Monitoring

- (s) The baseline monitoring should be carried out in all of the monitoring stations identified by the Resident Engineer for at least two consecutive weeks prior to the commissioning of the construction work according to the following frequency:-
  - daily for 24-hour sampling, and
  - at least 3 times per day for 1-hour sampling which should be taken while the highest dust impact is expected.
- (t) There should not be any construction or dust generation activities in the vicinity of the stations during baseline monitoring.

(u) In case no monitoring data or questionable results are submitted, the Resident Engineer under reasonable consideration has the right to assign a new set of data to be used as baseline reference.

#### Regular Monitoring

- (v) In regular impact monitoring, the sampling frequency of at least once for every six-day should be strictly observed in all of the monitoring stations for 24-hour monitoring. For the 1hour monitoring, 3 times for every 6-day at the highest dust impact occasion should be observed.
- (w) Specific time to start and stop the 24-hour TSP monitoring should be clearly defined for each location by the Environmental and Auditing Consultant and strictly followed by the operator.

#### Non-compliance Impact Monitoring

(x) In case of non-compliance with the air quality criteria, more frequent monitoring exercise should be conducted within 24 hours. This additional monitoring should be continued until the excessive dust emission of the deterioration in air quality problem is rectified.

If on-site cement batching facilities exist, the following clauses shall be deemed applicable:-

- (y) Conveyor belts shall be fitted with windboards, and conveyor transfer points and hopper discharge areas shall be enclosed to minimise emission of dust. All conveyors carrying materials which have the potential to create dust shall be totally enclosed and fitted with belt cleaners.
- (z) Cement or pulverised ash delivered in bulk shall be stored in closed silos fitted with high level alarm indicator. The high level alarm indicators shall be interlocked with filling line such that in the event of the hopper approaching an overfull condition, an audible alarm will operate, and after 1 minute the pneumatic line to the filling tanker will close.
- (aa) All air vents on cement silos shall be fitted with fabric filters provided with either shaking or pulse-air cleaning mechanisms. The fabric filter area shall be determined using the air to cloth ratio (0.01 - 0.03 m/s) or the filtering velocity.
- (bb) The Contractor shall frequently clean and water the concrete batching plant and crushing plant site and ancillary areas to minimise any dust emissions.
- (cc) Weigh hoppers shall be vented to suitable filter.
- (dd) The filter bags in the cement silo dust collector must be thoroughly shaken after cement is blown into the silo to ensure adequate dust collection for subsequent loading.
- (ee) For dry mix batching, the process should be done in total enclosure with exhaust to fabric filter.
- (ff) All cement and concrete trucks are to be effectively washed down after loading and prior to leaving the works.
- (gg) The Contractor shall provide and operate two high volume air samplers and associated equipment and shelters in accordance with the USA standard Title 40, Code of Federal Regulations, Chapter 1 (Part 50) Appendix B. Sampling shall be carried out 3 times in every 6 days at 10 No. sampling points on the site boundary for such periods and in a manner as instructed by the Resident Engineer. The samplers, equipment and shelters shall be constructed so as to be transferable between sampling points to enable monitoring of "dust in air" levels at any sampling points. Testing and analysis of sampled materials shall be carried out by a laboratory approved by the Resident Engineer.

#### 5. REMOVAL OF WASTE MATERIAL

- (a) The Contractor shall not permit any sewage, waste water of effluent containing sand, cement, silt or any suspended or dissolved material to flow from the site onto any adjoining land or allow any waste matter or refuse to be deposited anywhere within the site or onto any adjoining land and shall have all such matter removed from the site.
- (b) The Contractor shall be liable for any damages caused to adjoining land through his failure to comply with clause 6(a).
- (c) The Contractor shall be responsible for temporary training, diverting or conducting or open streams or drains intercepted by any works and for reinstating these to their original courses on completion of the Works.
- (d) The Contractor shall be responsible for adequately maintaining any existing site drainage system at all times including removal of solids in sand traps, manholes and stream beds.
- (e) Any proposed stream course and nullah temporary diversions shall be submitted to the Resident Engineer for agreement one month prior to such diversion works being commenced. Diversions shall be constructed to allow the water flow to discharge without overflow, erosion or washout. The are through which the temporary diversion runs is to be reinstated to its original condition or as agreed by the Resident Engineer after the permanent drainage system has been completed.
- (f) The Contractor shall furnish, for the Resident Engineer's information, particulars of the Contractor's arrangements for ensuring that material from any earthworks does not wash into the drainage system. If at any such arrangements prove to be ineffective the Contractor shall take such additional measures as the Resident Engineer shall deem necessary and shall remove all silt which may have accumulated in the drainage system whether within the Site or not.
- (g) The Contractor shall segregate all inert construction waste material suitable for reclamation or land formation and shall dispose of such material at such public dumping area(s) as may be specified from time to time by the Director of Civil Engineering Services.
- (h) All non-inert construction waste material deemed unsuitable for reclamation or land formation and all other waste material shall be disposed of at a public landfill.
- (i) The Contractor's attention is drawn to the Waste Disposal Ordinance, the Public Health and Municipal Services Ordinance and the Water Pollution Control Ordinance.
- (j) Any dredged material shall be disposed of at an approved marine dumping ground.

#### 6. DISCHARGE INTO SEWERS AND DRAINS

- (a) The Contractor shall not discharge directly or indirectly (by runoff) or cause or permit or suffer to be discharged into any public sewer, storm-water drain, channel, stream-course or sea, any effluent or foul or contaminated water of cooling or hot water without the prior consent of the Resident Engineer who may require the Contractor to provide, operate and maintain at the Contractor's own expense, within the premises of otherwise, suitable works for the treatment and disposal of such effluent or foul or contaminated or cooling or hot water. The design of such treatment works shall be submitted to the Resident Engineer for approval not less than one month prior to the commencement of construction or as agreed by the Resident Engineer.
- (b) If any office, site canteen or toilet facilities is erected, foul water effluent shall be directed to a foul sewer or to a sewage treatment facility either directly or indirectly by means of pumping or other means approved by the Resident Engineer.
- (c) The Contractor's attention is drawn to the Buildings Ordinance and to the Water Pollution Control Ordinance.

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Cost Estimation for Proposed Noise Barriers and Noise Insulation

### COST ESTIMATION FOR PROPOSED NOISE BARRIERS

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Noise Barrier Label	Barrier Height	Length	Estimated Approximate Cost (HK\$)*
D2EB-1	2m	120m	1,200,000
D2EB-2	2m	163m	1,630,000
D2WB-1	5m	70m	1,330,000
D2WB-2	5m	154m	2,926,000
L1EB-1	3m	<u>1</u> 0бт	1,378,000
L2EB-2	3m	63m	819,000
C	9,283,000		
Total Cost (+ 15	10,675,450		

\* Cost estimated based on an unit cost of HK\$10,000/ metre for 2m high noise barrier, 13,000/ metre for 3m high noise barrier, and 19,000/ metre for 5m high noise barrier.

