Appendix 4.7a Calculation of Construction Ground-borne Noise Levels during Non-Restricted Hours (Unmitigated Scenario)

Ground-borne Noise (GBN) from TBM resulting from the construction of new middle third tunnel

NSR ID.: PHD NSR Name : Planned Housing Development (NKIL6579)

Lp = L_{v,rms} + C_{dist} + C_{damping} + C_{building} + C_{floor} + C_{noise} + C_{multi} + C_{cum}

| Item | Description | Quantity | Reference and Assumption |
|-----------------------|---|------------|---|
| L _{v,rms} | Vibration source term (Peak Particle Velocity | 2.5 mm/s | Ref: Kowloon Canton Railway Corporation Kowloon Southern Link |
| | (PPV)) at R ₀ | | Environmental Impact Assessment Report (KSL) EIA Appendix 7-2-3 |
| | (from Graph1 DB320 Kwai Tsing Tunnel by | | PPV at 5.5m |
| | Exptrapolation) | | |
| | rms velocity | 0.625 mm/s | Lv,rms = PPV / Crest Factor, Crest Factor = 4 |
| | L _{v, rms} | 115.92 VdB | |
| C _{dist} | Distance Attenuation: -20*log (R/R ₀) | -26.8 dB | R = 121m; R ₀ =5.5m |
| C _{damping} | Soil Damping | 0 dB | Assume no soil damping as the vibration would transmit through rock layer |
| C _{building} | Coupling Loss into Building Structures | 0 dB | For conservative approach, no correction is assumed |
| C _{floor} | Floor to Floor Attenuation | 0 dB | 1 dB/ floor is assumed |
| C _{noise} | Conversion from Floor Vibration to Noise Levels | -27 dB | Reference from KSL EIA Report Appendix 7.1 |
| C _{multi} | Noise Level Increase due to Multiple Sources | 0 dB | Only 1 TBM will be operated |
| C _{cum} | Cumulative Effect due to Neighbouring Sites | 0 dB | No concurrent project identified within 300m from the NSR |
| Vibration to Noise | Conversion to A-weighted Noise | -20 dB | From the "Transit Noise and Vibration Impact Assessment" |
| | Predicted TBM Ground-borne Noise Level | 42 dB(A) | |

Appendix 4.7a Calculation of Construction Ground-borne Noise Levels during Non-Restricted Hours (Unmitigated Scenario)

Ground-borne Noise (GBN) from PME Operation

NSR ID. :

PHD Planned Housing Development (NKIL6579) NSR Name :

Construction of New Middle Third Tunnel

| PME: | Hydraulic Breaker | | | | | | | | |
|-----------------------|---|---------|---------|----------|----------|----------|-------|-------|--|
| Item | Description | | | | | | | | Reference and Assumption |
| | Octave Band Frequency | 16 | 31.5 | 63 | 125 | 250 | 500 | Hz | |
| L _{v.rms} | Source Vibration Velocity | 0.06 | 0.07 | 0.06 | 0.05 | 0.06 | 0.12 | mm/s | Reference from KSL EIA Appendix 7-1 |
| | Vibration Velocity, ref 10 [^] -6 mm/s | 96 | 97 | 96 | 94 | 96 | 102 | dB | |
| C _{dist} | Distance Attenuation: -20*log (R/R ₀) | -26.8 | -26.8 | -26.8 | -26.8 | -26.8 | -26.8 | dB | R = 121m; R ₀ =5.5m |
| C _{damping} | Soil Damping | 0 | 0 | 0 | 0 | 0 | 0 | dB | Assume no soil damping correction as vibration would transmit through rock layer |
| C _{building} | Coupling Loss into Building Structures | 0 | 0 | 0 | 0 | 0 | 0 | dB | For conservative approach, no correction is assumed |
| C _{floor} | Floor to Floor Attenuation | 0 | 0 | 0 | 0 | 0 | 0 | dB | 1 dB/ floor is assumed |
| C _{noise} | Conversion from Floor Vibration to Noise Levels | -27 | -27 | -27 | -27 | -27 | -27 | dB | Reference from KSL EIA Report Appendix 7.1 |
| C _{multi} | Noise Level Increase due to Multiple Sources | 0 | 0 | 0 | 0 | 0 | 0 | dB | |
| C _{cum} | Cumulative Effect due to Neighbouring Sites | 0 | 0 | 0 | 0 | 0 | 0 | dB | No concurrent project identified within 300m from the NSR |
| Vibration to Noise | Conversion to A-weighted Noise | -56.7 | -39.4 | -26.2 | -16.1 | -8.6 | -3.2 | dB | Standard acoustical principles |
| | Ground-borne Noise | -15 | 4 | 16 | 24 | 33 | 45 | dB(A) | |
| | Predicted Ground-borne Noise Level for 1 | | | | | | | | |
| | Hydraulic Breaker | | | | | | 44.9 | dB(A) | |
| | | | | | | | | | |
| PME: | Drill Rig | | | | | | | | |
| | Using the calculated hydraulic breaker | noise t | o corre | ect to D | rill Rig | Noise | 5.1 | dB(A) | 20 log(0.536/0.298) |
| | Predicted Ground | l-borne | e Noise | Level | for 1 D | rill Rig | 50 | dB(A) | |

| PME: | Hand-held Breaker | | | |
|------|--|-------|-------|---------------------|
| | Using the calculated hydraulic breaker noise to correct to Hand-held Breaker Noise | -0.57 | dB(A) | 20 log(0.279/0.298) |
| | Predicted Ground-borne Noise Level for 1 Hand-held Breaker | 44 | dB(A) | |

| Construction Activity | PME | No. of PME | GBN Level |
|---|-------------------------------|----------------|-----------|
| Construction of New Middle Third Tunnel | Hydraulic Breaker | 2 | 48 dB(A) |
| | Drill Rig | 5 | 57 dB(A) |
| | Hand-held Breaker | 3 | 49 dB(A) |
| | TBM | 1 | 42 dB(A) |
| | Overall Predicted Ground-born | e Noise Level | 58 dB(A) |
| | Daytime Ground-borne N | loise Criteria | 65 dB(A) |
| | Complia | nce (Yes/No) | Yes |

Enlargement of Existing Kowloon bound Tunnel

| PME: | Hydraulic Breaker | | | | | | | | |
|-----------------------|---|-------|-------|-------|-------|-------|-------|-------|--|
| Item | Description | | | | | | | | Reference and Assumption |
| | Octave Band Frequency | 16 | 31.5 | 63 | 125 | 250 | 500 | Hz | |
| L _{v.rms} | Source Vibration Velocity | 0.06 | 0.07 | 0.06 | 0.05 | 0.06 | 0.12 | mm/s | Reference from KSL EIA Appendix 7-1 |
| | Vibration Velocity, ref 10 [^] -6 mm/s | 96 | 97 | 96 | 94 | 96 | 102 | dB | |
| C _{dist} | Distance Attenuation: -20*log (R/R ₀) | -28.4 | -28.4 | -28.4 | -28.4 | -28.4 | -28.4 | dB | R = 145m; R ₀ =5.5m |
| C _{damping} | Soil Damping | 0 | 0 | 0 | 0 | 0 | 0 | dB | Assume no soil damping correction as vibration would transmit through rock layer |
| C _{building} | Coupling Loss into Building Structures | 0 | 0 | 0 | 0 | 0 | 0 | dB | For conservative approach, no correction is assumed |
| C _{floor} | Floor to Floor Attenuation | 0 | 0 | 0 | 0 | 0 | 0 | dB | 1 dB/ floor is assumed |
| C _{noise} | Conversion from Floor Vibration to Noise Levels | -27 | -27 | -27 | -27 | -27 | -27 | dB | Reference from KSL EIA Report Appendix 7.1 |
| C _{multi} | Noise Level Increase due to Multiple Sources | 0 | 0 | 0 | 0 | 0 | 0 | dB | |
| C _{cum} | Cumulative Effect due to Neighbouring Sites | 0 | 0 | 0 | 0 | 0 | 0 | dB | No concurrent project identified within 300m from the NSR |
| Vibration to Noise | Conversion to A-weighted Noise | -56.7 | -39.4 | -26.2 | -16.1 | -8.6 | -3.2 | dB | Standard acoustical principles |
| | Ground-borne Noise | -17 | 2 | 14 | 22 | 32 | 43 | dB(A) | |
| | Predicted Ground-borne Noise Level for 1 Hydraulic Breaker | | | | | | 43.3 | dB(A) | |

| Construction Activity | PME | No. of PME | GBN Level | | | | |
|--|-------------------------------------|------------|-----------|--|--|--|--|
| Enlargement of Existing Kowloon bound Tunnel | Hydraulic Breaker | 4 | 49 dB(A) | | | | |
| C | Daytime Ground-borne Noise Criteria | | | | | | |
| | Compliance (Yes/No) | | | | | | |

Rehabilitation of Existing Shatin Bound Tunnel

| PME: | Hydraulic Breaker | | | | | | | | |
|-----------------------|---|-------|-------|-------|-------|-------|-------|-------|--|
| Item | Description | | | | | | | | Reference and Assumption |
| | Octave Band Frequency | 16 | 31.5 | 63 | 125 | 250 | 500 | Hz | |
| Lyrms | Source Vibration Velocity | 0.06 | 0.07 | 0.06 | 0.05 | 0.06 | 0.12 | mm/s | Reference from KSL EIA Appendix 7-1 |
| | Vibration Velocity, ref 10 [^] -6 mm/s | 96 | 97 | 96 | 94 | 96 | 102 | dB | |
| C _{dist} | Distance Attenuation: -20*log (R/R ₀) | -25.2 | -25.2 | -25.2 | -25.2 | -25.2 | -25.2 | dB | R = 100m; R ₀ =5.5m |
| C _{damping} | Soil Damping | 0 | 0 | 0 | 0 | 0 | 0 | dB | Assume no soil damping correction as vibration would transmit through rock layer |
| C _{building} | Coupling Loss into Building Structures | 0 | 0 | 0 | 0 | 0 | 0 | dB | For conservative approach, no correction is assumed |
| C _{floor} | Floor to Floor Attenuation | 0 | 0 | 0 | 0 | 0 | 0 | dB | 1 dB/ floor is assumed |
| C _{noise} | Conversion from Floor Vibration to Noise Levels | -27 | -27 | -27 | -27 | -27 | -27 | dB | Reference from KSL EIA Report Appendix 7.1 |
| C _{multi} | Noise Level Increase due to Multiple Sources | 0 | 0 | 0 | 0 | 0 | 0 | dB | |
| C _{cum} | Cumulative Effect due to Neighbouring Sites | 0 | 0 | 0 | 0 | 0 | 0 | dB | No concurrent project identified within 300m from the NSR |
| Vibration to Noise | Conversion to A-weighted Noise | -56.7 | -39.4 | -26.2 | -16.1 | -8.6 | -3.2 | dB | Standard acoustical principles |
| | Ground-borne Noise | -13 | 5 | 17 | 26 | 35 | 46 | dB(A) | |
| | Predicted Ground-borne Noise Level for 1 | | | | | | | | |
| | Hydraulic Breaker | | | | | | 46.6 | dB(A) | |

| Using the calculated hydraulic breaker noise to correct to Drill Rig Noise 5.1 dB(A) 20 log(0.536/0.298) Predicted Ground-borne Noise Level for 1 Drill Rig 52 dB(A) | PME: | Drill Rig | | | | |
|---|------|-----------|--|-----|-------|---------------------|
| Predicted Ground-borne Noise Level for 1 Drill Rig 52 dB(A) | | | Using the calculated hydraulic breaker noise to correct to Drill Rig Noise | 5.1 | dB(A) | 20 log(0.536/0.298) |
| | | | Predicted Ground-borne Noise Level for 1 Drill Rig | 52 | dB(A) | |

Appendix 4.7a Calculation of Construction Ground-borne Noise Levels during Non-Restricted Hours (Unmitigated Scenario)

| Construction Activity | PME | No. of PME | GBN Level | | | | | | |
|--|--|----------------|-----------|--|--|--|--|--|--|
| Rehabilitation of Existing Shatin Bound Tunnel | Hydraulic Breaker | 1 | 47 dB(A) | | | | | | |
| | Drill Rig | 1 | 52 dB(A) | | | | | | |
| Overall Pred | Overall Predicted Ground-borne Noise Level | | | | | | | | |
| Dayt | ime Ground-borne N | loise Criteria | 65 dB(A) | | | | | | |
| | Complia | nce (Yes/No) | Yes | | | | | | |